

Review



### Topological Isomorphism of Liquid–Vapor, Fusibility, and Solubility Diagrams: Analogues of Gibbs–Konovalov and Gibbs–Roozeboom Laws for Solubility Diagrams

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Abstract: The comprehensive topological isomorphism of liquid–vapor, fusibility, and solubility diagrams in the proper sets of variables is proven with the aid of van der Waals equations of the shift in phase equilibrium. Analogues of Gibbs–Konovalov and Gibbs–Roozeboom laws are demonstrated in solubility diagrams of ternary and quaternary systems under crystallization of different types of solid solutions. For the demonstration, the quaternary reciprocal system  $K^+$ ,  $NH_4^+$ || $Cl^-$ ,  $Br^- - H_2O$  and its ternary subsystems with modeling of the liquid phase within the framework of the classical Pitzer formalism are mainly used. An algorithm for calculating solubility equilibria in these systems is given.

**Keywords:** phase diagram topological isomorphism; incomplete Gibbs potential metric; Gibbs–Konovalov laws; Gibbs–Roozeboom rules; reciprocal solid solutions; alyotrope

#### 1. Thermodynamics Backgrounds

1.1. Van der Waals Equation of the Shift in Phase Equilibrium in the Metric of Gibbs Potential

Let us consider an n-component heterogenium system and introduce the (n-1)-dimensional

vectors of compositions  $\overrightarrow{X}^{(i)} = (x_1^{(i)}, x_2^{(i)} \dots x_{n-1}^{(i)})$ , where  $x_j^{(i)}$  is mole fraction of the *j*-th component in the *i*-th phase.

Let us consider a heterogenium equilibrium between two phases,  $\alpha$  and  $\beta$ . The following parameters are independent variables of phase states in the metric of Gibbs potential: temperature, T; pressure, P; and mole numbers of components,  $n_i$  (or mole fractions). The ( $\alpha$ - $\beta$ ) equilibrium shift can be described by the following system of differential van der Waals equations in vector–matrix form in the variables of phase  $\alpha$  (Equation (1)) and phase  $\beta$  (Equation (2)), plus an additional equation (Equation (3)):

$$(\overset{\rightarrow}{X}^{(\alpha)} - \overset{\rightarrow}{X}^{(\beta)})\hat{G}^{(\alpha)}d\overset{\rightarrow}{X}^{(\alpha)} = S^{(\alpha \to \beta)}dT - V^{(\alpha \to \beta)}dP$$
(1)

$$(\overset{\rightarrow}{X}^{(\beta)} - \overset{\rightarrow}{X}^{(\alpha)})\hat{G}^{(\beta)}d\overset{\rightarrow}{X}^{(\beta)} = S^{(\beta \to \alpha)}dT - V^{(\beta \to \alpha)}dP$$
(2)

$$\hat{G}^{(\alpha)}d\overset{\rightarrow}{X}^{(\alpha)} + \nabla S^{(\alpha)}dT - \nabla V^{(\alpha)}dP = \hat{G}^{(\beta)}d\overset{\rightarrow}{X}^{(\beta)} + \nabla S^{(\beta)}dT - \nabla V^{(\beta)}dP \tag{3}$$

check for **updates** 

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**Copyright:** © 2023 by the authors. Licensee MDPI, Basel, Switzerland. This article is an open access article distributed under the terms and conditions of the Creative Commons Attribution (CC BY) license (https:// creativecommons.org/licenses/by/ 4.0/). where  $V^{(\tau)}$  and  $S^{(\tau)}$  are the molar volumes and entropies of the corresponding phase  $(\tau = \alpha \text{ or } \beta)$ ;  $\nabla V^{(\tau)}$  and  $\nabla S^{(\tau)}$  are the gradients of these properties with respect to concentration,  $(\partial V^{(\tau)} / \partial x_i^{(\tau)})_{T,P,x_k^{(\tau)} \neq x_{i,n}^{(\tau)}}$  and  $(\partial S^{(\tau)} / \partial x_i^{(\tau)})_{T,P,x_k^{(\tau)} \neq x_{i,n}^{(\tau)}})$ ;  $\overrightarrow{X}^{(\tau)}$  is a vector that characterizes the state of the figurative point of the phase  $\tau$  in the concentration space of system;  $d\overrightarrow{X}^{(\tau)}$  is a vector characterizing the displacement of  $\overrightarrow{X}^{(\tau)}$  according to displacement of the two-phase equilibrium;  $\widehat{G}^{(\tau)}$  is an operator corresponding to the matrix of the second derivatives  $G_{ij}^{(\tau)}$ :

$$G_{ij}^{(\tau)} = \left(\frac{\partial^2 G^{(\tau)}}{\partial x_i^{(\tau)} \partial x_j^{(\tau)}}\right)_{T,P,x_k^{(\tau)} \neq x_{i,n}^{(\tau)}}$$
(4)

where  $G^{(\tau)}$  is the molar Gibbs energy potential of the phase  $\tau$ . According to the phase stability criterion, the matrices of the  $\hat{G}^{(\tau)}$  operators and corresponding quadratic bilinear forms are nondegenerate. Additionally, according to the phase diffusion stability criterion, the matrices corresponding to the quadratic bilinear form  $\hat{G}^{(\tau)}$  are defined positively:

$$(d^{2}G^{(\tau)})_{T,P} = \sum_{i=1}^{n-1} \sum_{j=1}^{n-1} G_{ij}^{(\tau)} dx_{i}^{(\tau)} dx_{j}^{(\tau)} > 0$$
(5)

and according to Sylvester's criterion, the following system of determinants (minors of main diagonal) should be determined positively:

$$\begin{cases} \Delta_{n-1}^{(\tau)} = \begin{vmatrix} G_{1,1}^{(\tau)} & \cdots & G_{1,n-1}^{(\tau)} \\ \vdots & \ddots & \vdots \\ G_{n-1,1}^{(\tau)} & \cdots & G_{n-1,n-1}^{(\tau)} \end{vmatrix} > 0 \\ \Delta_{n-2}^{(\tau)} = \begin{vmatrix} G_{21}^{(\tau)} & \cdots & G_{2,n-2}^{(\tau)} \\ \vdots & \ddots & \vdots \\ G_{n-1,1}^{(\tau)} & \cdots & G_{n-1,n-2}^{(\tau)} \end{vmatrix} > 0 \\ & & & & \\ \Delta_{2}^{(\tau)} = \begin{vmatrix} G_{ii}^{(\tau)} & G_{ij}^{(\tau)} \\ G_{ji}^{(\tau)} & G_{jj}^{(\tau)} \end{vmatrix} > 0 \\ & & & & \\ \Delta_{1}^{(\tau)} = G_{ii}^{(\tau)} > 0 \end{cases}$$
(6)

The physical senses of parameters

$$S^{(\alpha \to \beta)} = [S^{(\beta)} - S^{(\alpha)} + (\overrightarrow{X}^{(\beta)} - \overrightarrow{X}^{(\alpha)})\nabla S^{(\alpha)}]$$

$$S^{(\beta \to \alpha)} = [S^{(\alpha)} - S^{(\beta)} + (\overrightarrow{X}^{(\alpha)} - \overrightarrow{X}^{(\beta)})\nabla S^{(\beta)}]$$

$$V^{(\alpha \to \beta)} = [V^{(\beta)} - V^{(\alpha)} + (\overrightarrow{X}^{(\beta)} - \overrightarrow{X}^{(\alpha)})\nabla V^{(\alpha)}]$$

$$V^{(\beta \to \alpha)} = [V^{(\alpha)} - V^{(\beta)} + (\overrightarrow{X}^{(\alpha)} - \overrightarrow{X}^{(\beta)})\nabla V^{(\beta)}]$$
(7)

are, correspondently, the entropy and volume changes in the process of the isothermal– isobaric formation of one mole of phase  $\beta$  from an infinitely large mass of phase  $\alpha$ , and vice versa.

# 1.2. Incomplete Gibbs Potential(s) and Van der Waals Equation of Phase Equilibrium Shift in Its Metric

Let us introduce the incomplete Gibbs potential (or Korjinskii's potential [1]) for an *n*-component system:

$$G^{[w]} = G - \mu_1 n_1 = \sum_{i=2}^n \mu_i n_i \tag{8}$$

where  $\mu_i$  and  $n_i$  are the chemical potential and mole number of the *i*-th component. Such potentials can be invented in many ways, but here, we will consider only the case when the first component is a solvent—water, for example—that is,  $n_1 = n_w$ .

