

Article

Tailing Ash for the Removal of Methylene Blue from Aqueous Solutions by Batch Adsorption

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Abstract: One of the more problematic textile wastewaters to manage is dyeing wastewater, especially methylene-blue-containing wastewater. Its release has a significant negative impact on ecosystems, which could harm the environment. Adsorption techniques are still an efficient technology to eliminate and remove the coloring agent. Tailing ash, obtained from the floatation process, was selected as an adsorbent in the present study. The purpose of this study was to analyze the performance of tailing ash (TA) for MB removal. The effects of operating parameters investigated were pH (2–10), stirring speed (50–150 rpm), initial dye concentration (20–100 mg/L), contact time (120 min), adsorbent dosage (0.5–2.5 g), and temperature (25–45 °C). The performance of TA pretreated with hydrogen peroxide (H₂O₂) and thermal tailing ash were also investigated. The experimental results for batch adsorption indicated that 96.23% removal of methylene blue took place at the optimum condition (pH = 10, initial adsorbent dosage = 1.5 g, 150 rpm, contact time = 120 min, 45 °C). The results showed that the dye adsorption capacity increased with contact time and adsorbate dosage. The adsorption data were then fitted to kinetic models and isotherm models. The pseudo-second-order model was the most suitable model for the kinetic of adsorption and the Freundlich isotherm was the best-fitted isotherm model. This research provides a feasible approach to reusing tailing ash as an effective low-cost adsorbent for water quality improvement.



Citation: Yahya, C.J.F.b.; Choong, T.S.Y.; Li, F.; Ghani, W.A.W.A.K.; Aziz, F.N.A.A.; Jamil, S.N.A.M. Tailing Ash for the Removal of Methylene Blue from Aqueous Solutions by Batch Adsorption. *Processes* **2023**, *11*, 2282. <https://doi.org/10.3390/pr11082282>

Academic Editor: Luis Puigjaner

Received: 3 May 2023

Revised: 28 June 2023

Accepted: 6 July 2023

Published: 28 July 2023

Keywords: tailing ash; adsorption; dye



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1. Introduction

Despite being a major CO₂ emitter, power generation using coal is still important from an economic point of view. Annually, more than 780 million metric tons of coal conversion ash are produced worldwide [1,2]. Coal is still being used significantly in energy production [3]. Power generation using coal as fuel produces fly ash and bottom ash. In Malaysia, fly ash can be used in cement factories [4]. Coal bottom ash is of limited use due to its high carbon content.

A large area is required to dispose of the large amount of bottom ash, which eventually becomes a source of pollution. From the viewpoint of a circular economy, coal bottom ash could be utilized as a resource. In the European Project CHARPHITE under the scope of the “Third ERA-MIN Joint Call (2015) on Sustainable Supply of Raw Materials in

Europe" [5], unburned carbon was recovered to be utilized as graphite material. After the unburned carbon is recovered, a large quantity of tailing is left behind. It is important to find use for the tailing. Adsorption is a widely applied method for the removal of color in textile wastewater. Compared to methods such as biotreatment, flocculation–coagulation, photocatalytic degradation, Fenton chemical oxidation, cation exchange membranes, and electrochemical degradation, adsorption has the advantages of the availability of material and simple design and operation [6]. The literature shows that a significant number of waste products have been utilized as adsorbents. These include coal, peat, fly ash, bagasse, iron slag, shale oil ash, zeolites, magnesium chloride, maize cob, and wool [6].

The present paper is an attempt to investigate the possibility of utilizing waste material tailing ash derived after the flotation of coal bottom ash to remove the well-known dye methylene blue. The aims of this paper are to report the effect of various process parameters on the removal of the dye, to optimize the process parameters, and to apply several adsorption isotherms and kinetic equations to the adsorption rate.

2. Materials and Methods

2.1. Materials

The tailing ash used here is a by-product derived after the recovery of unburned carbon from coal bottom ash, which was acquired from TNB Janamanjung. This material was taken directly from the bottom of a combustion chamber. Methylene blue was purchased from Sigma Aldrich (St Louis, MO, USA). Hydrogen peroxide (H₂O₂, 30%) was acquired from Merck. The 1000 mg/L methylene blue dye stock solution was prepared by dissolving 1.0 g of methylene blue (MB, C₁₆H₁₈ClN₃S, structure shown in Figure 1) in 1000 mL distilled water. The distilled water was used throughout the experiment to prepare the desired concentration range of the solutions. The 0.1 M hydrochloric acid (HCl) and 0.1 M sodium hydroxide (NaOH) solutions were used to adjust the pH.

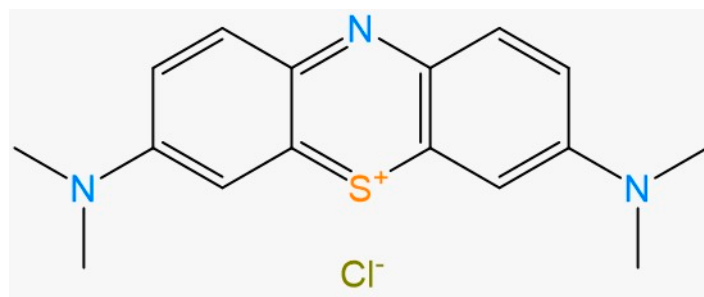


Figure 1. Chemical structure of methylene blue.

2.2. Analytical Method

A UV–visible spectrophotometer (HITACHI U-2010) was used to monitor the adsorption process and the Brunauer–Emmett–Teller (BET) nitrogen adsorption method was used to determine the surface area of the tailing ash. The tailing ash's basic elemental composition was analyzed using X-ray fluorescence spectrometry (XRF) (ZSX Primus IV) and the salt titration method was used to measure the point of zero charge (PZC). The pH_{pzc} was measured using the pH drift method.

The adsorbent was first acquired from the flotation process to obtain 63 μm sized powder. It was washed successfully with distilled water and then dried at 100 °C to remove the moisture. The adsorbent was stored in desiccators until use.

2.3. Flotation Process

The column flotation was carried out at pH of 6, 7.5, and 9 with the air flowrate injected at 4 to 10 L/min for 10 min of conditioning time. Additionally, 1000, 3000, and 5000 g/ton kerosene and 1400, 1600, and 1800 g/ton MIBC were used as the reagent. Kerosene and MIBC act as a collector and frother, respectively. The flotation experiment was carried

out in a glass column with a 6 cm diameter and 2.0 L capacity. The size of the bottom ash was fixed at 63 μm and loaded at 50 g/L. Each sample was conditioned in water for 5 min to ensure complete wetting at the desired pH before the addition of reagents. The conditioning period for the kerosene was 2 min and for MIBC was 30 s. The kerosene and MIBC were added in droplets. The conditioning period for each test was 10 min. At the end of the experiment, the flotation products (called concentrates) were filtered, dried, and weighed.

2.4. Methylene Blue Concentration Determination

Using a UV-visible spectrophotometer (HITACHI U-2010), the concentration of methylene blue was determined spectrophotometrically by taking measurements at the absorbance maximum. A calibration curve was plotted between the absorbance and the concentration of the methylene blue solution to obtain the absorbance concentration profile. The amount of methylene blue uptake per unit of adsorbent was calculated using the following equation:

$$q_e = \frac{C_0 - C_e}{m} V \quad (1)$$

$$q_t = \frac{C_0 - C_t}{m} V \quad (2)$$

where C_0 (mg/L) and C_t (mg/L) are the methylene blue concentration initially and at time t , respectively; C_e (mg/L) is the methylene blue concentration at the adsorption equilibrium; q_e and q_t are the adsorption capacity at equilibrium and at time t , respectively; V (L) is the volume of methylene blue solution; and m (g) is the weight of the tailing ash.

