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Generalized Distribution Feeder Switching with Fuzzy Indexing for Energy Saving

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Abstract: The objective of this study is to analyze feeder loss minimization and load balance under given constraints. Effective methods are required for feeder switching/reconfiguration. Feeder switching is a mixed-integer large-scale combinatorial problem for optimization, not easily solvable with classical optimization techniques, especially involving a great number of switches. This paper proposes a fuzzy indexing algorithm for feeder switching, with membership functions defined for switches such as thermometers or indices. The optimal switches can be determined through fuzzy index operations. With membership functions defined, the developed method used numerical operations for indices instead of the “set” operation or the min-max operations of traditional fuzzy algorithms. The optimization problem becomes a simple numeric calculation instead of a large-scale sorting problem and is much faster than most algorithms. It greatly reduces the computation time and enhances efficiency, which is suitable for either planning or operation purposes. Many algorithms were tested with three typical examples chosen for illustration, including the “optimal” results with an exhausted search. It shows that the proposed algorithm is very effective and can balance the load to reduce the loss and costs in obtaining the solution.

Keywords: network reconfiguration; fuzzy algorithm; load balance; membership functions



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1. Introduction

A distribution system covers a very wide area and a large number of feeders. For economic reasons, it is not feasible to monitor the entire network. With recent technology, automation/smart grid has gradually extended to the distribution area with more tools [1–3]. For distribution energy saving, distribution lines account for about 5% to 13% of the total power network losses [2,3]. Apart from this, load balance and loss reduction can yield a better voltage profile and are worthy problems for study [4–7].

The distribution system needs to meet the load growth as well as effective operation to ensure economics and security. In high load density areas with scarce land resources, feeders are often heavily loaded, which not only increases line losses, but also affects the operational efficiency and security. Feeder phase unbalances are another cause for line losses. A particular example is Taiwan, with over 300 thousand open-Y and open-delta distribution transformers which further worsen the situation. Heavy loaded feeders and unbalanced loads have a high need for reconfiguration among feeders.

Feeder switching not only solves the problem of inter-feeder load unbalance, but it is also a solution to the problem of phase imbalance; as a result, it solves transformer load management and terminal voltage problems. In addition, the optimal placement and control of the capacitor bank and voltage regulator can be integrated for reactive power compensation to further reduce loss.

The simplest way to reconfigure a feeder is the empirical search method, where the feasible switching combinations increase exponentially with the number of switches. Feeder switching is a large-scale mixed-integer combinatorial problem, not easily solvable

using classical methods, although many studies have previously investigated the topic. Heuristic search [3,4] proposed the idea of reducing the search space according to empirical rules provided by experts, usually in the form of an expert system. It could improve performance but has limits in reaching optimality. The transportation rule [3], similar to the linear programming method, modeled the problem in transportation mode to minimize costs. Since the line loss is nonlinear, it needs to go through the linearization process, and accuracy is poor. Optimal power flow [6–8] determines switches according to the analysis of optimal load flow with all switches closed. The section with the lowest current is chosen to open when constraints are met. The simplified load flow method [7] described the feeder reconfiguration problem with the model of integer programming, using two approximate methods for line loss. The accurate one took more time, and the simplified load flow was less accurate but with a better performance.

More recently, artificial intelligence (AI) has provided an option for dealing with the mixed-integer combinatorial optimization problem. However, AI needs to compromise due to poor performance in sorting. The genetic algorithm (GA) [9,10] was proposed, but the calculation time was long and increased exponentially with the increased complexity of the system. Simulated annealing (SA) [11–13] is a comprehensive random search method, where the convergent speed is slow and very often trapped in the local optimum. The selection of initial temperature is critical, with the need of an effective disturbance mechanism, or the method could fail [14,15].

In general, the heuristic search method has faster solution speed but not necessarily better accuracy. GA and SA are good for non-analytical problems but are also too slow. Moreover, most proposed studies were either single feeder or inter-feeder based, neglecting the fact that the impacts are from both sides. A district-based general algorithm considering both factors is apparently more helpful.

This paper proposes a fuzzy indexing algorithm for feeder switching with efficient rules to deal with a large number of switches [14–16]. It defines four membership functions to represent the characteristics of unbalanced distribution, such as thermometers or indices. Through fuzzy index operations, the optimal switches can be determined [17,18]. Although membership functions are defined, the proposed method uses numerical operations for indices instead of the “set” operation or the min-max operations of traditional fuzzy algorithms. The optimization problem becomes a simple numeric calculation instead of a large-scale sorting problem and is much faster. The load flow is executed once after finding the optimum switching (i,j), unlike other methods requiring load flow execution or heavy computation at every step. The effectiveness was compared with many methods. The “optimal” solution from an exhausted search, requiring large computation, and the del_P loss formula [2], laid the foundation for comparison. Three typical examples were used [2,7,8] to show the optimization process. Recent investigation shows methods involving estimation, solar panel, or circuit theory [19–22], while considering mixed-integer [23] or radiality constraints [24]. Mixed-integer and radiality were contemplated in this research; however, index operations are more efficient to simplify the process and reduce the sorting time and are simpler than the set operation on membership functions [25], as proposed by the author.