Let us again consider an *n*-component heterogenium system and introduce the (n - 2)-dimensional vectors of compositions  $\overrightarrow{Y}^{(i)} = (y_1^{(i)}, y_2^{(i)} \dots y_{n-1}^{(i)})$ , where  $y_j^{(i)}$  is the mole fraction of the *j*-th component (in the *i*-th phase) in the concentration space reduced with respect to the mole number of the solvent. These are the Janecke indices of solutes:

$$y_i = n_i / \sum_{j=2}^n n_j \tag{9}$$

The following parameters are independent variables of phase states in the metric of incomplete Gibbs potential (8): temperature, T; pressure, P; Janecke indices,  $y_i$ ; chemical potential of solvent,  $\mu_w$ . Similar to the previous one, the ( $\alpha$ – $\beta$ ) equilibrium shift can be described by the following system of differential van der Waals equations in the vectormatrix form:

$$(\overset{\rightarrow}{Y}^{(\alpha)} - \overset{\rightarrow}{Y}^{(\beta)})\hat{G}^{[w](\alpha)}d\overset{\rightarrow}{Y}^{(\alpha)} = S^{[w](\alpha \to \beta)}dT - V^{[w](\alpha \to \beta)}dP + n_w^{[w](\alpha \to \beta)}d\mu_w$$
(10)

$$(\overset{\rightarrow}{Y}{}^{(\beta)}-\overset{\rightarrow}{Y}{}^{(\alpha)})\hat{G}^{[w](\beta)}d\overset{\rightarrow}{Y}{}^{(\beta)} = S^{[w](\beta\to\alpha)}dT - V^{[w](\beta\to\alpha)}dP + n_w^{[w](\beta\to\alpha)}d\mu_w$$
(11)

$$\hat{G}^{[w](\alpha)}d\overset{\rightarrow}{Y}^{(\alpha)} + \nabla S^{[w](\alpha)}dT - \nabla V^{[w](\alpha)}dP + \nabla n_w^{[w](\alpha)}d\mu_w =$$

$$\hat{G}^{[w](\beta)}d\overset{\rightarrow}{Y}^{(\beta)} + \nabla S^{[w](\beta)}dT - \nabla V^{[w](\beta)}dP + \nabla n_w^{[w](\beta)}d\mu_w$$
(12)

where  $V^{[w](\tau)}$ ,  $S^{[w](\tau)}$ , or  $n_w^{[w](\tau)}$  are the molar volume, entropies, or solvent mole number of phase  $\tau$ , which are calculated without taking into account the solvent (per mole solutes). Further,  $\nabla V^{[w](\tau)}$ ,  $\nabla S^{[w](\tau)}$ ,  $\nabla n_w^{[w](\tau)}$  are the gradients of these properties with reduced concentration,  $\left(\frac{\partial V^{[w](\tau)}}{\partial y_i^{(\tau)}}\right)_{T,P,y_k^{(\tau)}\neq y_{i,n-1}^{(\tau)},\mu_w^{(\tau)}}$ ,  $\left(\frac{\partial S^{[w](\tau)}}{\partial y_i^{(\tau)}}\right)_{T,P,y_k^{(\tau)}\neq y_{i,n-1}^{(\tau)},\mu_w^{(\tau)}$ ,  $\left(\frac{\partial S^{[w](\tau)}}{\partial y_i^{(\tau)}}\right)_{T,P,y_k^{(\tau)}\neq y_{i,n-1}^{(\tau)$ 

$$\left(n_{w}^{[w](\tau)}/\partial y_{i}^{(\tau)}\right)_{T,P,y_{k}^{(\tau)}\neq y_{i,n-1}^{(\tau)},\mu_{w}^{(\tau)}}, \text{ correspondently; } \overrightarrow{Y}^{(\tau)} \text{ is a vector, characterizing the state} \right)$$

of the figurative point of the phase  $\tau$  in the solvent-reduced concentration space;  $dY \xrightarrow{\to (\tau)} dY$ 

is a vector characterizing the displacement of  $\stackrel{\rightarrow}{Y}^{(\tau)}$  according to displacement of the two-phase equilibrium;  $\hat{G}^{[w](\tau)}$  is an operator, corresponding to the matrix of the second derivatives  $G_{ii}^{[w](\tau)}$ :

$$G_{ij}^{[w](\tau)} = \left(\frac{\partial^2 G^{[w](\tau)}}{\partial y_i^{(\tau)} \partial y_j^{(\tau)}}\right)_{T, P, y_k^{(\tau)} \neq y_{i, n-1}^{(\tau)}, \mu_w^{(\tau)}}$$
(13)

According to the phase stability criterion and Sylvester's criterion, the reduced analogues of expressions (5) and (6) remain valid:

$$\left(d^2 G^{[w](\tau)}\right)_{T,P,\mu_W} = \sum_{i=2}^{n-1} \sum_{j=2}^{n-1} G^{[w](\tau)}_{ij} dy_i^{(\tau)} dy_j^{(\tau)} > 0$$
(14)

$$\Delta_{n-2}^{[w](\tau)} = \begin{vmatrix} G_{1,1}^{[w](\tau)} & \cdots & G_{1,n-2}^{[w](\tau)} \\ \vdots & \ddots & \vdots \\ G_{n-2,1}^{[w](\tau)} & \cdots & G_{n-2,n-2}^{[w](\tau)} \\ A_{n-3}^{[w](\tau)} = \begin{vmatrix} G_{2,1}^{[w](\tau)} & \cdots & G_{2,n-2}^{[w](\tau)} \\ \vdots & \ddots & \vdots \\ G_{n-2,1}^{[w](\tau)} & \cdots & G_{n-2,n-2}^{[w](\tau)} \\ & \ddots \\ \Delta_{2}^{[w](\tau)} = \begin{vmatrix} G_{ii}^{[w](\tau)} & G_{ij}^{[w](\tau)} \\ G_{ji}^{[w](\tau)} & G_{jj}^{[w](\tau)} \\ G_{ji}^{[w](\tau)} & S_{ij}^{[w](\tau)} \end{vmatrix} > 0$$

$$\Delta_{1}^{[w](\tau)} = G_{ii}^{[w](\tau)} > 0$$
(15)

Parameters

$$S^{[w](\alpha \to \beta)} = [S^{[w](\beta)} - S^{[w](\alpha)} + (\overrightarrow{Y}^{(\beta)} - \overrightarrow{Y}^{(\alpha)}) \nabla S^{[w](\alpha)}]$$

$$S^{[w](\beta \to \alpha)} = [S^{[w](\alpha)} - S^{[w](\beta)} + (\overrightarrow{Y}^{(\alpha)} - \overrightarrow{Y}^{(\beta)}) \nabla S^{[w](\beta)}]$$

$$V^{[w](\alpha \to \beta)} = [V^{[w](\beta)} - V^{[w](\alpha)} + (\overrightarrow{Y}^{(\beta)} - \overrightarrow{Y}^{(\alpha)}) \nabla V^{[w](\alpha)}]$$

$$V^{[w](\beta \to \alpha)} = [V^{[w](\alpha)} - V^{[w](\beta)} + (\overrightarrow{Y}^{(\alpha)} - \overrightarrow{Y}^{(\beta)}) \nabla V^{[w](\beta)}]$$

$$n_{w}^{[w](\alpha \to \beta)} = [n_{w}^{[w](\beta)} - n_{w}^{[w](\alpha)} + (Y^{(\beta)} - Y^{(\alpha)}) \nabla n_{W}^{(W)(\alpha)}]$$

$$n_{w}^{[w](\beta \to \alpha)} = [n_{w}^{[w](\alpha)} - n_{w}^{[w](\beta)} + (Y^{(\alpha)} - Y^{(\beta)}) \nabla n_{W}^{(W)(\beta)}]$$
(16)

have the physical senses of entropy, volume, and change in solvent mole number in the isotherm–isobaric-solvent–isopotential process of formation of one mole of phase  $\beta$  from an infinitely large mass of phase  $\alpha$  and vice versa in the concentration space, reduced with respect to the mole number of the solvent.

For some additional details and references, see [2].