2.5. Adsorption Study

The adsorption studies were conducted in batches. A conical flask solution containing 100 mL of MB solution at 20 mg/L was used as a control sample in this study. A fixed amount of tailing ash was added to a conical flask solution containing 100 mL of MB solution at 20–100 mg/L.

The flasks were then mechanically agitated intermittently at room temperature to achieve equilibrium. The supernatant was carefully filtered through a 0.45 μm syringe filter when equilibrium was reached within 75 to 120 min. Then the samples were analyzed spectrophotometrically by measuring the absorbance at the maximum wavelength of 660 nm. All of the experiments were conducted in triplicate. A schematic diagram of the adsorption study is shown in Figure 2.

The dye removal efficiency (%R) was calculated using Equation (3).

$$\%R = \frac{C_0 - C_e}{C_0} \times 100 \quad (3)$$

2.6. Material Development

2.6.1. Tailing Ash Pretreated with H_2O_2

After about 24 h, the small-sized granules of tailing ash were immersed into a hydrogen peroxide solution (30% w/v) to oxidize all undesired organic impurities from it. The solution was then filtered and washed again several times by doubly distilled water. The material was then kept in an oven at 100 $^\circ\text{C}$ to remove the moisture for about 15 min. It was then stored in vacuum desiccators until further use.

2.6.2. Thermal Tailing Ash

Further heat treatment was required to produce the thermal tailing ash. This was accomplished by heating the dried material in a furnace at 500 $^\circ\text{C}$ for about 30 min. The product was then stored in a vacuum desiccator until further use.

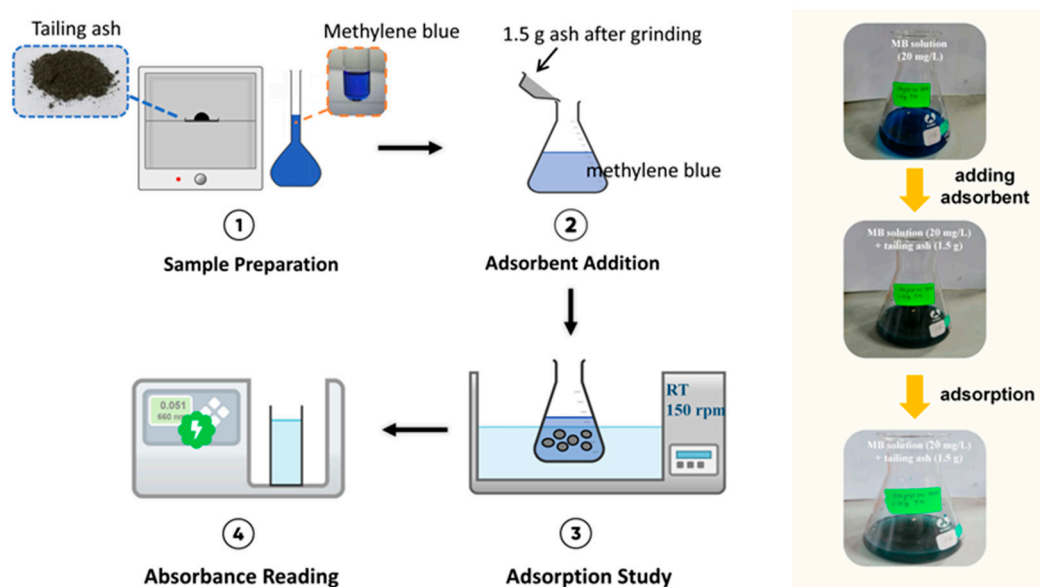


Figure 2. Schematic diagram of adsorption study.

3. Results

3.1. Characterization

According to Gupta and Suhas [7], low-cost adsorbents can be employed to remove dyes where adsorption capacities depend on their surface area or micro/meso porosity, pore size distribution, and particle size. The results of the characterization of the tailing ash are shown below.

3.1.1. XRF Analysis Results

Table 1 shows the results of the XRF analysis of the tailing ash. It is noted that the main composition of the tailing ash is SiO_2 , Al_2O_3 , Fe_2O_3 , CaO , and the residual carbon from coal burning. Silica, alumina, iron, and calcium oxide were the major contents of the bottom ash. The highest was SiO_2 (wt 32.52%), followed by CaO (wt 16.93%), Fe_2O_3 (wt 15.95%), and Al_2O_3 (wt 10.96%), which had the possibility to remove dye from wastewater.

Table 1. Results of XRF analysis of tailing ash.

Component	wt (%)
SiO_2	32.52
Al_2O_3	10.96
Fe_2O_3	15.95
CaO	16.93
MgO	6.83
K_2O	0.71
Na_2O	0.63
TiO_2	0.83
SO_3	0.58
Cl	-
P_2O_5	0.21
BaO	0.25
MnO	0.14
SrO	0.17
ZrO_2	0.03
V_2O_5	-
Cr_2O_3	0.02
CeO_2	0.03
ZnO	0.01

3.1.2. SEM Analysis Results

The morphology of the tailing ash samples was influenced by the combustion temperature and cooling rate during the incineration process [8]. Figure 3 shows the morphology of the tailing ash, showing the pores and surface texture. High surface porosity was observed in the pieces, and this decreased their thermal conductivity. The samples consisted of irregularly shaped, hollow, and spherical particles (ceno-spheres), which had also been reported in other studies [9]. Moreover, the irregularly shaped and dark particles seen in the tailing ash were likely related to carbon.

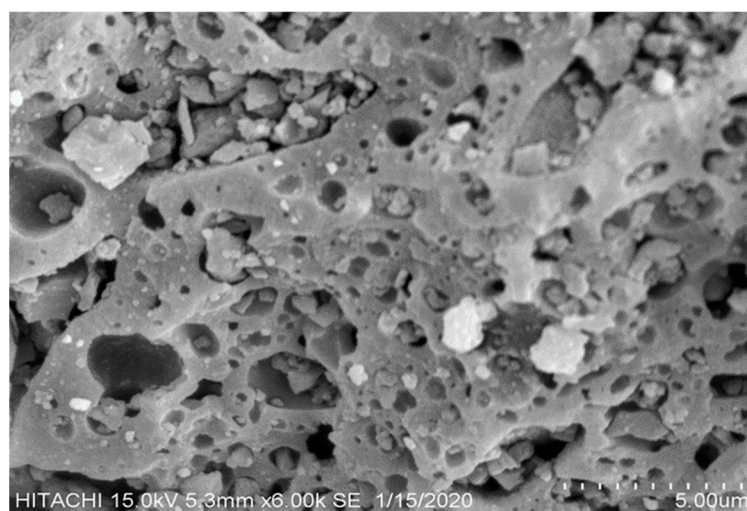


Figure 3. SEM micrograph of tailing ash.

3.1.3. BET Analysis Results

Table 2 shows the results of the BET analysis. The surface areas of three samples were found to be 3.5420 m²/g for tailing ash, 4.0471 m²/g for tailing ash pretreated H₂O₂, and 3.2220 m²/g for thermal tailing ash. Moreover, activating the tailing ash with H₂O₂ caused an increase in the surface area. The larger surface area of H₂O₂ tailing ash will give an improved and effective contact area for adsorption. Figure 4 shows the BET nitrogen isotherm for the tailing ash, tailing ash pretreated H₂O₂, and thermal tailing ash. This result shows that the isotherms displayed the presence of a narrow hysteresis loop, which is a characteristic assigned to type IV isotherms [10].