2. Fundamental Theory

According to [2], the estimation method of feeder switching makes the following assumptions:

1. The loss increment ΔP obtained by switching is a quadratic function of the equivalent load current in the corresponding power supply area;
2. The increase in loss ΔP is a convex function, so there is an optimal value I_{opt} to minimize ΔP , and this optimal value I_{opt} represents the optimal equivalent load current that can be transferred;

There are two more constraints respected in the feeder switching process:

3. All feeders are radially structured;

4. Closing of a tie switch should be followed by the opening of a sectionalized switch.

Figure 1 is a schematic diagram of a two-feeder system, where feeder A has m load points, and feeder B has n load points and is marked with heavy black dots. A tie switch (dash line) connects the two feeders. Other lines numbered 1, 2 and 3 are sectionalized switches. R_{Loop} is the impedance of the loop when connecting the two feeders. For the total load transfer I_{tot} from feeder B to A [2], the loss will increase by

$$\Delta P = 2\text{Re}[I_{tot}(E_m - E_n)^* + |I_{tot}|^2(R_{Loop})]. \quad (1)$$

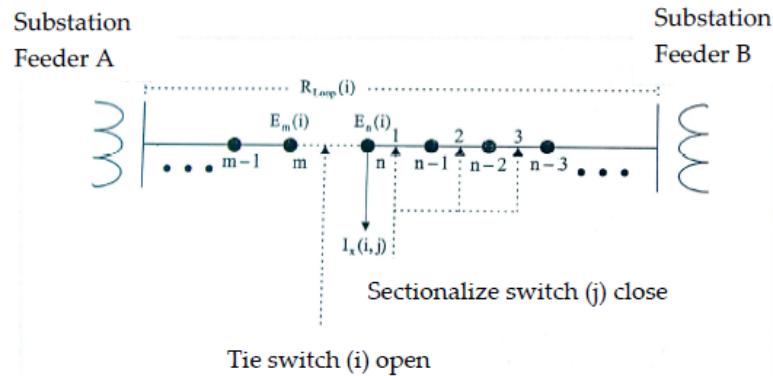


Figure 1. Schematic diagram of a two-feeder system.

Since $|I_{tot}|^2(R_{Loop})$ is always positive, $|E_m|$ should be less than $|E_n|$ to make ΔP negative, that is, needing a higher $|E_n|$ voltage. Reducing the feeder loss can be achieved by transferring the terminal with higher voltage to the terminal with lower voltage. Omitting the imaginary part, (1) becomes

$$\Delta P = 2I_{tot}(E_m - E_n) + |I_{tot}|^2(R_{Loop}) \quad (2)$$

Assuming that for feeder B, the distance from load point n to substation B is x , and the load current is distributed evenly along feeder B, (2) becomes

$$\Delta P = 2I(x)(E_m - E_n) + |I(x)|^2(R_{Loop}), \quad (3)$$

where $I(x)$ represents the total current transfer I_{tot} as a function of x , i.e., the point of load transfer. To obtain the most effective transfer current $I(x)$, differentiating ΔP with respect to $I(x)$, we have

$$\frac{d(\Delta P)}{dI(x)} = 2(E_m - E_n) + 2I(x)R_{Loop} = 0,$$

$$I(x) = I_{opt} = \frac{E_n - E_m}{R_{Loop}}, \quad E_n > E_m. \quad (4)$$

This formula indicates that there is an optimal load transfer current I_{opt} where the increase in loss ΔP is the lowest.

In Figure 2, vertical axis $I_{tot} = I_x$ is the total load transfer. The transfer loads are n and $n-1$ in Figure 1, i.e., opening section switch No. 2. The total current transfer is $I_2 = I_n + I_{n-1}$, and $\Delta 1$ is the current difference between I_2 and I_{opt} . Similarly, $\Delta 2$ is the current difference between $I_3 = I_n + I_{n-1} + I_{n-2}$ and I_{opt} by opening switch No. 3. Since $\Delta 1 < \Delta 2$ in Figure 2, current transfer by opening section switch No. 2 is a better choice.