### 1.3. Isotherm–Isobaric Solubility Diagram of Ternary Systems. Analogues of Three Gibbs–Roozeboom Rules, Three Gibbs–Konovalov Laws

For fusibility diagrams of binary systems at P = const, the van der Waals Equations (1)–(3) have a very simple form, for example:

$$\left(x_1^{(s)} - x_1^{(l)}\right)\hat{G}_{1,1}^{(s)}dx^{(s)} = S^{(s \to l)}dT$$
(17)

where *s* and *l* denote solid and liquid phases, correspondently. Similarly, for liquid–vapor diagrams of binary systems, we have

$$\left(x_1^{(l)} - x_1^{(v)}\right)\hat{G}_{1,1}^{(l)}dx^{(l)} = S^{(l \to v)}dT \text{ (at } P = \text{const})$$
(18)

or

$$\left(x_{1}^{(l)} - x_{1}^{(v)}\right)\hat{G}_{1,1}^{(l)}dx^{(l)} = -V^{(l \to v)}dP \text{ (at } T = \text{const})$$
(19)

The van der Waals equation of the shift in solubility equilibrium (10)–(12) in the ternary system at T, P = const is as follows:

$$\left(y_1^{(s)} - y_1^{(l)}\right)\hat{G}_{1,1}^{[w](s)}dy_1^{(s)} = n_w^{[w](s \to l)}d\mu_w$$
<sup>(20)</sup>

Equations (17)–(20) in the appropriate variables are isostructural, being  $S^{(s \to l)} > 0$ ,  $S^{(l \to v)} > 0$ ,  $V^{(l \to v)} > 0$ , and  $n_w^{[w](s \to l)} > 0$ , according to physical sense; and  $\hat{G}_{1,1}^{(s)} > 0$ ,

 $\hat{G}_{11}^{(l)} > 0$  and  $\hat{G}_{1,1}^{[w](s)} > 0$ , according to the criterion of the stability. So, we can formulate analogues of three Gibbs–Roozeboom rules and three Gibbs–Konovalov laws.

First Rule (Law). Mathematically:

$$\left( dT/dx_{1}^{(l)} \right)_{P} > 0 \text{ if } x_{1}^{(s)} > x_{1}^{(l)}$$
 (21)

$$\left( \frac{dT}{dx_1^{(l)}} \right)_P > 0 \text{ and } \left( \frac{dP}{dx_1^{(l)}} \right)_T < 0 \text{ if } x_1^{(l)} > x_1^{(v)}$$
 (22)

In other words, (21): the melting temperature of solid solutions in binary systems at constant pressure increases as the content of the component whose content in the solid solution is higher than in the liquid phase increases; (22): in binary systems, the boiling temperature of solutions at constant pressure and constant temperature decreases as the content of the component whose content in the solution is higher than in the vapor increases.

Analogue:

$$(d\mu_w/dy_1^{(s)})_{T,P} > 0 \text{ if } y_1^{(s)} > y_1^{(l)}$$
 (23)

The chemical potential of the solvent (or its thermodynamic activity or partial pressure) at constant pressure and temperature in the ternary system increases as the reduced (calculated without taking into account the solvent) content in the solid solution of the component—whose solventless content in the solid solution is higher than in the liquid solution—increases.

These laws are not of a general nature, and are valid for multicomponent systems only in special cases, which we will discuss below.

Second Rule (Law).

$$\left( dT/dx_{1}^{(l)} \right)_{P} = 0 \text{ if } x_{1}^{(s)} = x_{1}^{(l)}$$
 (24)

$$\left(\frac{dT}{dx_1^{(l)}}\right)_P = 0 \text{ and } \left(\frac{dP}{dx_1^{(l)}}\right)_T = 0 \text{ if } x_1^{(l)} = x_1^{(v)}$$
 (25)

The melting temperature (of both solid solutions and constant composition phases) at constant pressure in a binary system passes through the extremum when the compositions of liquid and solid phases coincide.

When the liquid composition is coincident with the vapor composition, both the boiling point of the solution at constant pressure and its vapor pressure at constant temperature pass through an extremum (binary azeotrope).

$$\left(d\mu_{w}/dy_{1}^{(s)}\right)_{T,P} = 0 \text{ if } y_{1}^{(s)} = y_{1}^{(l)}$$
 (26)

The chemical potential of the solvent (or its thermodynamic activity or partial pressure) at constant pressure and temperature in the ternary system passes through the extremum when the composition of the liquid phase coinsides with the composition of the solid one in a solvent-free concentration space.

This rule (law) is absolutely general in nature, and is valid for systems with arbitrary numbers of components and any type of phases at equilibrium.

Moreover, at the equilibrium solid phase of constant composition (the formation of a congruently soluble compound on the solubility diagram or the formation of a congruently melting compound on the melting diagram), one can determine the type of extremum,  $(\mu_w)_{T,P}$  or  $(T)_P$ , respectively. It is always maximum. Indeed, let us differentiate, for example, Equation (1):

$$(\overset{\rightarrow}{X}^{(l)} - \overset{\rightarrow}{X}^{(s)})\hat{G}^{(l)}d\overset{\rightarrow}{X}^{(l)} = S^{(l \to s)}dT - V^{(l \to s)}dP$$
(27)

$$d\vec{X}^{(l)}\hat{G}^{(l)}d\vec{X}^{(l)} + (\vec{X}^{(l)} - \vec{X}^{(s)})\hat{G}^{(l)}d^{2}\vec{X}^{(l)} + (\vec{X}^{(l)} - \vec{X}^{(s)})\widehat{DG}^{(l)}d\vec{X}^{(l)} = (28)$$
$$S^{(l\to s)}dT + S^{(l\to s)}d^{2}T$$

where operator  $\widehat{DG}^{(l)}$  corresponds to the matrix of the second derivatives  $DG_{ij}^{(l)} = G_{ij}^{(l)}$   $(i \ge 2)$ in all lines except the first one, where we must set the following members:  $DG_{1,j}^{(l)} = \left(\partial \Delta_{n-1}^{(l)} / \partial X_j^{(l)}\right)_{T,P,x_{k \neq j,n}}$ . Finally, we obtain:

$$dX^{\to (l)} \hat{G}^{(l)} dX^{\to (l)} = S^{(l \to s)} d^2 T$$
(29)

The term  $dX^{\rightarrow(l)}\hat{G}^{(l)}dX^{\rightarrow(l)}$  is positively determined according to the criterion of the binodal stability quadratic form, whereas  $S^{(l\rightarrow s)} < 0$ . So,  $(d^2T)_P < 0$  and  $T_P$  should pass through the maximum.

It can be proven quite similarly for solubility diagrams that

$$d\vec{Y}^{(l)}\hat{G}^{[w](l)}d\vec{Y}^{(l)} = n_w^{[w](l\to s)}d^2\mu_w$$
(30)

and so  $(d^2 \mu_w)_{TP} < 0$  and  $\mu_w$  should pass through the maximum (distonic point).

The solubility diagram of the NaCl–CdCl<sub>2</sub>–H<sub>2</sub>O system [3] in coordinates "partial water pressure,  $P_w$ , Janecke index of CdCl<sub>2</sub>,  $y_{CdCl_2}$ " can be used as an example (Figure 1). It is clear that all three functions—(1)  $P_w$ ; (2) water activity:  $a_w = P_w/P_w^0$  (where  $P_w^0$  is pressure under pure water); (3) chemical potential of water:  $\mu_w = \mu_w^0 + RT \ln a_w$ —change in the same direction, so it does not matter which of them will be used to build the solubility diagram.



**Figure 1.** Diagram of solubility of the ternary system NaCl–CdCl<sub>2</sub>–H<sub>2</sub>O at 25 °C [3]. *E* is ternary eutonics, *D* is ternary distonics.

Another example is the Na<sup>+</sup>, Cd<sup>2+</sup>  $||Cl^-, S^-H_2O|$  quaternary reciprocal system at 25 °C, where the activity of water passes through the maximum at the point of the ternary compound NaCl·CdSO<sub>4</sub>·5H<sub>2</sub>O (Figure 2, [3]).



**Figure 2.** Solubility diagram of the Na<sup>+</sup>, Cd<sup>2+</sup> || Cl<sup>-</sup>, SO<sub>4</sub><sup>2-</sup> —quaternary reciprocal system at 25 °C [3]. The thin dashed and solid lines are isopotentials of water in the crystallization field of the ternary compound. The end of the arrow points to the point of the compound and simultaneously to the maximum activity of water.

Third rule (law).