Table 2. Results of BET analysis.

Sample	Surface Area (m ² /g)	Pore Volume (cm ³ /g)	Pore Size (nm)
Tailing ash	3.5420	0.078078	38.5800
Tailing ash pretreated with H ₂ O ₂	4.0471	0.098927	55.899
Thermal tailing ash	3.2220	0.096678	60.0112

3.2. Adsorption Study

3.2.1. Effect of pH and Determination of pH Point of Zero Charge (pH_{pzc}) of Tailing Ash

The pH effect on the adsorption of methylene blue is one of the important factors of controlling the adsorption of dyes. Figure 5 shows the effect of pH on MB removal. The uptake of dyes increased with the increase in the pH, achieving about 89.9% removal at pH 10. This indicated that the more alkaline the solution, the more methylene blue was adsorbed. From Figure 2, it was observed that the adsorption capacity q_e increased from 0.9 mg/g to 1.2 mg/g, with the increasing pH value from 2 to 10. Similarly, a previous study reported that the adsorption capacity of dye increased with the increase in the initial

pH [11]. When the pH of the solution is increased, the number of negatively charged sites in the adsorbent increases, while the number of positively charged sites decreases. Because of electrostatic forces, negatively charged surface areas on the adsorbent can promote cationic dye adsorption [12]. In the lower pH range, the low adsorption of methylene blue also exhibited the potential for the growth of a neutral or weakened charge at the porous biochar surface, which decreased the electrostatic motivation for the methylene blue adsorption onto it [13]. Hence, all of the following studies were conducted at pH 10.0 as the optimal pH.

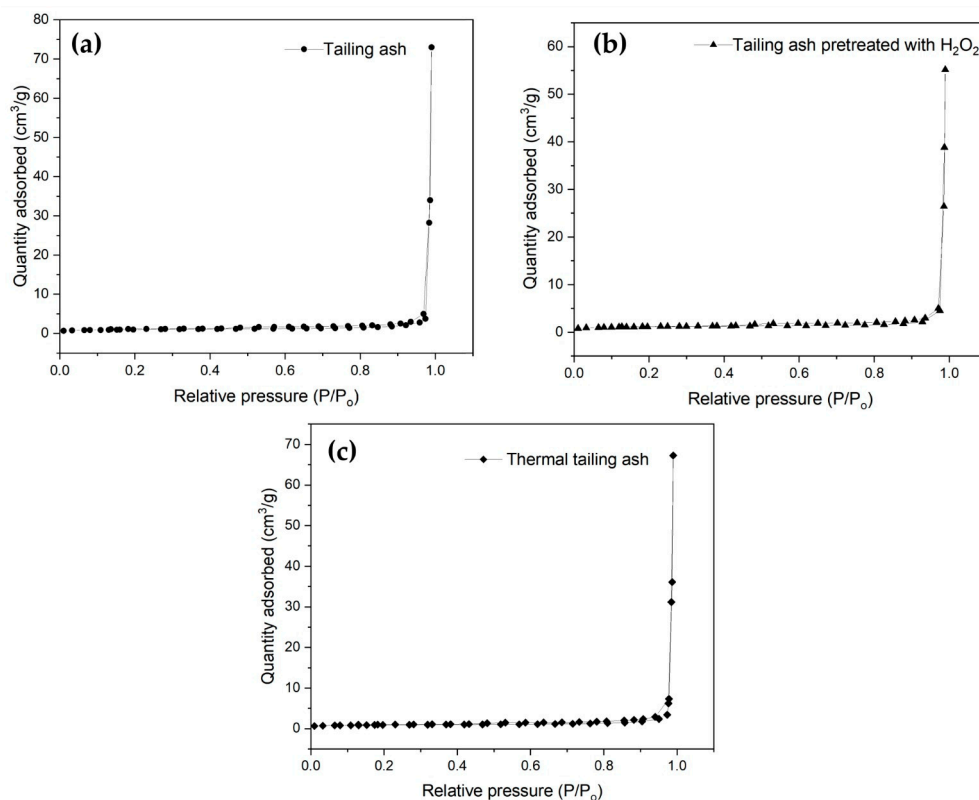


Figure 4. BET nitrogen isotherm plot for (a) tailing ash, (b) tailing ash pretreated with H₂O₂, and (c) thermal tailing ash.

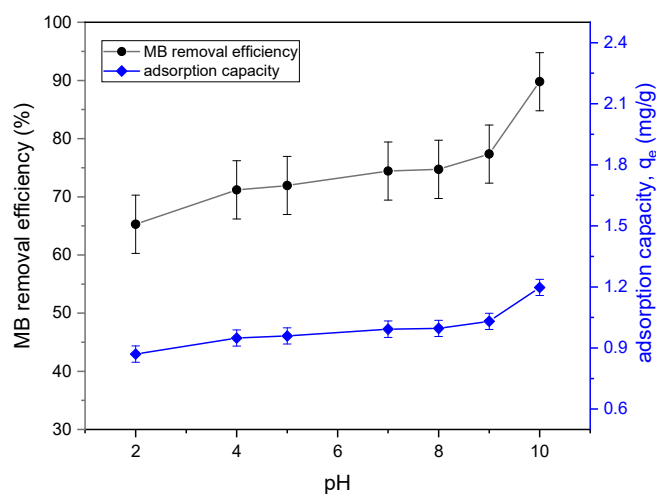


Figure 5. Effect of pH on the removal efficiency and q_e of MB adsorption onto tailing ash (initial MB concentration = 20 mg/L, adsorbent dosage = 1.5 g, stirring speed = 150 rpm, contact time = 120 min, RT (25 °C)).

When the charge in the adsorbent surface is zero, the pH is known as pHPzc. The pHPzc of tailing ash has been deduced from figures where the initial pH is equal to the final pH (intersection of curves). From Figure 6, it can be seen that the pHPzc of the tailing ash was 7.7. At the pH of 7.7, the surface becomes positively charged (+ve), while at a pH greater than 7.7, it becomes negatively charged (−ve). The literature reported that the cations uptake is favorable to a pH > pHPzc, whereas the uptake of anions is encouraged to a pH < pHPzc of sorbent [14].

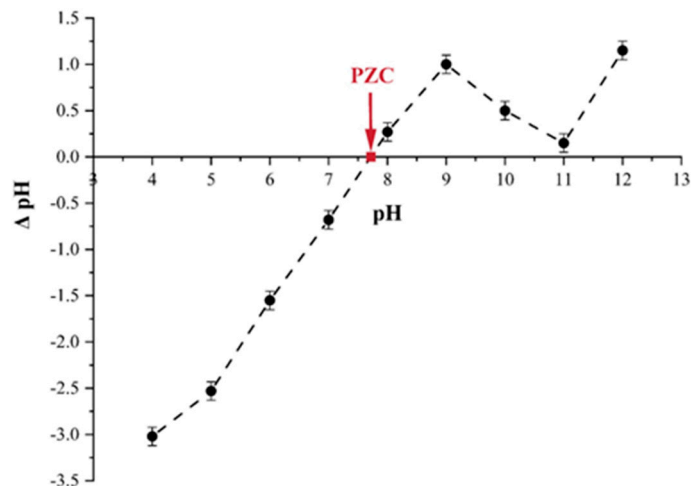


Figure 6. Determination of pH point of zero charge (pHPzc) of tailing ash.