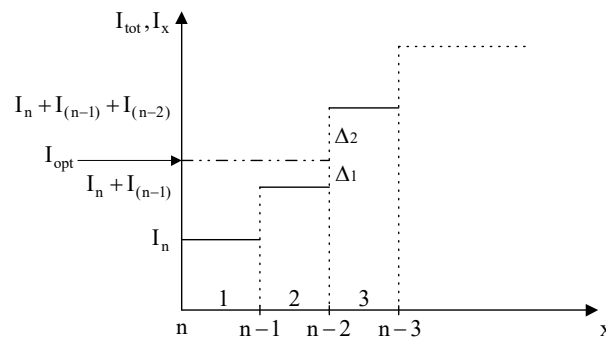


Figure 2. Optimal load transfer current.

3. The Fuzzy Index Feeder Switching

Feeder switching is the load redistribution by changing the status of tie switches and sectionalized switches [12,13]. The feasible switching combinations increase exponentially with the number of switches in the system. Formulation of the large-scale mixed-integer combinatorial problem makes it difficult to solve.

To analyze switching operations using fuzzy numerical calculation, two strategies were developed: the tie switch strategy and the sectionalized switch strategy. Combining both strategies can yield an overall strategy to choose the switches for operation.

3.1. Tie Switch Strategy

3.1.1. Large Loss to Small Loss

Define $P_L(r_i) = \frac{P_L(i_n)}{P_L(i_m)}$ = power loss ratio of two feeders connected by switch (i). That is, the power loss ratio $P_L(r_i)$ is defined for tie switch (i) connecting two feeder ends n and m, with both feeder losses compared, where

$P_L(i_n)$ is the light feeder loss;

$P_L(i_m)$ is the heavy feeder loss.

An associate membership function, $\tilde{\mu}_d$ is defined in (5) and called the “loss severity factor” for calculating the severity of tie switch (i) for transfer, as shown in Figure 3. The term $\tilde{\mu}_d$ is defined as

$$\tilde{\mu}_d(i) = e^{-\left[\frac{P_L(r_{max}) - P_L(r_i)}{P_L(r_{max})}\right]}, P_L(r_i) \leq P_L(r_{max}), \tag{5}$$

where $P_L(r_{max})$ is the maximum ratio of $P_L(r_i)$ among all tie switches $\{(i)\}$.

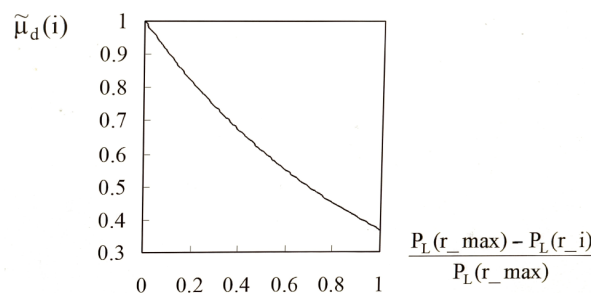


Figure 3. The loss severity factor $\tilde{\mu}_d(i)$.

3.1.2. High Voltage to Low Voltage

The higher the voltage drop ΔE across the tie switch, the more urgently the power transfer is required. A membership function $\tilde{\mu}_a$ is defined in (6) as the “voltage indication factor” to calculate the severity of voltage difference ΔE across the tie switch (i). Figure 4 indicates the urgency of needing a transfer. The term $\tilde{\mu}_a$ is defined by

$$\tilde{\mu}_a(i) = e^{-\left[\frac{\Delta E(\max) - \Delta E(i)}{\Delta E(\max)}\right]}, \Delta E(i) \leq \Delta E(\max), \tag{6}$$

where $\Delta E(i) = E_n(i) - E_m(i)$ is the voltage difference across both ends of tie switch (i).
 $E_n(i)$ is the end with higher voltage drop;
 $E_m(i)$ is the end with lower voltage drop;
 $\Delta E(\max)$ is the highest voltage drop among all tie switches $\{(i)\}$.

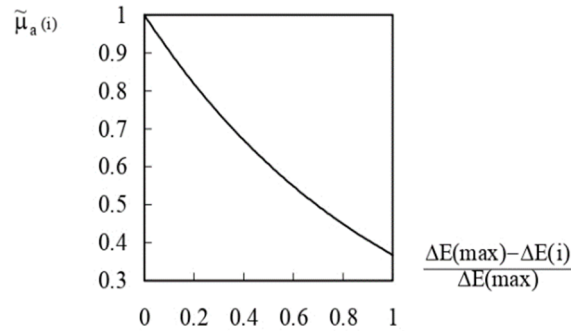


Figure 4. The voltage indication factor $\tilde{\mu}_a(i)$.