Let us rewrite Equation (17) for the liquid phase:

$$\left(x_1^{(l)} - x_1^{(s)}\right)\hat{G}_{1,1}^{(l)}dx^{(l)} = S^{(l \to s)}dT$$
(31)

and Equations (18) and (19) for the vapor phase:

$$\left(x_1^{(v)} - x_1^{(l)}\right)\hat{G}_{1,1}^{(v)}dx^{(v)} = S^{(v \to l)}dT$$
(32)

$$\left(x_1^{(v)} - x_1^{(l)}\right)\hat{G}_{1,1}^{(v)}dx^{(v)} = -V^{(v \to l)}dP$$
(33)

Let us do the same with Equation (20):

$$\left(y_1^{(l)} - y_1^{(s)}\right)\hat{G}_{1,1}^{[w](l)}dy_1^{(l)} = n_w^{[w](l \to s)}d\mu_w$$
(34)

Let us now divide Equations (31)–(34) into Equations (17)–(20) in pairs. According to Equation (16), effects ( $\alpha \rightarrow \beta$ ) and ( $\beta \rightarrow \alpha$ ) have the opposite sign, whereas the second derivatives  $G_{ii}^{(\tau)}$  are always positives. Thus, we obtain and prove the following inequalities:

$$\begin{pmatrix} \frac{dx_{1}^{(s)}}{dx_{1}^{(l)}} \end{pmatrix}_{p} = -\frac{S^{(s\to l)}}{S^{(l\to s)}} \frac{G^{(s)}_{1,1}}{G^{(l)}_{1,1}} > 0 \begin{pmatrix} \frac{dx_{1}^{(v)}}{dx_{1}^{(l)}} \end{pmatrix}_{p} = -\frac{S^{(v\to l)}}{S^{(l\to v)}} \frac{G^{(v)}_{1,1}}{G^{(l)}_{1,1}} > 0 \begin{pmatrix} \frac{dx_{1}^{(v)}}{dx_{1}^{(l)}} \end{pmatrix}_{T} = -\frac{V^{(v\to l)}}{V^{(l\to v)}} \frac{G^{(v)}_{1,1}}{G^{(l)}_{1,1}} > 0 \begin{pmatrix} \frac{dy_{1}^{(s)}}{dx_{1}^{(l)}} \end{pmatrix}_{p} = -\frac{n^{[w](s\to l)}}{n^{[w](l\to s)}_{w}} \frac{G^{[w](s)}_{1,1}}{G^{[w](l)}_{1,1}} > 0$$

$$(35)$$

In other words, in binary systems, the compositions of liquid and vapor (both at T = const and at P = const) when moving along the liquid–vapor curve and the compositions of the melt and solid solution (at P = const) when moving along the melting curve always change in the same direction.

Likewise, the compositions of liquid and solid solutions calculated without taking into account the solvent, when moving along the solubility curve in a ternary system (at T, P = const), always change in the same direction.

These laws are not of a general nature, and are valid for multicomponent systems only in special cases, which we will discuss below.

### **2.** Algorithm of Calculation of Ternary Solubility Diagrams under Solid Solution Formation

The cumbersome wording of the considered laws (which become even more confusing in the case of quaternary systems) requires illustrations. For this purpose, we will use the solubility diagram of the reciprocal quaternary system  $K^+$ ,  $NH_4^+||Cl^-$ ,  $Br^- - H_2O$  (and its subsystems), which was chosen due to the following reasons:

- A large set of data on the concentration dependences of excess thermodynamic functions for all binary subsystems of the quaternary system is available.
- A large set of data on solubility for all ternary subsystems of the quaternary system (including the composition of equilibrium solid solutions) is also available. Moreover, there is a set of data concerning mixing the thermodynamic functions of binary solid solutions.
- In the ternary subsystems are realized different types of solid solutions: continuous series, and solid solutions with miscibility gaps.
- There are excellent (in our opinion) experimental data of solubility for the quaternary system itself, including the composition of ternary solid solutions.
- In the quaternary system are realized monovariant curves corresponding to the equilibria of saturated liquid with two different solid solutions.
- Analogues of Gibbs–Konovalov rules and Gibbs–Roozeboom laws may be installed, and demonstrate almost everything by the examples of ternary subsystems and quaternary reciprocal systems when the composition is moving along curves of open evaporation–crystallization, incomplete extrema, and thermodynamic simplification.

The algorithm of calculation (in particular based on the classic Pitzer equations [4–6]) of the solubility diagrams for ternary [7–9] (this section provides links to some pioneer publications only; the total number of papers on this topic is vast) and quaternary [7,10] systems, quaternary reciprocal systems [7,11], diagonal cuts of quaternary reciprocal systems [12], and more component systems [7,13] with constant composition solid phases has been widely used for several decades.

Articles devoted to the calculation of solubility diagrams under the formation of solid solutions, both in ternary and quaternary systems, are undoubtedly rarer [14–19]. This paper contains some generalizations of the last ones.

#### 2.1. Binary Subsystem Treatment

Parameters for the all binary subsystems are summarized in Table 1. They are suitable for the description of full concentration ranges up to saturation. Note that in this paper, the authors did not seek to describe the excess functions of the solutions as accurately as possible. The aim of the work was to illustrate strict thermodynamic laws. In this case, if the model is thermodynamically consistent (as Pitzer's model is), the parameter sets are not decisive.

Table 1.	Binary	parameters	of Pitzer's	equations	in the	$NH_4^+$ ,	$K^+  Cl^-$	, Br <sup>–</sup>	$-H_2O$	quaterna	ary
system at	t 25 °C.										

Crusterer	Binary Parameter Values								
System –	$oldsymbol{eta}^{(0)}$	$oldsymbol{eta}^{(1)}$	$oldsymbol{eta}^{(2)}$	$C^{(oldsymbol{arphi})}$	α1	α2			
$NH_4Cl - H_2O$	0.05201	0.1922	—	-0.00301	2.0	_			
KCl – H <sub>2</sub> O	0.04632	0.2222	—	-0.000397	2.0	_			
$NH_4Br - H_2O$	0.04240	0.06454	0.0981	-0.00222	2.0	1.0			
KBr – H <sub>2</sub> O	0.02543	0.2307	—	-0.00156	2.0	_			

Parameters for the KCl – H<sub>2</sub>O system were calculated from a smoothed array [20] of experimental data. For the KBr – H<sub>2</sub>O system, we used experimental data [21–23]. For the NH<sub>4</sub>Cl – H<sub>2</sub>O system, we calculated parameters from isopiestic data [24,25]. For the NH<sub>4</sub>Br – H<sub>2</sub>O system, we introduced the additional parameter  $\beta^{(2)}$  with the degree value  $\alpha_2$  = 1. The parameter fitting was based on the original data [23,25–27], with the obvious dropping points [23,26] discarded and the overlapping data [19,22] used only once.

For all binary subsystems, the standard deviations of the calculated values of osmotic coefficients from experimental ones,  $\sigma_{\varphi}$ , did not exceed 0.0014.

The thermodynamic potentials of the binary solid phases, calculated taking into account the activity coefficients of all solution components (or logarithms of solubility products, *ln* SP), are represented in Table 2.

Table	2.	Solubility	and	thermodynamic	potentials	of	binary	solid	phases	in	the
$NH_4^+$ ,	$K^+    C$	$Cl^-, Br^ H$	20 qu	aternary system at	t 25 °C.						

Solid Composition	Syngony <sup>a</sup>	Solubility, $m^{(s)}$ , mole/kg H <sub>2</sub> O	ln SP
	cfc	4.769 <sup>b</sup>	2.064
KCI -	cub <sup>e</sup>	$6.2 \pm 1.2$	$2.7\pm0.5$
	cfc	5.72 <sup>c</sup>	2.595
KBr	cub <sup>e</sup>	$6.5\pm1.0$	$2.9\pm0.4$
NIL CI	cub	7.393 <sup>b</sup>	2.853
NH4CI -	cfc <sup>e</sup>	$9.3 \pm 0.9$	$3.3\pm0.2$
NILI D.	cub	7.993 <sup>d</sup>	3.115
INFI4DI -	cfc <sup>e</sup>	$9.6 \pm 0.3$	$3.47\pm0.07$

<sup>a</sup> Hereafter: *cfc*—cubic face-centered lattice, *cub*—cubic lattice. <sup>b</sup> Corresponding values at 25 °C (26.23% and 28.34%) are recommended in [28]. <sup>c</sup> Value at 25 °C (40.5%) is recommended in [29]. <sup>d</sup> Average value at 25 °C from the data of 12 articles (43.91  $\pm$  0.07%). <sup>e</sup> The solid phase of this syngony is metastable at 25 °C.