3.2.2. Effect of Stirring Speed

Figure 7 shows the effect of stirring speed on MB removal. A stirring speed from 50 to 150 rpm was applied for this study. It was revealed that an increase in the stirring speed from 50 to 150 rpm resulted in an increase in the MB removal efficiency (76.24%) and q_e (1.01 mg/g). The thickness of the adsorbent boundary layer tended to decrease due to an increase in the speed of agitation of the solution [15]. The highest adsorption capacity (q_e) was about 0.999 mg/g at 150 rpm.

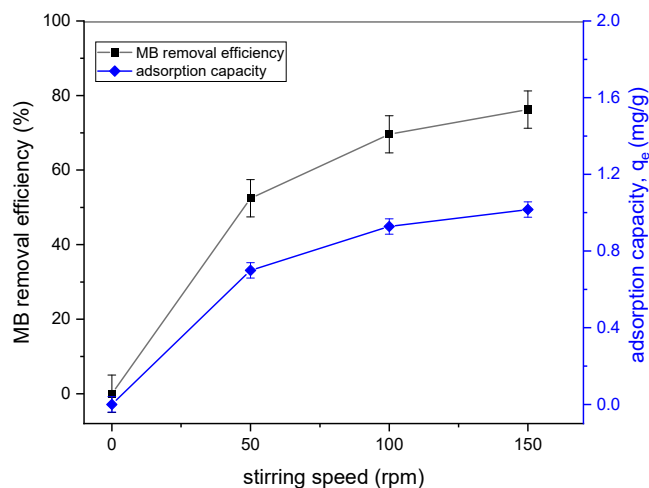


Figure 7. Effect of stirring speed on the removal efficiency and q_e of MB adsorption onto tailing ash (initial MB concentration = 20 mg/L, adsorbent dosage = 1.5 g, contact time = 120 min, pH = 10, RT (25 °C)).

3.2.3. Effect of Initial Dye Concentration and Contact Time

Figure 8a illustrates the effect of initial dye concentration and contact time on MB removal using tailing ash. As can be observed, the MB removal efficiency dropped as

the initial concentration increased from 20 to 100 mg/L, resulting in a decrease in the percentage of the dye adsorbed from 74.82% to 49.6%. Within the first 15 min, over 60% removal of MB occurred. It also demonstrated that increasing the contact duration resulted in a significant increase in the dye adsorbed until equilibrium (75 min contact time) for all initial concentrations ranging from 20 to 100 mg/L. The initial fast adsorption or uptake rate was due to the increased number of vacant sites available for adsorption at the initial stage [16]. Figure 8b shows the adsorption capacity, q_e , of MB at various initial concentration values. The adsorption capacity was 0.99, 1.63, 2.25, 2.64, and 3.48 mg/g. It is clearly seen that the adsorption capacity increased with the initial concentrations of MB.

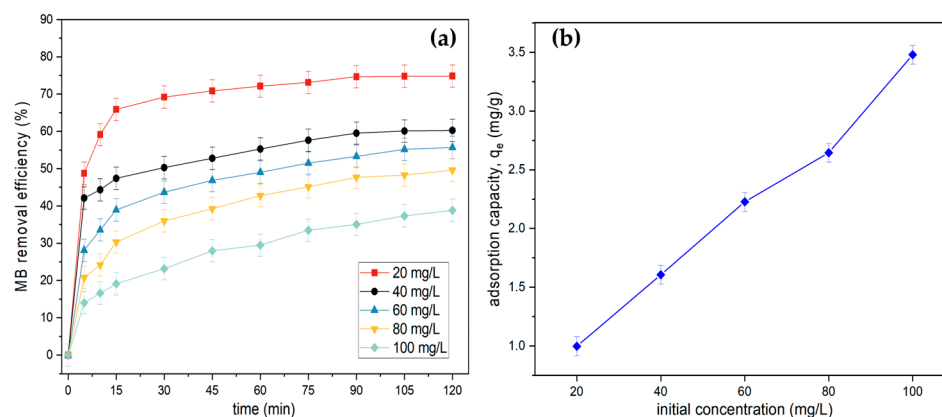


Figure 8. (a) Effect of contact time and initial MB concentration and on MB adsorption onto tailing ash (initial MB concentration = 20 mg/L, adsorbent dosage = 1.5 g, stirring speed = 150 rpm, contact time = 120 min, pH = 10, RT). (b) Effect of initial MB concentration.

3.2.4. Effect of Adsorbent Dosage

The effect of adsorbent dosage for MB removal was studied to determine the most appropriate amount of adsorbent at various MB concentrations. The investigation was carried out by varying the amount of tailing ash from 0.5 g to 2.5 g. The result is presented in Figure 9. This study found that when the amount of adsorbent was increased, the removal efficiency increased. The dye uptakes with tailing ash increased excessively from 1 g to 1.5 g, which is from 65.8% to 84.7%. It could also be noticed that q_e increased with an increase in the adsorbent dose until the optimum dose of 1.5 g and remained almost constant even with an increase in the adsorbent dosage. This suggested that for dye adsorption, an appropriate adsorbent should be used to lower the adsorbent cost. Additionally, the higher adsorbent dose provided more adsorption sites for the adsorbate, but it was commonly found that, when the adsorbent concentration was too high, some adsorption sites may be blocked by spatial or physical hindrance that can cause a decrease in the availability of some sorption sites [15].

3.2.5. Effect of Temperature

The effect of the initial adsorbate concentration on temperature for MB removal efficiency was investigated at temperatures of 25 °C, 35 °C, and 45 °C at initial concentration ranges from 20 to 100 mg/L (Figure 10). The experiments were carried out with a fixed adsorbent dose of 1.5 g of tailing ash adsorbent at pH 10. The results indicated that the uptake of methylene blue was favored at high temperatures. Figure 10 shows that the uptake is 96% at low concentrations and the adsorption capacity increases with the increase in the concentration of the dye. These results also signify the good efficacy of the adsorbents towards MB. Adsorption may increase due to an increase in the rate of diffusion of the adsorbate molecules over the surface boundary layer and the presence of internal pores in the adsorbent particles [17].

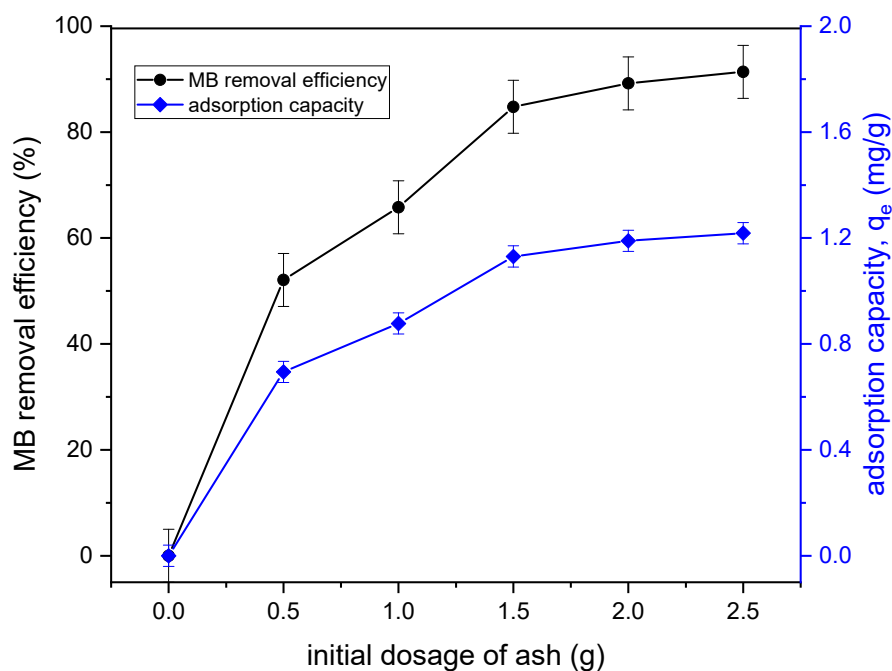


Figure 9. Effect of adsorbent dosage of TA on the removal efficiency and q_e of MB adsorption onto tailing ash (initial MB concentration = 20 mg/L, adsorbent dosage = 1.5 g, stirring speed = 150 rpm, contact time = 120 min, pH = 10, RT (25 °C)).