3.1.3. Determination of the Candidate Tie Switch

With the membership functions \tilde{u}_d and \tilde{u}_a , a “tie candidate index” membership $\tilde{u}_t(i)$ can be defined for each tie using

$$\tilde{u}_t(i) = \tilde{u}_a(i) \times \tilde{u}_d(i), \tag{7}$$

$$\tilde{u}_t(\max) : \max\{\tilde{u}_a(i) \times \tilde{u}_d(i)\}. \tag{8}$$

The term $\tilde{u}_t(i)$ shows the need of tie switch (i) to close: the larger the value, the more urgently the tie needs to be closed. The switch with the maximum $\tilde{u}_t(\max)$ is the candidate switch.

3.2. Sectionalized Switch Strategy

3.2.1. Calculation of Optimal Load

With tie switch (i) selected, the sectionalized switches need to be determined according to current I_{opt} . For a specific tie switch (i), a membership function $\tilde{u}_b(i, j)$ is defined for the load point (j) as the “optimal current transfer factor” to calculate the closeness of the load (j) transfer current to I_{opt} . With (i) given, Figure 5 shows the membership function $\tilde{u}_b(i, j)$ of load (j) defined by

$$\begin{aligned} \tilde{\mu}_b(i, j) &= e^{\left[\frac{I_x(i, j) - I_{opt}(i)}{I_{opt}(i)}\right]}, I_x(i, j) \leq I_{opt}(i), \\ &= e^{-\left[\frac{I_x(i, j) - I_{opt}(i)}{I_{opt}(i)}\right]}, I_x(i, j) \geq I_{opt}(i). \end{aligned} \tag{9}$$

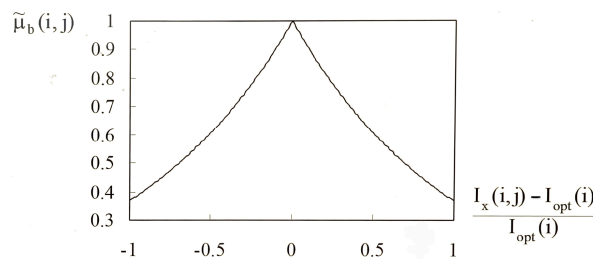


Figure 5. The optimal current transfer factor $\tilde{u}_b(I, j)$.

3.2.2. The Effect of Excessive Transfer

If the transferred current is greater than I_{opt} , i.e., transferring the feeder with low current to high current, a negative impact on reducing losses is caused. A membership function $\tilde{\mu}_c(i,j)$ is defined similar to $\tilde{\mu}_b(i,j)$ in Figure 6 for the “effect of excessive current switching” to forbid the move by

$$\tilde{\mu}_c(i,j) = e^{-w \left[\frac{I_x(i,j) - I_{opt}(i)}{I_{opt}(i)} \right]}, I_x(i,j) \geq I_{opt}(i), \quad (10)$$

where w is the weighting factor for “over-transfer cut-off control”, and $w = 3$ could generally forbid $I_x(i,j)$ from being greater than $I_{opt}(i)$, i.e., forbid the switching operation.

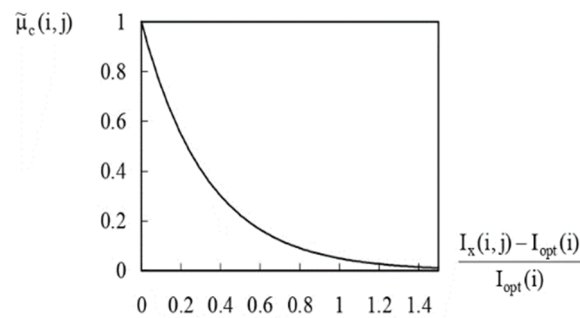


Figure 6. The effect of excessive current switching $\tilde{\mu}_c(i,j)$.

3.3. A Complete Switching Strategy

With all the membership functions defined, we can design the complete switching strategy using the simple value $\tilde{\mu}_s(i,j)$. That is, a simple rule for decision making with value $\tilde{\mu}_s(i,j)$ is calculated with operation (i,j) .

3.3.1. Transfer for Multiple Feeders

The decision making rules followed the operations below.

$$\text{If } I_x(i,j) \leq I_{opt}(i), \quad (11)$$

$$\tilde{\mu}_s(i,j) = \tilde{\mu}_a(i) \times \tilde{\mu}_b(i,j) \times \tilde{\mu}_d(i).$$

$$\text{If } I_x(i,j) \geq I_{opt}(i), \quad (12)$$

$$\tilde{\mu}_s(i,j) = \tilde{\mu}_a(i) \times \tilde{\mu}_b(i,j) \times \tilde{\mu}_c(i,j) \times \tilde{\mu}_d(i)$$