#### 2.2. Ternary Subsystem Treatment

2.2.1. Parametrization of Ternary Liquid Solutions

For three of the four ternary subsystems, isopiestic data on water activity in the region of homogeneous liquid solutions are available in the literature. In the KCl – KBr –  $H_2O$  [22,30] and KBr –  $NH_4Br$  –  $H_2O$  [23] systems, water isoactivity lines are straight, i.e., these systems

obey Zdanovskii's rule. In the  $NH_4Cl - NH_4Br - H_2O$  system [25,31], very weak deviations from the straightness of water isoactivity lines are observed, which are comparable with the accuracy of the measurements. It is reasonable to assume that in the  $KCl - NH_4Cl - H_2O$ system, the water isoactivity lines will be also straight (or very close to straightness). Accordingly, calculations of Pitzer's ternary parameters were performed using "artificial arrays" of water isoactivity lines [32]. In all cases, the obtained values of the ternary parameters were very small, less than 0.0006 by module.

As we are going to describe the quaternary reciprocal system  $NH_4^+$ ,  $K^+||Cl^-$ ,  $-H_2O$ , we need to unify the parameters  $\theta_{Cl,Br}$  and  $\theta_{K,NH_4}$  in conjugated ternary systems. We put them equal to zero. Further calculations showed that all other parameters can also be set equal to zero without losing the accuracy of the description of the water activity data. Accordingly, we accepted  $\theta_{K,NH_4} = \theta_{Cl,Br} = \Psi_{K,NH_4,Cl} = \Psi_{K,NH_4,Br} = \Psi_{K,Cl,Br} = \Psi_{NH_4,Cl,Br} = 0.0$ . It is pertinent to note that in the general case, the straightness of the water isoactivity lines does not mean that the Pitzer ternary parameters are zero and vice versa.

#### 2.2.2. Solubility Equilibrium Data for the KCl – KBr – H<sub>2</sub>O Subsystem

The KCl – KBr – H<sub>2</sub>O system ranks among the first in the number of publications devoted to the study of solubility diagrams with solid solutions. At 25 °C alone, at least a dozen papers are devoted to this system [33–45] (in papers [34,38,39,41,45], the composition of the solid phase was not determined). In general, all of the mentioned experimental data are in good agreement with each other; only data [44] are somewhat different. A continuous series of solid solutions,  $KCl_xBr_{1-x}$ , are realized in this system. Approximations of phase equilibrium curves by polynomials were carried out in [46,47]; the calculation of the solubility diagram was performed in [48]. Moreover, densities of saturated solutions [33,42,45], densities and parameters of crystal lattice of solid solutions [49]; and some other solution characteristics, for example, enthalpies of crystallization of solid solutions [50], were investigated at 25 °C.

A number of papers were devoted to the calculation of the Gibbs energy of solid solution formation using different methods [51–54]; these data are in reasonable agreement with each other.

2.2.3. Solubility Equilibrium Data for the  $NH_4Cl - NH_4Br - H_2O$  Subsystem

The NH<sub>4</sub>Cl – NH<sub>4</sub>Br – H<sub>2</sub>O system was studied in less detail. The experimental solubility data [40,55] refer only to 25 °C. Evidence of these papers is in almost perfect agreement. Data on water pressure under saturated solutions and solid solution densities are also given in [55], while the dissolution heats of solid solutions are given in [31].

The Gibbs free energy of solid solution formation was calculated in papers [31,52,53,55,56]. Data from earlier work [55] suggest that the  $NH_4Cl_xBr_{1-x}$  solid solutions undergo decomposition due to diffusion instability. However, this conclusion has not been confirmed in later works, including by the authors themselves. So, a continuous series of solid solutions is realized in this system.

#### 2.2.4. Solubility Equilibrium Data for the KCl – NH<sub>4</sub>Cl – H<sub>2</sub>O Subsystem

Numerous papers have been devoted to the study of phase equilibria in this system, seven of which contain data at 25 °C [33,40,57–61]. However, in papers [59,61], only the compositions of the liquid phase are presented, while on the contrary, there are no complete data for the liquid phase in paper [61]. In paper [60], the composition of a single point is given, and the data of [33] have a very large scatter and do not agree well with the results of other works. Some data from [59] also fall out of the general set. From the other properties of equilibrium phases in the system, one can note the measurements of the density of saturated solutions in [33,59].

Two series of solid solutions,  $K_x(NH_4)_{1-x}Cl$  and  $(NH_4)_xK_{1-x}Cl$ , are realized in this system. It is not quite correct to talk about a miscibility gap in a series of solid solutions

here, since due to different crystal lattices, these solutions do not have a unified equation of state.

#### 2.2.5. Solubility Equilibrium Data for the KBr – NH<sub>4</sub>Br – H<sub>2</sub>O Subsystem

Phase equilibria at 25 °C in this system were studied in [33,40,62,63]. A considerable amount of consistent data were obtained, excepting two points from [33]. Note that in paper [62], the recalculation of the composition of "wet residues" into mole fractions of components in the solid phase is performed imprecisely, and in paper [63], it is necessary to combine the data of Tables 1 and 2 to obtain data on the liquid phase compositions with four significant digits instead of two. Data on the density of saturated solutions are represented in paper [33], and information on water activity in saturated solutions and the calculation of Gibbs energy of solid solution formation is available in paper [63].

Again, two series of solid solutions,  $K_x(NH_4)_{1-x}Br$  and  $(NH_4)_xK_{1-x}Br$ , are realized in this system.

#### 2.2.6. Algorithm of Ternary Solubility Diagram Calculation

Regardless of the type of crystallizing solid solutions, the first calculation step is to calculate the Gibbs free energy of solid solution formation,  $\Delta G$ , from the experimental solubility data. In the case of the CA – C'A – H<sub>2</sub>O system, where the (CA)<sub>X</sub>(C'A)<sub>1–X</sub>· $\nu$ H<sub>2</sub>O solid solutions are crystallized, we can write:

$$\frac{\Delta G}{RT} = x_{\text{CA}\cdot\nu\text{H}_2\text{O}}^{(s)} \left[ \ln a_{\text{CA}}^{(l)} - \ln SP_{\text{CA}\cdot\nu\text{H}_2\text{O}}^{(s)} \right] + \left( 1 - x_{\text{CA}\cdot\nu\text{H}_2\text{O}}^{(s)} \right) \left[ \ln a_{\text{C'A}}^{(l)} - \ln SP_{\text{C'A}\cdot\nu\text{H}_2\text{O}}^{(s)} \right] + \nu_{\text{H}_2\text{O}} \ln a_{\text{H}_2\text{O}}^{(l)}$$
(36)

where  $a_i^{(l)}$  is activity of the *i*-th salt or water in the liquid phase,  $x_{CA \cdot \nu H_2O}^{(s)}$  is the mole fraction of  $CA \cdot \nu H_2O$  in the solid solution. Of course, the same equation is valid, mutatis mutandis, for the  $CA - CA' - H_2O$  system with the  $(CA)_X(CA')_{1-X} \cdot \nu H_2O$  solid solutions, and  $\nu$  can be equal to zero.

 $SP_{Salt 
u H_2O}^{(lattice)}$  is the thermodynamic potential of the solid solution component (thermodynamic solubility product), and is defined and is calculated as

$$\ln SP_{\text{Salt}\nu\text{H}_2\text{O}}^{(\text{lattice})} = \frac{1}{RT} \Big[ \mu_{\text{Salt}\nu\text{H}_2\text{O}}^{0(\text{lattice})} - \mu_{\text{Salt}\nu\text{H}_2\text{O}}^{0(l)} \Big] = \ln a_{\text{Salt}}^{(l,\text{sat})} + \nu_{\text{H}_2\text{O}} \ln a_{\text{H}_2\text{O}}^{(l,\text{sat})}$$
(37)

where the superscript "lattice" emphasizes that the solid solution component possesses the same crystal lattice (syngony) as the solid solution itself (which may correspond to a metastable state);  $\mu_{Salt \cdot \nu H_2O}^{0(lattice)}$  is its standard chemical potential in a state such as this;  $\mu^{0(l)}$  is the normalized standard chemical potential of the component in the liquid phase;  $a_i^{(l,sat)}$  is the activity of the *i*-th component in the liquid solution saturated with respect to the solid phase in the aforesaid state. A compound can possess several *SPs*, but each of them is invariant at fixed *T* and *P*. It should be additionally noted that according to the criterion of bimodal and spinodal thermodynamic stability, the solubility of the solid solution components (and the corresponding values of thermodynamic potentials, *SP*) in the metastable state should always be higher than in the stable state.