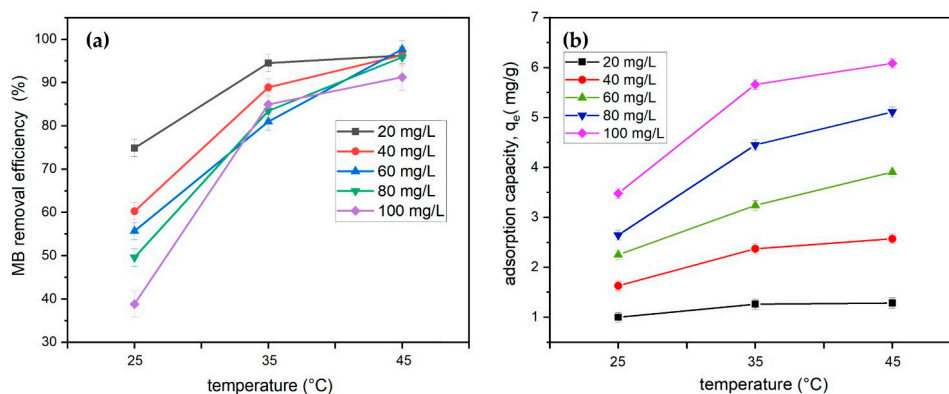


Figure 10. (a) Effect of temperature of TA on the removal efficiency and (b) q_e of MB adsorption onto tailing ash (initial MB concentration = 20 mg/L, adsorbent dosage = 1.5 g, stirring speed = 150 rpm, contact time = 120 min, pH = 10, 25–45 °C).

3.3. Modification of Adsorbent

Figure 11 shows the MB removal by thermal TA, TA, and TA pretreated with H_2O_2 . As we can see, the highest removal of 83.0% is promoted by TA pretreated with H_2O_2 compared with the separate tailing ash of 61.4% and thermal TA with 55.78% of removal. Involving H_2O_2 in the modification of the adsorbent can increase the number of surface active sites by providing it with a wider surface available for the adsorption [18]. Previous studies reported that acid treatment produced increased numbers of various surface oxygen complexes, which enhanced the active adsorbent sites [19].

According to Figure 12a, thermal TA and TA had a lower adsorption for MB dye when compared to TA pretreated with H_2O_2 . The small surface area and poor adsorption selection efficiency resulted in a low cationic MB adsorption capability. TA pretreated with H_2O_2 had the highest removal efficiency with 83.0% removal. The adsorption capacity of thermal TA, TA, and TA pretreated with H_2O_2 are presented in Figure 12b, in which TA pretreated with H_2O_2 gave a higher capacity (1.045 mg/g). In addition, the adsorption of

all tailing ash attained equilibrium between 90 and 120 min of contact. Since adsorption is a surface phenomenon, the higher adsorption rate was attributed to the greater accessibility to pores and the larger surface area [8].

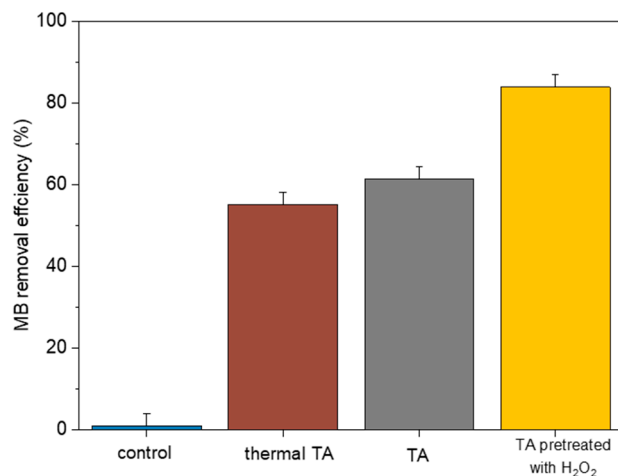


Figure 11. MB removal by thermal TA, TA, and TA pretreated with H₂O₂ (initial MB concentration = 20 mg/L, stirring speed = 150 rpm, contact time = 120 min, adsorbent dosage = 1.5 g, pH = 3, RT (25 °C)).

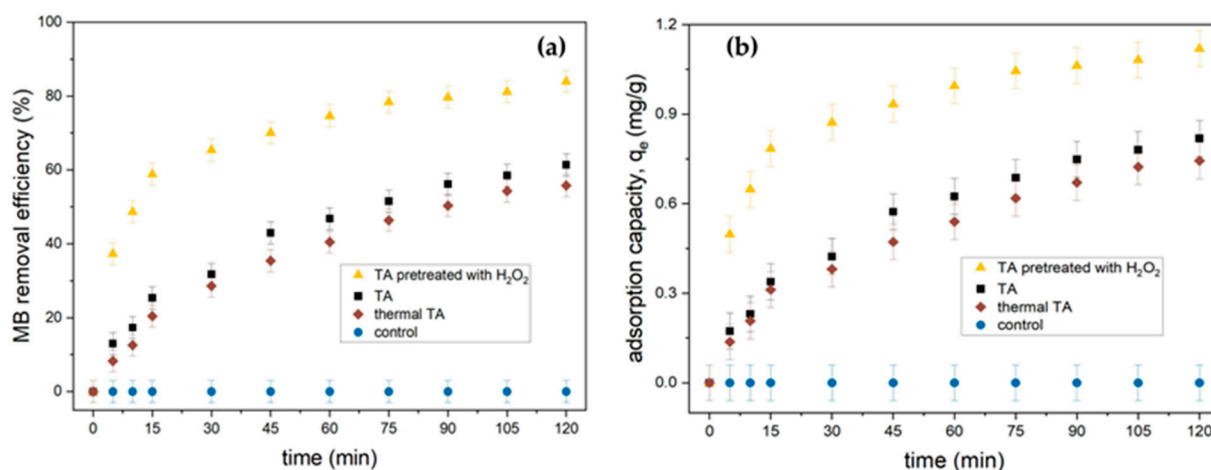


Figure 12. (a) Effect of contact time on MB removal by thermal TA, TA, and TA pretreated with H₂O₂ (initial MB concentration = 20 mg/L, adsorbent dosage = 1.5 g, stirring speed = 150 rpm, contact time = 120 min, pH = 3, RT). (b) Adsorption capacity, q_e , of thermal TA, TA, and TA pretreated with H₂O₂.