We have the decision rule as

$$\tilde{\mu}_s(\max) = \max \{ \tilde{\mu}_s(i,j) \}. \quad (13)$$

3.3.2. Transfer for Single Feeder

The decision making rules followed the operations below

$$\text{If } I_x(i,j) \leq I_{opt}(i), \quad (14)$$

$$\tilde{\mu}_s(i,j) = \tilde{\mu}_a(i) \times \tilde{\mu}_b(i,j).$$

$$\text{If } I_x(i,j) \geq I_{opt}(i), \quad (15)$$

$$\tilde{\mu}_s(i,j) = \tilde{\mu}_a(i) \times \tilde{\mu}_b(i,j) \times \tilde{\mu}_c(i,j).$$

We have the same decision rule as

$$\tilde{\mu}_s(\max) = \max \{ \tilde{\mu}_s(i,j) \}$$

Single feeder transfer can resolve uneven load distribution among branches and solve the voltage problem. We only need membership functions $\tilde{u}_a(i)$, $\tilde{u}_b(I_{ij})$ and $\tilde{u}_c(i,j)$. The largest value $\tilde{u}_s(\max)$ is the optimal switching solution, such as a multiple feeder.

4. A Layered Feeder Switching Scheme

After switching, a switch pair (i, j) will be found; it is called the solution in the first layer. That is, the remaining tie and sectionalized switch can be reconfigured again to further reduce the loss in a hierarchical or “layered” scheme. The system is re-evaluated to find the new switch pair in a second layer, thus neglecting the switches chosen in the earlier layer.

4.1. For Multiple Feeders

Step 1: Read system load flow data and compute

$$P_{\text{Loss}}(\text{feeder}), \Delta E(\text{tie}), I_x(\text{bus}), R_{\text{loop}}(\text{tie}), P_L(r_{\text{max}}), \Delta E(\text{max});$$

Step 2: For layer l , search for the tie switch (i) with (8);

Step 3: Find a sectionalized switch with (11) or (12);

Step 4: Find complete switching strategy with (13);

Feeder reconfiguration using the optimal sequence (i,j) and

Step 5: Execute the load flow program.

If the reconfigured feeder loss is higher, go to the next layer, i.e., $l = l + 1$ go to step 2.

Step 6: Repeat until the remaining tie switches are 0.

The load flow is executed for validation after the optimum operation (i,j) . It is a great advantage compared with other methods requiring load flow execution or heavy computation at every step.

4.2. For a Single Feeder

Modifying Step 3 using Equation (14) or (15), we get a reconfiguration scheme for a single feeder.

5. Test Results and Discussion

To show the effectiveness of the proposed algorithm, various systems were tested and compared. Three popular examples were used to show the effectiveness. For multiple feeders, two methods were used for comparison:

1. The exhausted search enumeration:

Load flow is executed to evaluate each switching pair (i,j) . It guarantees the optimal solution at the cost of large computational resources. It is a very strong case;

2. del_P loss formula method [2]:

The ΔP change is estimated to evaluate each switching pair (i,j) , involving a lot of computation but is more efficient than running load flow. The one with the maximum loss reduction is the solution.

For single feeder reconfiguration, Baran [7] and Goswami [8] were algorithms used for comparison. Algorithms [7,8] have many factors to change and are interesting for comparison.

5.1. Multiple Feeder Transfer

5.1.1. Case 1: A Three-Feeder System

Figure 7 shows a network in [2] with 3 feeders, 13 load points, 3 tie switches (15, 21, 26) and 13 section switches.

In the first layer, $\tilde{u}_t(21) = 0.8088$ is the largest. Tie 21 is the switch to close, and we can calculate I_{opt} . Following the calculation, one switch of (16, 17, 22, 24) needs to open.

Figure 2 shows the evaluation process and switch 17 is chosen. A similar process follows in all the examples below; $\tilde{u}_s(21,17) = 0.4174$ is the largest. Therefore, we have a switch pair (21, 17) as the solution to the first layer. Similarly, $\tilde{u}_s(15, 19) = 0.423$ is the solution to the second layer. Since the third search can no longer reduce the loss, the optimal switching sequences stopped with (21, 17) and (15, 19).