At this stage, for systems with a continuous series of solid solutions, the essential point is the need to check the consistency of solubility in binary subsystems and ternary systems and choose consistent values of ln *SP*; the procedure for such a check is described in [15,64]. It is somewhat more difficult to calculate  $\Delta G$  in ternary systems under the formation of two series of solid solutions because part of the ln *SP* values cannot always be directly determined from the binary solubility data. The methods of action in this case are considered in paper [18].

We approximated the determined values of  $\Delta G$  with a subregular solution model (of course any other model can be used as well):

$$\Delta G^{ex} = \Delta G - \sum_{i=\text{KCl},\text{KBr}} \left[ x_i^{(s)} \ln x_i^{(s)} \right] = x_{\text{KCl}}^{(s)} x_{\text{KBr}}^{(s)} \left[ \alpha_0 + \alpha_1 \left( x_{\text{KCl}}^{(s)} - x_{\text{KBr}}^{(s)} \right) \right]$$
(38)

where  $\alpha_0$  and  $\alpha_1$  are adjustable parameters. Strictly speaking, a subregular model was required only for the KCl–KBr solutions; in the other three cases  $\alpha_1 = 0$ , that is, the model of regular solutions, was used—see Table 3. The results of the calculations of  $\Delta G$  for the systems under consideration are shown in Figure 3a,b.

Table 3. Parameters of regular and subregular models for solid solutions at 25  $^\circ C.$ 

System *	α <sub>0</sub> , kJ/mol	α <sub>1</sub> , kJ/mol	System *	α <sub>0</sub> , kJ/mol	$\alpha_1$ , kJ/mol
$NH_4Cl - KCl (cub)$	$7.7\pm1.8$		$NH_4Cl - KCl (cfc)$	$3.8\pm0.2$	—
$NH_4Br - KBr(cub)$	$8.5\pm1.2$		$NH_4Br - KBr(cfc)$	$2.9\pm0.3$	—
KCl– KBr(cub)	$3.6\pm0.5$	_	KCl– KBr(cfc)	$\begin{array}{c} 3.64 \pm 0.05 \\ 3.63 \pm 0.06 \end{array}$	$0.5\pm0.1$
$NH_4Cl - NH_4Br(cub)$	$3.8\pm0.1$		$NH_4Cl - NH_4Br(cfc)$	$3.7\pm0.7$	

\* *cub*—cubic lattice, *cfc*—cubic face-centered lattice.

The subregular model provides us with the activity coefficients of solid solution components,  $f_i^{(s)}$ :

$$\begin{cases} RT \ln f_{\text{KCl}}^{(s)} = \left(x_{\text{KBr}}^{(s)}\right)^2 \left[\alpha_0 + \alpha_1 \left(3x_{\text{KCl}}^{(s)} - x_{\text{KBr}}^{(s)}\right)\right] \\ RT \ln f_{\text{KBr}}^{(s)} = \left(x_{\text{KCl}}^{(s)}\right)^2 \left[\alpha_0 + \alpha_1 \left(x_{\text{KCl}}^{(s)} - 3x_{\text{KBr}}^{(s)}\right)\right] \end{cases}$$
(39)

The final calculations are reduced to solving a system of equations derived from the phase and chemical equilibrium conditions. In the general case, it looks like

$$\begin{cases} \ln a_{CA}^{(l)} + \nu_{H_{2O}} \ln a_{H_{2O}}^{(l)} = \ln SP_{CA \cdot \nu H_{2O}}^{(s)} + \ln a_{CA \cdot \nu H_{2O}}^{(s)} \\ \ln a_{C'A}^{(l)} + \nu_{H_{2O}} \ln a_{H_{2O}}^{(l)} = \ln SP_{C'A \cdot \nu H_{2O}}^{(s)} + \ln a_{C'A \cdot \nu H_{2O}}^{(s)} \end{cases}$$
(40)



Figure 3. Cont.



**Figure 3.** (a) Calculated values of excess Gibbs energy of solid solution formation in experimental points (open signs) and their approximation by regular model (solid lines) and subregular model (dotted lines) in the systems  $K^+$ ,  $NH_4^+$  || $Br^-$ - $H_2O$  (left) and  $K^+$  || $Cl^-$ ,  $Br^-$ - $H_2O$  (right) at 25 °C. (b) Calculated values of excess Gibbs energy of solid solution formation in experimental points (open signs) and their approximation by regular model (solid lines) in the systems  $K^+$ ,  $NH_4^+$  || $Cl^-$ - $H_2O$  (left) and  $NH_4^+$  || $Cl^-$ ,  $Br^-$ - $H_2O$  (right) at 25 °C.

The results of calculations of the liquidus are presented in Figure 4, and the distribution diagrams of the salt components between the equilibrium phases are presented in Figure 5a,b. In the  $K^+||Cl^-, Br^--H_2O$  system, both solid phase models reproduce the experimental liquidus well, but the distribution diagram is somewhat better reproduced by the subregular solution model than by the regular solution model.



**Figure 4.** Experimental (open signs) and calculated (solid lines) data on the composition of saturated solutions in ternary systems  $K^+$ ,  $NH_4^+$ || $Cl^-$ - $H_2O$ ,  $K^+$ ,  $NH_4^+$ || $Br^-$ - $H_2O$ ,  $K^+$ || $Cl^-$ ,  $Br^-$ - $H_2O$ ,  $NH_4^+$ || $Cl^-$ ,  $Br^-$ - $H_2O$  at 25 °C (in salt molalities). Data falling out of the general set: a number of triangles with a base on the right [33], stars [44,45], a few pentagons [61].



**(b)** 

**Figure 5.** (a) The systems  $K^+$ ,  $NH_4^+$  || $Br^--H_2O$  (left) and  $K^+$ || $Cl^-$ ,  $Br^--H_2O$  (right) at 25 °C: experimental (open signs) and calculated (solid lines) data on the distribution of salt components between liquid and solid solutions in solvent-free concentration space (Janecke indexes). (b) The systems  $K^+$ ,  $NH_4^+$  || $Cl^--H_2O$  (left) and  $NH_4^+$  || $Cl^-$ ,  $Br^--H_2O$  (right) at 25 °C: experimental (open signs) and calculated (solid lines) data on the distribution of salt components between liquid and solid solutions in solvent-free concentration space (Janecke indexes).

2.2.7. Classification of Solid Solutions on Ternary Solubility Diagrams

Without encroaching on Roozeboom's classification, in our opinion, it is convenient to distinguish six basic types of solid solutions in the light of the aforesaid work.

Types I: Continuous series of solid solutions without miscibility gaps.

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This is the most trivial case: the hydrate composition and syngony of both components of solid solutions are the same. *SP* values can be found from the solubility of components in binary subsystems and  $\Delta G$  values are calculated in experimental points from Equation (36). The monovariant solubility curve is the geometric place of points that satisfy the system of two nonlinear Equations (40) with respect to three unknown variables, the composition of the saturated ternary liquid solution (for example, CA and C'A molalities), and the mole fraction of one of the solid solution components. Any of these variables can be fixed before solving the system.

According to the derived above analogues of the Gibbs–Roozeboom rules and Gibbs– Konovalov laws, three subtypes are possible.

Subtype Ia: Extrema of water activity are absent.

This is a fairly common type, but it is not represented in the ternary systems considered here. Let us consider as an example the diagram of the  $TbCl_3$ -GdCl\_3-H<sub>2</sub>O at 25 °C, Figure 6 [65].



**Figure 6.** Diagram of solubility as water activity vs. Janecke index of the TbCl<sub>3</sub>–GdCl<sub>3</sub>–H<sub>2</sub>O system at 25 °C under formation of the Tb<sub>x</sub>Gd<sub>1-x</sub>Cl<sub>3</sub>·6H<sub>2</sub>O solid solutions.

Subtype Ib: A minimum of water activity is present.