3.4. Functioning of H₂O₂

In order to clarify the potential combining effects of HTA on MB removal, the original tailing ash was employed for a comparative investigation with the involvement of hydrogen peroxide of different percentages. The result is shown in Figure 13. The graph shows the highest removal was obtained using 3% of H₂O₂ tailing ash (HTA). The results indicated that hydrogen peroxide involvement significantly promoted their removal efficiency to 74.18% compared with the separate tailing ash of 59.96% and separate hydrogen peroxide of 28.99%, respectively. It can be concluded that H₂O₂ can react as a catalyst to remove MB, which can help decompose the MB. Existing transition metals (shown in Table 1), such as Fe, Co, Ni, and Mn, in the biomass can trigger the Fenton-like reaction to release the hydroxyl radicals [20].

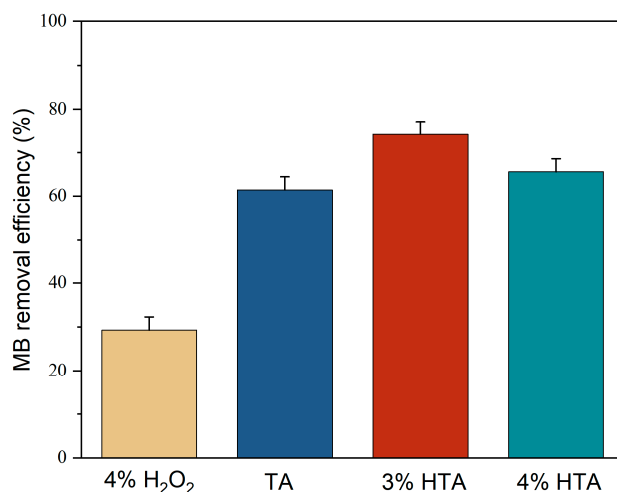


Figure 13. MB removal by H₂O₂, TA, and HTA (initial MB concentration = 20 mg/L, stirring speed = 150 rpm, contact time = 120 min, adsorbent dosage = 1.5 g, pH = 3, RT).

Effect of Contact Time by TA, H₂O₂, and HTA for MB Removal

Figure 14 shows the effect of contact time on MB removal by the three samples, namely, tailing ash (TA), hydrogen peroxide (H₂O₂), and tailing ash with hydrogen peroxide (HTA). In acidic conditions, tailing ash with hydrogen peroxide (HTA) has the greatest removal efficiency of 77.2% and adsorption capacity of 1.03 mg/g (Figure 15) when compared to tailing ash and H₂O₂ alone. The adsorption capacity of methylene blue by the tailing ash with hydrogen peroxide increased as the contact time increased, and then reached a maximum value. Tailing ash is a low-cost adsorbent that can react to remove the MB. It can be concluded that H₂O₂ can react as a catalyst to remove and help decompose the MB. Existing transition metals (shown in Table 1), such as Fe, Co, Ni, and Mn, in the biomass can trigger the Fenton-like reaction to release the hydroxyl radicals [20].

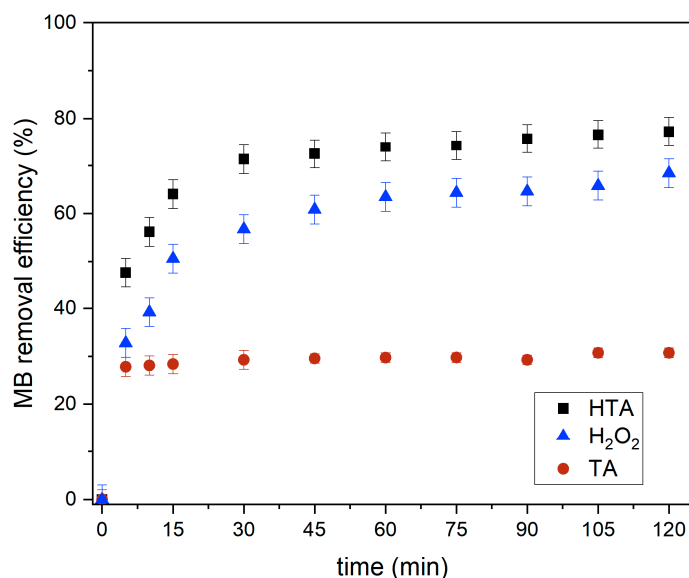


Figure 14. Effect of contact time on MB removal using TA, H₂O₂, and HTA (initial MB concentration = 20 mg/L, adsorbent dosage = 1.5 g, stirring speed = 150 rpm, contact time = 120 min, pH = 3, RT).

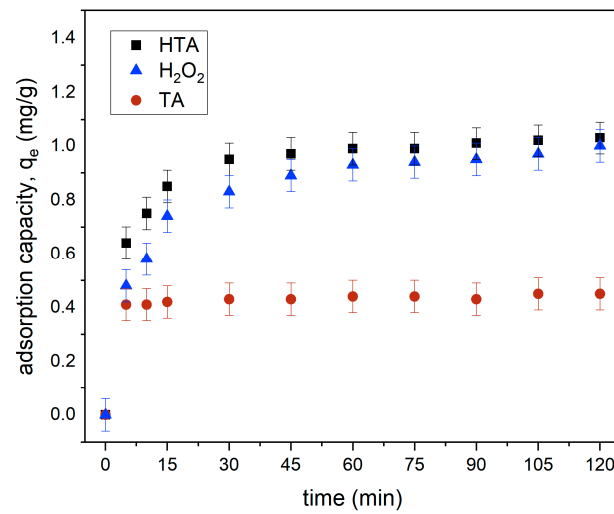


Figure 15. Effect of contact time on adsorption capacity (initial MB concentration = 20 mg/L, adsorbent dosage = 1.5 g, stirring speed = 150 rpm, contact time = 120 min, pH = 3, RT).

3.5. Adsorption Kinetics and Isotherm

3.5.1. Adsorption Kinetics

The reaction rate between the adsorbents and adsorbates and the factors affecting the reaction rate were studied using adsorption kinetics. A discussion of the results was made according to the fitting of the adsorption data by the kinetic models and the adsorption mechanism [11]. The consistency between the experimental results and the theoretical values of the model was evaluated on the basis of the coefficient of determination (the R^2 value was close to or equal to 1) [11].

The pseudo-first-order equation is:

$$\ln(q_e - q_t) = \ln q_e - k_1 t \tag{4}$$

where k_1 is the rate constant of adsorption (1/min), q_e is the quantity of dye adsorbed at equilibrium (mg/g), and q_t is the equilibrium concentration at various times t (in mg/g). The rate constant in this model was determined by the slope of the plot of $\ln(q_e - q_t)$ over time (t).

The pseudo-second-order equation is:

$$\frac{t}{q_t} = \frac{1}{k_2 q_e^2} + \frac{t}{q_e} \tag{5}$$

where k_2 is the second-order rate constant (g/mg/min) that can be determined for different MB concentrations according to the linear plots of t/q_t versus t , as shown in Figure 16b.

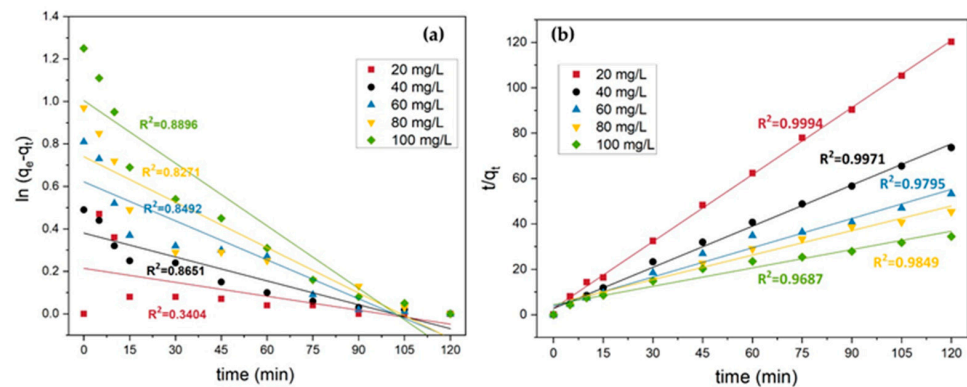


Figure 16. (a) Pseudo-first-order kinetic (initial MB concentration = 20 mg/L, adsorbent dosage = 1.5 g, stirring speed = 150 rpm, contact time = 120 min, pH = 10, RT). (b) Pseudo-second-order kinetic.