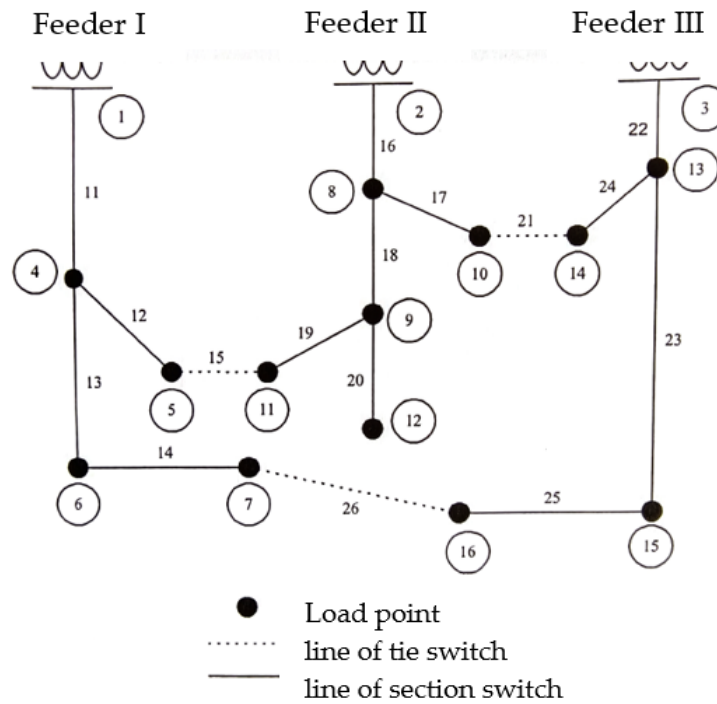


Figure 7. A three-feeder distribution system.

Figure 8 shows the tree path of the optimal solution, including the values of tie switches \tilde{u}_t and \tilde{u}_s for each path. The normally open switches become 17, 19 and 26. For this small system, so-called “optimal” results exist, which are verifiable using the exhausted search. For a large-scale network, we try to find the optimal or sub-optimal solution since there is no way to verify it. Table 1 shows the comparison charts where all three methods yield the same optimal results for this simple network. The proposed method works successfully, as well as the other two methods.

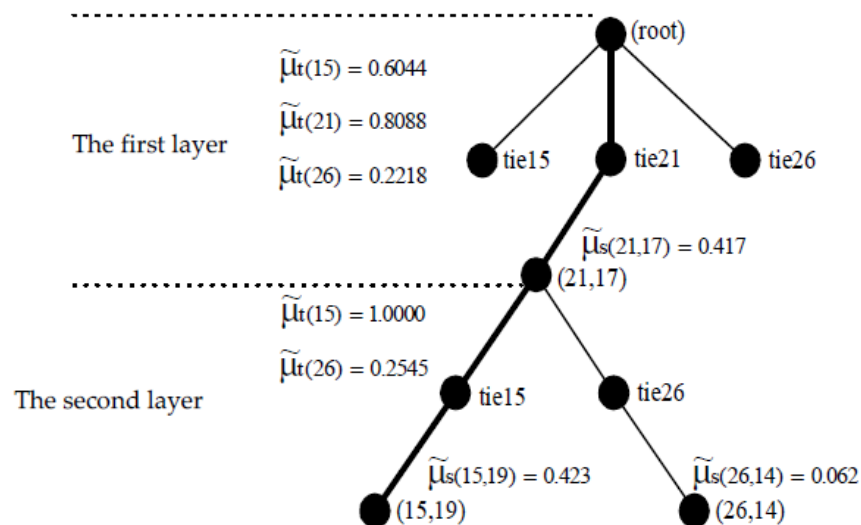


Figure 8. The layered switching process.

Table 1. Loss reduction for three-feeder network.

Layer	Optimal Switch Configuration			del_P Loss Formula			Fuzzy Index Algorithm		
	(on,off)	Loss (p.u)	Red (%)	(on,off)	Loss (p.u.)	Red (%)	(on,off)	Loss (p.u)	Red (%)
1	(21,17)	0.004839	5.400	(21,17)	0.004839	5.400	(21,17)	0.004839	5.400
2	(15,19)	0.004662	8.860	(15,19)	0.004662	8.860	(15,19)	0.004662	8.860

5.1.2. Case 2: Five Feeder System with 33 Switches

The system configuration of Case 2 can be visualized in Figure 9. There are 5 power sources, 23 load points, 10 tie switches and 23 section switches. Figure 10 shows the tree structure of the process. Each node in the figure represents a possible solution; the thick line represents the chosen path. The figure also shows values of the membership functions.

The simulation results are in Table 2. The first column has the original tie switch numbers. Other columns show tie switches after the reconfiguration with the associated method. It shows that the results obtained from the fuzzy indexing algorithm and the exhausted search are the same, i.e., the “optimal” solution has been found but not the del_P formula. Meanwhile, the fuzzy indexing algorithm used a simple numerical calculation instead of the heavy power flow computation of exhausted search at every stage, showing the effectiveness of the proposed method.