Two such ternary systems are presented among those considered here, namely  $KCl - KBr - H_2O$  and  $NH_4Cl - NH_4Br - H_2O$ . For both systems, we calculated stable and metastable variants of the diagram (Figures 7 and 8). In all cases, the minimum water activity in the saturated solutions is realized when the compositions of equilibrium phases in the solvent-reduced concentration space are equal, in full accordance with the analogue of the second Gibbs–Roozeboom rule and Gibbs–Konovalov law. We propose to call such a minimum alyotrope (" $\alpha$ " + " $\lambda \dot{\nu} \omega$ " + " $\tau \rho \dot{\sigma} \tau \sigma \zeta$ ", "no change on dissolving"), by analogy with azeotropes (" $\alpha$ " + " $\zeta \dot{\epsilon} \omega$ " + " $\tau \rho \dot{\sigma} \tau \sigma \zeta$ ", "no change on boiling") in liquid–vapor diagrams.



**Figure 7.** Solubility diagram of water activity vs. Janecke index of the KCl–KBr–H<sub>2</sub>O system at 25 °C. Solid points correspond to the formation of stable solid solutions on the base of face-centered (*cfc*) lattice, while open circles correspond to metastable cubic (*cub*) solution formation. Hereafter,  $A^{(3)}$  is alyotrope point.



**Figure 8.** Solubility diagram of water activity vs. Janecke index of the NH<sub>4</sub>Cl–NH<sub>4</sub>Br–H<sub>2</sub>O system at 25 °C. Solid points correspond to the formation of stable solid solutions on the base of cubic (*cub*) lattice, while open circles correspond to the metastable face-centered (*cfc*) solution formation.

Subtype Ic: A maximum of water activity is present.

There are no such examples in the ternary systems under consideration. Moreover, we looked through the reference data for more than 130 ternary water–salt systems with a continuous series of solid solutions, and could not find a single example where the water activity (or the molar fraction of water, which is almost equivalent) in saturated solutions passes through the maximum.

This is surprising, since for liquid–vapor diagrams and fusibility diagrams of binary systems, which are topologically isomorphic to solubility diagrams of ternary systems [7], diagrams with both minimum and maximum  $T_P(x)$  and  $P_T(x)$  are well known. This is the only case among all those known to the authors that does not correspond to the postulate of complete topological equivalence of liquid–vapor diagrams, melting diagrams, and solubility diagrams in the corresponding sets of variables.

Type II: Discontinuous series of solid solutions with miscibility gaps due to diffusion instability.

In this case, the solubility diagram consists of two curves corresponding to the crystallization of the same solid solution (with the same qualitative (hydrate) composition and uniform syngony) decaying at the nonvariant point due to diffusion instability (this occurs when there are strong positive deviations of the solid solution from ideality). As before, the *SP* values are available from the binary solubilities of its components, and system (40) describes both curves with  $0 \le x_1^{(s)} \le x_1^{(\lim_1)}$  and  $x_1^{(\lim_2)} \le x_1^{(s)} \le 1$ , where  $\lim_1$  and  $\lim_2$  symbolize the broadness of the diffusion instability of the solid solutions and  $x_1^{(\lim_1)} < x_1^{(s)} < x_1^{(\lim_2)}$  is the miscibility gap.

As is well known, the equation for the loss of phase diffusion stability (or spinodal curve) for a binary solid solution, *s*, is as follows:

$$\left(\frac{\partial^2 G^{(s)}}{\partial x_i^{(s)} 2}\right)_{T,P} = 0 \text{ or } \left(\frac{\partial \mu_i^{(s)}}{\partial x_i^{(s)}}\right)_{T,P} = 0$$
(41)

Within the model of regular (or subregular) solutions, Equation (41) is reduced to an algebraic quadratic (or cubic) equation, which allows one to find both the  $x_1^{(\lim_{1 \to 1})}$  and  $x_1^{(\lim_{1 \to 1})}$  roots.

Alternatively, we can calculate the composition of the nonvariant point by solving a system of four equations similar to Equation (40) with respect to two liquid phase composition variables (molalities, for example) and two solid phase composition variables  $(x_1^{(\lim_1)} \text{ and } x_1^{(\lim_2)})$ .

Moreover, if we have reliable experimental data on the composition of solid solutions at the point of decomposition, we can determine their nonideality parameters directly with Equation (41).

In reality, such a case is rare. However, two (partially metastable) diagrams can be presented for the ternary systems under consideration; see Figures 9 and 10.

Type III: Discontinuous (different) series of solid solutions with miscibility gaps due to difference in syngony.

In this case, the solubility diagram also consists of two curves, corresponding to the crystallization of two solid solutions with the same qualitative composition but different syngony. It is more correct to speak not about a miscibility gap, but about two series of different solid solutions, because these solutions do not have a common equation of state in principle.

Here, we have four *SP* values, two for each of the solid solution components possessing the corresponding crystal lattice. However, only two of them can be determined directly, since in most cases there are no data on the binary solubility of the component in an alien syngony. The missing *SP* values can be determined simultaneously with fitting the solid phase model parameters from experimental solubility data.



**Figure 9.** Solubility diagram of water activity vs. Janecke index of the KCl –  $NH_4Cl - H_2O$  system at 25 °C. All solid solutions have cubic syngony (*cub*). Solid points correspond to stable part of diagram; open cycles respond metastable one. Hereafter,  $E^{(3)}$  is ternary eutonics.



**Figure 10.** Solubility diagram of water activity vs. Janecke index of the KBr –  $NH_4Br$  –  $H_2O$  system at 25 °C. All solid solutions have cubic syngony (*cub*). Solid points correspond to stable part of diagram; open cycles respond metastable one.

Again, the system of two Equations (40) is suitable for calculating each of the two branches of solubility of solid solutions (each branch has its own system), and the

nonvariant point can be calculated by solving the system of four such equations. It is easier, however, to first determine the composition of the solid phases using the following system:

$$\begin{cases} \ln SP_{CA \cdot \nu H_2O}^{(ss_1)} + \ln a_{CA \cdot \nu H_2O}^{(ss_1)} = \ln SP_{CA \cdot \nu H_2O}^{(ss_2)} + \ln a_{CA \cdot \nu H_2O}^{(ss_2)} \\ \ln SP_{C'A \cdot \nu H_2O}^{(ss_1)} + \ln a_{C'A \cdot \nu H_2O}^{(ss_1)} = \ln SP_{C'A \cdot \nu H_2O}^{(ss_2)} + \ln a_{C'A \cdot \nu H_2O}^{(ss_2)} \end{cases}$$
(42)

where  $ss_i$  denotes solid solution *i*. This system reflects the obvious fact that solid solutions are in equilibrium not only with the liquid solution but also with each other. System (42) can also be used to check the experimental data on solubility.

It should be noted that model parameters of the solvent-free solid phase can be determined from indirect data such as solubility in another solvent, fusibility diagrams, or diagrams of the resolution of the solid solution. Sometimes, this requires temperature extrapolation.

Among the ternary systems under consideration, there are two diagrams (stable) of this type; see Figures 11 and 12.



**Figure 11.** Solubility diagram of water activity vs. Janecke index of the KCl - NH<sub>4</sub>Cl - H<sub>2</sub>O system at 25 °C.

Type IV: Discontinuous (different) series of solid solutions with miscibility gaps due to differences in hydrate composition.

In this case, the solubility diagram also consists of two branches corresponding to the crystallization of two solid solutions with different hydrate compositions, whilst their syngony may be the same or may be different. Here, we also should speak of two different solid solutions rather than a miscibility gap, as for type III.

What has been said about the calculation of the solubility diagrams of type III remains valid, except for two peculiarities. First, the missing *SP* values can often be obtained from the binary solubility diagram of the component with moderate temperature extrapolation. Second, the equations of system (8) turn out not to be decoupled from the liquid phase, since they contain an additional term related to the difference in hydrate composition:



**Figure 12.** Solubility diagram of water activity vs. Janecke index of the KBr - NH<sub>4</sub>Br - H<sub>2</sub>O system at 25 °C.

As an example, let us present a solubility diagram in the  $NdCl_3$ - $PrCl_3$ - $H_2O$  ternary system at 25 °C; see Figure 13 [66].



**Figure 13.** Solubility diagram of water activity vs. Janecke index of the NdCl<sub>3</sub>–PrCl<sub>3</sub>–H<sub>2</sub>O system at 25 °C [66]. Solid solutions are  $Pr_xNd_{1-x}Cl_3 \cdot 7H_2O$  and  $Pr_xNd_{1-x}Cl_3 \cdot 6H_2O$ .