From Figure 16b, it was found that the pseudo-second-order model fitted better than the pseudo-first-order model (Figure 16a) to explain the adsorption process of MB on the tailing ash. The calculated correlation coefficients (R^2) were found to be close to 1 (0.099) and the experimental q_e that differ from the calculated ones are listed in Table 3.

Table 3. Pseudo-first-order model and pseudo-second-order model form.

C_0 (mg/L)	q_e (mg/g) Exp.	Pseudo-First-Order Model			Pseudo-Second-Order Model		
		k_1 (1/min)	q_e (mg/g) Cal.	R^2	k_2 (g/mg/min)	q_e (mg/g) Cal.	R^2
20	0.99	0.003	1.32	0.5548	0.077	1.03	0.9994
40	1.63	0.003	1.42	0.8796	0.027	1.68	0.9971
60	2.25	0.006	1.76	0.8574	0.007	2.41	0.9795
80	2.64	0.006	1.96	0.8339	0.006	2.78	0.9849
100	3.48	0.009	2.53	0.8999	0.002	3.94	0.9687

3.5.2. Adsorption Isotherm Study

The adsorption mechanisms of the tailing ash in the removal of the methylene blue dye solutions were analyzed using Langmuir, Freundlich, and Temkin adsorption isotherm models. It is important to establish the most appropriate correlation for the equilibrium curves to optimize the design of an adsorption system for the adsorption of adsorbates [21]. The equilibrium adsorption of methylene blue dye solutions by TA were used to determine the Langmuir, Freundlich, and Temkin isotherm models. The Langmuir, Freundlich, and Temkin adsorption isotherm can be written as follows:

$$\frac{C_e}{q_e} = \frac{1}{K_L q_{max}} + \frac{C_e}{q_{max}} \quad (6)$$

$$\ln(q_e) = \ln K_F + \left(\frac{1}{n}\right) \ln(C_e) \quad (7)$$

$$q_e = B \ln A + B \ln C_e \quad (8)$$

where K_L is the Langmuir adsorption constant (L/mg) related to the energy of adsorption and q_{max} is the Langmuir constants that are related to the adsorption capacity (mg/g); K_F is the Freundlich constant (L/mg) and $1/n$ is the heterogeneity factor; B is a constant related to the heat of adsorption and is defined by the expression $B = RT/b$; b is the Temkin constant (J/mol); T is the absolute temperature (K); R is the gas constant (8.314 J/mol K); and A is the Temkin isotherm constant (L/g). The Langmuir isotherm model determines the adsorption of ions on the surface of the adsorbent on the monolayer and specific homogeneous surface [14,17]. The Freundlich isotherm model assumes that multi-layer adsorption processes occur on heterogeneous surfaces. The Temkin isotherm model assumes that the adsorption heat of all molecules decreases linearly with the increase in the coverage of the adsorbent surface, and that adsorption is characterized by a uniform distribution of binding energies, up to maximum binding energy [22,23].

Figure 17a–c show the Langmuir (C_e/q_e versus C_e) plot, Freundlich ($\ln q_e$ versus $\ln C_e$), and Temkin ($\ln C_e$ versus q_e), respectively, for the removal of MB with TA. The high value of R^2 obtained from the linear graph of $\ln q_e$ versus $\ln C_e$ was 0.9934, which demonstrated that the adsorption process meets the Freundlich isotherm model, as shown in Figure 12b. Tailing ash is made up of heterogeneous, multi-layered surfaces, which are available for adsorption, as demonstrated by the Freundlich isotherm, the governing equilibrium model [8]. The obtained parameters for each model are summarized in Table 4.

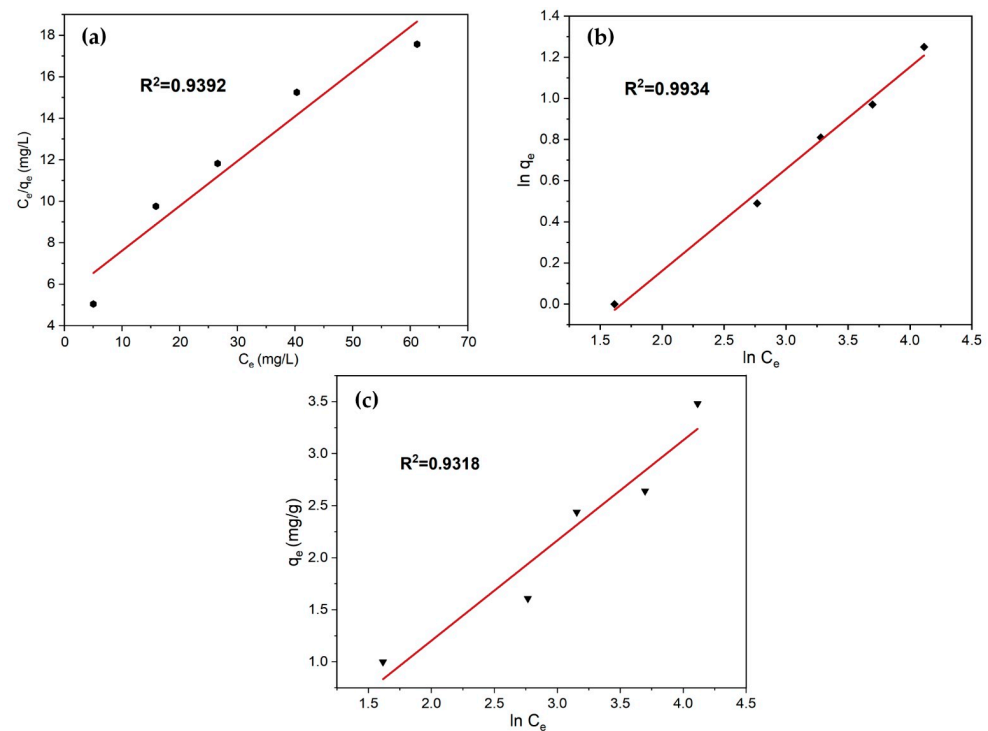


Figure 17. (a) Langmuir, (b) Freundlich, and (c) Temkin isotherm plots for adsorption of MB on tailing ash.

Table 4. Isotherm parameters of the Langmuir, Freundlich, and Temkin models.

Model	Isotherm Parameters	R ²
Langmuir	$q_{max} = 4.63$ mg/g $K_L = 0.183$ L/mg	0.9392
Freundlich	$K_f = 0.44$ mg/g $1/n = 0.496$	0.9934
Temkin	$B = 0.73$ $b = -3.4$ kJ/mol $A = 1.24$ L/g	0.9845

The adsorption data were also analyzed according to the nonlinear form of the Langmuir isotherm, as shown in Figure 18. In all cases, all error values for any of the parameter sets are lower than the same errors determined for the linear form of the isotherm. The comparatively lower magnitudes of the error values together with the lower range of variation in the isotherm parameters [24] suggests that the Langmuir isotherm does provide a good model for the adsorption of MB onto tailing ash.