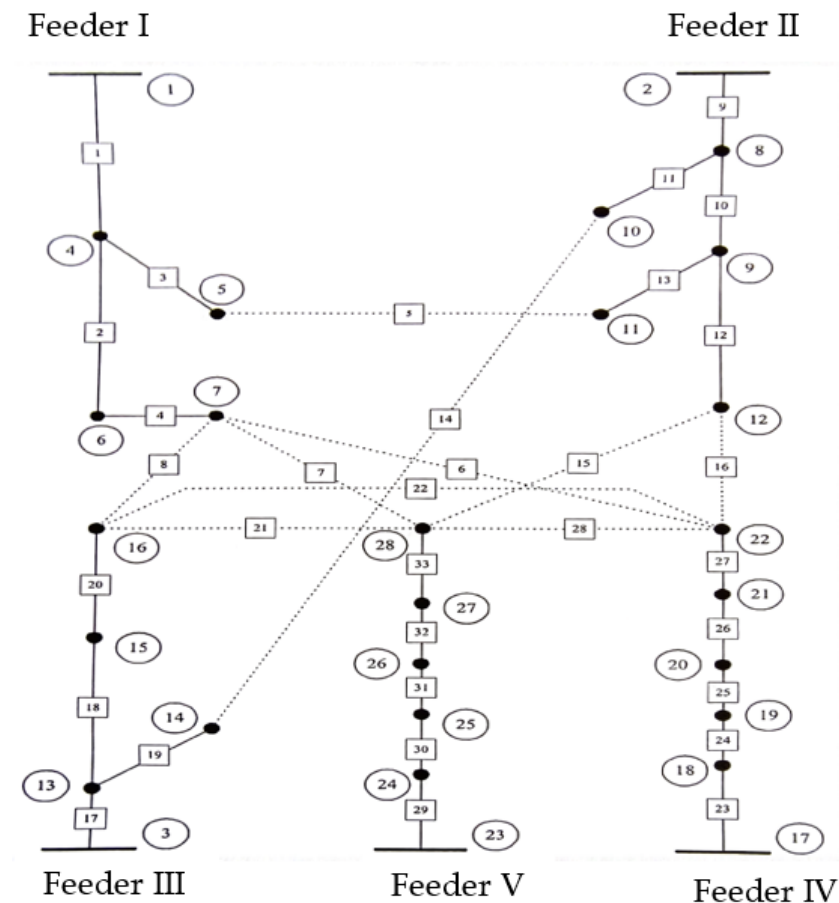


Figure 9. Five-feeder system with 33 switches.

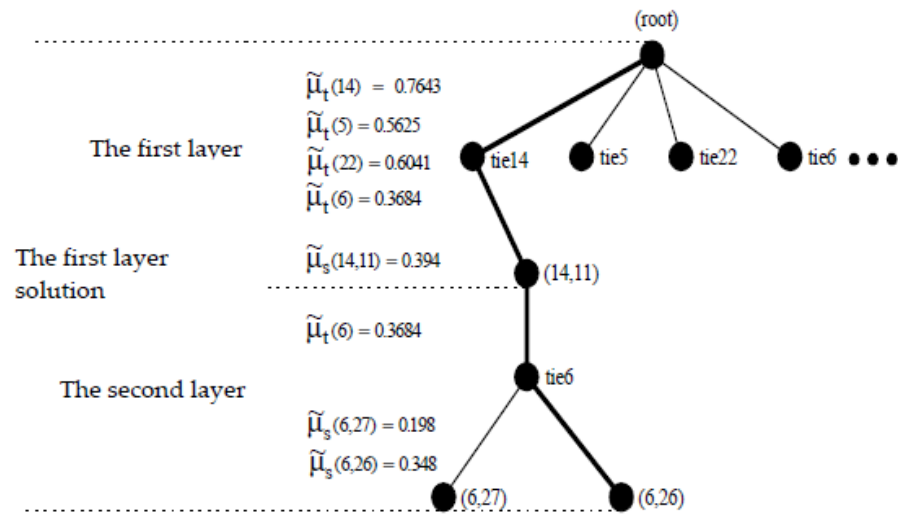


Figure 10. Tree structure of the five-feeder system.

Table 2. Simulation results of Example 2.

Original (Tie Switch)	Exhausted Search	del_p Formula	Fuzzy index Algorithm
5,6,7,8,14,15,16,21,22,28	5,7,8,11,15,16,21,22,26,28	6,7,8,13,14,15,16,21,26,28	5,7,8,11,15,16,21,22,26,28
Action switch	(14,11),(6,26)	(22,26),(5,13)	(14,11),(6,26)
Loss red. (p.u.)	0.000510 (p.u)	0.000504 (p.u)	0.000510 (p.u)
Reduction (%)	6.104%	6.032%	6.104%

For the optimal solution, the first switching pair (14,11) can reduce the loss by 3.303% and is the most significant, while the second switch pair (6,26) can reduce the loss by 2.801%. The total loss of the system can be reduced from 0.008355 to 0.007845 (p.u.), and the minimum voltage will be increased from 0.969 to 0.971 (p.u.). Figure 11 shows the change in loss per feeder before and after the reconfiguration.