3.5.3. Thermodynamic Parameters

The thermodynamic parameters were verified using the data from the adsorption isotherms. The changes in standard free energy (ΔG°), enthalpy (ΔH°), and entropy (ΔS°) of adsorption for methylene blue were calculated. The values are given in Table 5. The negative free energy value indicates the feasibility of the process and spontaneous process nature of adsorption. Moreover, the result showed that by increasing the adsorption temperature, the ΔG° values gradually decreased. This phenomenon reveals that the adsorption process is more favorable at high temperatures. The negative enthalpy value implies that the process is an exothermic removal of energy from the reaction [25]. The values of ΔH° and ΔS° can be determined from the slopes and the intercepts of the linear graph of $\ln(K_L)$ versus $1/T$, as shown in Figure 19.

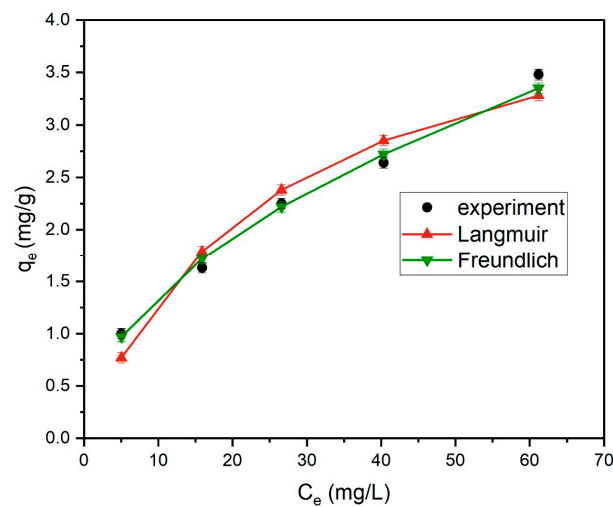


Figure 18. Nonlinear regression fitting of Langmuir and Freundlich isotherms of MB adsorption by tailing ash.

Table 5. Thermodynamic parameters for adsorption of MB by tailing ash at different temperatures.

ΔH° KJ/mol	ΔS° KJ/(K mol)	ΔG° KJ/mol		
		298	308	318
−0.4555	−128.226	−7.5403	−11.9745	−16.6550

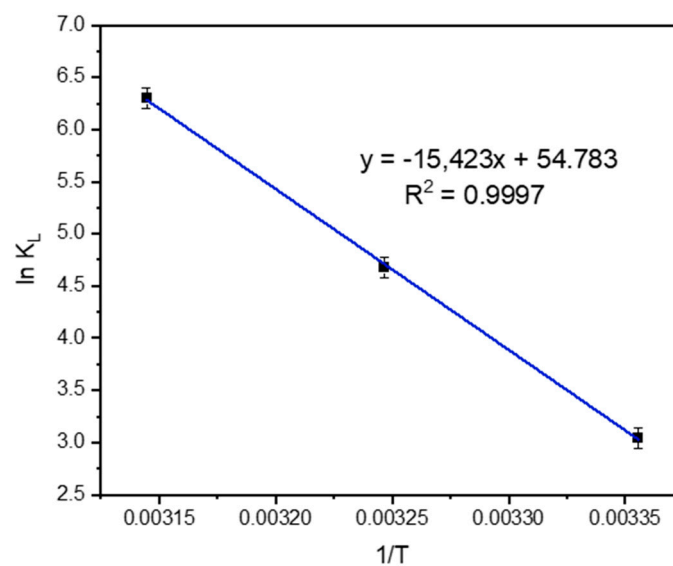


Figure 19. Van't Hoff plot for adsorption of MB by tailing ash.

Table 6 compares the adsorption capacity, q_e (mg/g), of MB on different adsorbents. As with the data reported in the literature, the adsorption capacity of the MB on ash obtained in this study is rather low [26]. The MB is a cationic dye that produces positively charged ions when dissolved in water, and the positive surface charge of the adsorbent tends to oppose the adsorption of cationic species, leading to low adsorption capacity [27]. The adsorption capacity could be enhanced via surface modifications or extracting adsorptive material from waste material [27,28]. In the future, we plan to synthesize synthetic zeolite from coal bottom ash for the more effective removal of MB [29].

Table 6. Comparison of low-cost adsorbents for MB.

Low-Cost Adsorbent	MB Removal, %	Q_{max} (mg/g)	pH	Ref.
Tailing ash	96.23	6.08	10	(this study)
Fly ash (modified with alkali)	97.11	28.65	7	[30]
Activated carbon (Cola nuts shell)	90	87.37	3.5	[31]
Orange peel	98.76	98	2	[14]
High-lime fly ash	96.99	6.06	9–10	[26]
Heat-treated gnetum gneumon shell	95.80	14.37	6	[32]
Mesoporous silica nanoparticles	95	31	7	[28]
Magnetic mesoporous silica	96.35	208.31	10	[27]

4. Conclusions

The present study showed that tailing ash can be used as an adsorbent for the removal of methylene blue from aqueous solutions. Tailing ash is a more cost-effective adsorbent than commercially available adsorbents. The tailing ash was derived from the floatation of bottom ash, which is a freely available waste material with no additional cost and is usually dumped in landfill areas. The adsorption of methylene blue onto tailing ash adsorbents was conducted under several experimental parameters such as pH, stirring speed, adsorbent dosage, initial dye concentration, contact time, and temperature. The adsorbents were characterized using XRF, SEM, and BET. The SEM image shows that the adsorbents consist of porous particles. The XRF results show that the adsorbent consists mainly of SiO_2 , Al_2O_3 , and Fe_2O_3 . The experimental results for batch adsorption showed that up to 96.23% MB removal was achieved under optimum conditions (pH = 10, initial adsorbent dosage = 1.5 g, 150 rpm, contact time = 120 min, 45 °C). The kinetic modeling study showed that the experimental data followed the pseudo-second-order model, and for isotherms, the data followed the Freundlich model with correlation coefficient values (R^2) equal to 0.993. This study demonstrated that tailing ash can be used as an excellent adsorbent and the developed method is quite inexpensive.

Author Contributions: Conceptualization, T.S.Y.C.; methodology, T.S.Y.C. and S.N.A.M.J.; validation, T.S.Y.C., W.A.W.A.K.G., F.N.A.A.A. and S.N.A.M.J.; formal analysis, T.S.Y.C., C.J.F.b.Y. and F.L.; investigation, C.J.F.b.Y.; resources, C.J.F.b.Y.; data curation, C.J.F.b.Y.; writing—original draft preparation, C.J.F.b.Y.; writing—review and editing, T.S.Y.C. and F.L.; visualization, T.S.Y.C., C.J.F.b.Y. and F.L.; supervision, T.S.Y.C., W.A.W.A.K.G., F.N.A.A.A. and S.N.A.M.J.; funding acquisition, T.S.Y.C. All authors have read and agreed to the published version of the manuscript.

Funding: This research was funded by Universiti Putra Malaysia via the Graduate Research Fellowship program (GRF) (GS51339).

Data Availability Statement: The data presented in this study are available on demand from the corresponding author or the first author.

Acknowledgments: The authors would like to acknowledge Universiti Putra Malaysia for financial support via the Graduate Research Fellowship program (GRF), and TNB Janamanjung power plant for providing the coal bottom ash for this research.

Conflicts of Interest: The authors declare no conflict of interest.

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