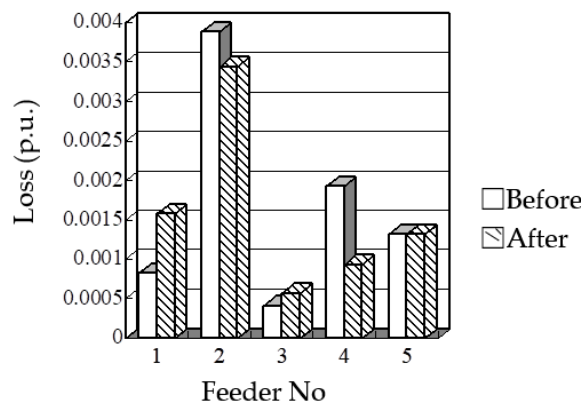


Figure 11. Loss change in each feeder.

5.2. Single Feeder Transfer

Single feeder switching can solve the uneven load distribution and the voltage problem. Feeder reconfiguration problems solved by Baran [7] and Goswami [8] had many forms and were interesting for comparison.

Table 3 also shows the loss reduction percentage for each switching. It shows that the first switching of the proposed method can reduce the loss by 22.77% and has the greatest effect on loss reduction. The “*” sign means no more switching needed.

Table 4 shows the tie switch numbers before and after the switching associated with each method, where the first column has the original tie switches for reference.

Table 4. Comparison chart of tie switch numbers.

Original Tie Switch	Goswami (I)	Goswami (II)	Goswami (III)	Baran. (I)	Baran. (II/III)	Fuzzy Index
33	7	7	7	11	6	7
34	9	9	9	28	11	9
35	14	14	14	31	31	14
36	32	32	32	33	34	32
37	37	37	37	34	37	37
Number of operations	7	7	4	5	3	5
Loss reduction (%)	31.148%	31.148%	31.148%	27.83%	23.83%	31.148%

In Table 4, Baran (II/III) has fewer switching operations but yields a higher loss. We can also see that the proposed method and Goswami I, II can reach the same reduction, but the proposed method requires fewer switching operations.

The loss reduction in every switching operation of the proposed method is also shown in Figure 13. After feeder reconfiguration, the minimum voltage of the system is also increased from 0.9131 (p.u.) of load point 18 to 0.9378 (p.u.) of load point 32.

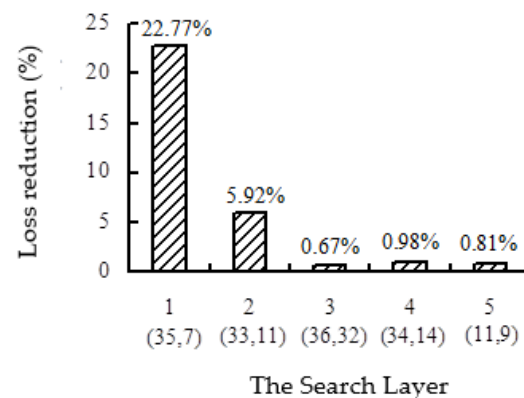


Figure 13. The loss reduction of each switching layer.

6. Conclusions

This paper proposes fuzzy index theory to solve the optimal switching problem and reduce loss. The fuzzy index algorithm used membership functions to simplify the computation, and the solutions were accurate and reliable. There are many advantages to the proposed method:

1. It deals with the large-scale mixed-integer combinatorial problem where conventional techniques would generally fail;
2. The fuzzy indexing simplifies the optimization process with easy numeric calculations instead of large-scale sorting or a large amount of computation;
3. It executes the load flow only once after finding the switch (i,j); this is a great advantage compared with other methods requiring heavy computation;

4. The solution quality is high. It shows that for a small system, the “optimal” results exist and are verifiable by exhausted search. However, for large-scale networks, the solution will be optimal or sub-optimal;
5. The method is suitable for real-time applications even for a large distribution system;
6. It is applicable to all feeder configurations, including the multiple-feeder and single-feeder systems;
7. It can get the best configuration with less switching operations and save on costs;
8. The first switching is the most significant to reduce the loss and balance the load;
9. Proper switching can solve the transformer load management and terminal voltage problems.

More constrains can be added, such as the line rating, voltage limits, and loading limits, together with capacitor banks or DGs for better compensation [21]. With the proposed simple algorithm and test results, the method is effective to implement for either operational or planning purposes.

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