Type V: Internal series of solid solutions.

Two main subtypes can be distinguished here.

Subtype Va.

This subtype is caused by the dehydration of solvated solid solutions due to decreasing water activity as the concentration of components in the liquid phase increases. A new solid solution curve with lower water content can "wedge" into the crystallization curve of solid solutions with higher water content. Basic solubility diagrams of this type are shown in Figure 14.



**Figure 14.** Basic schemes of diagram of solubility of the CA – C'A – H<sub>2</sub>O ternary system with the dehydration of solid solution. C<sub>X</sub> C'<sub>1-X</sub>A·Q<sub>1</sub>H<sub>2</sub>O  $\rightarrow$  C<sub>X</sub> C'<sub>1-X</sub>A·Q<sub>2</sub>H<sub>2</sub>O + (Q<sub>1</sub> – Q<sub>2</sub>)H<sub>2</sub>O (Q<sub>1</sub> > Q<sub>2</sub>). Waters activities of dehydration of binary crystal hydrates are  $a_W^{ds(CA\cdot Q_1H_2O)}$  and  $a_W^{ds(C'A\cdot Q_1H_2O)}$ .

As example of this type of diagram, we can point to the following: the  $MgSO_4 - NiSO_4 - H_2O$  system at 35 °C, in which a series of  $Mg_xNi_{1-x}\cdot 6H_2O$  solid solutions of type Ia appear "inside" a series of the  $Mg_xNi_{1-x}\cdot 7H_2O$  solid solutions belonging to type Ia [67,68]; and the  $CoSO_4 - NiSO_4 - H_2O$  system above 26 °C, in which a series of the  $Co_xNi_{1-x}\cdot 6H_2O$  solid solutions of type Ia "lies on" the miscibility gap in a series of the  $Co_xNi_{1-x}\cdot 7H_2O$  solid solutions belonging to type III [69,70].

Subtype Vb. Solid solutions on the base of a ternary compound (double salt).

As an example, we can consider the solubility diagram of the system  $MgCl_2 - FeCl_2 - H_2O$  within 40–60 °C, where three series of solid solutions are crystallized:  $Mg_xFe'_{1-x}Cl_2\cdot 6H_2O$  based on  $MgCl_2\cdot 6H_2O$ ,  $Mg'_yFe_{1-y}Cl_2\cdot 4H_2O$  based on  $FeCl_2\cdot 4H_2O$ , and  $(MgCl_2)_z\cdot (FeCl_2)_{1-z}\cdot 8H_2O$  [71–73]. The scheme of the solubility diagram in this case is shown in Figure 15. The calculation algorithm in this case is also preserved, but it should be taken into account that all parameters of the middle solid solution are not available and must be determined by fitting procedure.



**Figure 15.** Scheme of diagram of solubility in ternary system with the formation of solid solutions on the base of ternary compound (double salt).

Type VI: Solid solutions with the variable water content, or so-called "abnormal solid solutions".

As for solid solutions with variable water content in water–salt systems, there is no consensus in the literature either on the mechanism of their formation or on the components that form them. Some authors even question the very fact of their existence. Accordingly, consideration of such solutions is out of the scope of this paper.

# 3. Diagrams of Quaternary Reciprocal Systems under Formation of Ternary Reciprocal Solid Solutions

3.1. Backgrounds of Modeling Ternary Reciprocal Solid Solutions

A multicomponent system C, C', C'' ...  $||A, A', A'' ... (-H_2O)|$  is called reciprocal if at least one reversible chemical reaction can occur:

$$CA' + C'A \rightleftharpoons CA + C'A'$$
 (44)

Here, in general, C, C' and A, A' are qualitatively different constituents of substances, such as cations and anions, elements of  $A^3$ -groups and  $B^5$ -groups, alcoholic and acidic functional groups, etc.

According to the conditions of chemical equilibrium in a phase of variable composition, the consequence of Equation (44) is the following:

$$\mu_{CA} + \mu_{C'A'} = \mu_{C'A} + \mu_{CA'} \tag{45}$$

where  $\mu_i$  is chemical potential of the *i*-th component in the phase.

In the modeling of the liquid phase on the basis of well-known Friedman axiomatics (most often used in modeling of electrolyte solutions, for example, in the Pitzer model), when the asymmetric normalization of excess thermodynamic functions (in infinitely dilute solution water activity equal to 1 and logarithm of activity coefficient of any salt equal to 0) is used, no additional concordance with Equation (45) is required, since

$$\Delta \ln a^{\infty(l)} = \ln a^{\infty(l)}_{CA} + \ln a^{\infty(l)}_{C'A'} - \ln a^{\infty(l)}_{C'A} - \ln a^{\infty(l)}_{CA'} \equiv 0$$

$$\Delta G^{0(l)} = \mu^{0(l)}_{CA} + \mu^{0(l)}_{C'A'} - \mu^{0(l)}_{C'A} - \mu^{0(l)}_{CA'} \equiv 0$$
(46)

where  $a_i^{\infty(l)}$  and  $\mu_i^{0(l)}$  are the activity and standard chemical potential of the *i*-th salt in an infinitely dilute solution, and  $\Delta G^{0(l)}$  is the standard change in the Gibbs energy of reaction (44) in an infinitely diluted solution. Incidentally, to agree with equations such as (46) in calculations in reciprocal systems, we need to unify ternary parameters (such as  $\theta_{C,C'}$  and  $\theta_{A,A'}$  in Pitzer equations) in conjugated systems C, C'||A – H<sub>2</sub>O and C, C'||A' – H<sub>2</sub>O, C||A, A' – H<sub>2</sub>O and C'||A, A' – H<sub>2</sub>O.

If symmetric normalization (the logarithm of the activity coefficient equals to 0 for any pure component) is used in the modeling in the reciprocal system—as is the case, for example, in the solid solution model—then

$$\Delta \ln a^{(s)} = \ln a^{(s)}_{CA \cdot \nu H_2O} + \ln a^{(s)}_{C'A' \cdot \nu H_2O} - \ln a^{(s)}_{C'A \cdot \nu H_2O} - \ln a^{(s)}_{CA' \cdot \nu H_2O} \neq 0$$

$$\Delta G^{0(s)} = \mu^{0(s)}_{CA \cdot \nu H_2O} + \mu^{0(s)}_{C'A' \cdot \nu H_2O} - \mu^{0(s)}_{C'A \cdot \nu H_2O} - \mu^{0(s)}_{CA' \cdot \nu H_2O} \neq 0$$
(47)

because of the different standard state for pure salts.

The problem of harmonization of the model of reciprocal solid solutions with Equation (45) was solved by one of the authors in papers [74,75] for the case of calculating the fusibility diagrams of reciprocal  $A^{3}B^{5}$  systems. For the ternary reciprocal regular solution of isovalent substitution  $C_{x}C'_{1-x}||A_{y}C'_{1-y}\cdot\nu H_{2}O|$  ( $\nu$  can be equal to zero as for  $K_{x}(NH_{4})_{1-x}Cl_{y}Br_{1-\nu}$ , in our case), we have

$$\mu_{CA \cdot \nu H_{2}O}^{(s)} = \mu_{CA \cdot \nu H_{2}O}^{0(s)} + RT \ln(xy) + (1-x)^{2} \left[ y \alpha_{CA - C'A}^{(s)} + (1-y) \alpha_{CA' - C'A'}^{(s)} \right] + (1-y)^{2} \left[ x \alpha_{CA - CA'}^{(s)} + (1-x) \alpha_{C'A - C'A'}^{(s)} \right] + (1-x)(1-y) \Delta G^{0(s)}$$

$$\mu_{C'A \cdot \nu H_{2}O}^{(s)} = \mu_{C'A \cdot \nu H_{2}O}^{0(s)} + RT \ln((1-x)y) + x^{2} \left[ y \alpha_{CA - C'A}^{(s)} + (1-y) \alpha_{CA' - C'A'}^{(s)} \right] + (1-y)^{2} \left[ x \alpha_{CA - CA'}^{(s)} + (1-x) \alpha_{C'A - C'A'}^{(s)} \right] + x(1-y) \Delta G^{0(s)}$$

$$\mu_{CA' \cdot \nu H_{2}O}^{(s)} = \mu_{CA' \cdot \nu H_{2}O}^{0(s)} + RT \ln(x(1-y)) + (1-x)^{2} \left[ y \alpha_{CA - C'A}^{(s)} + (1-y) \alpha_{CA' - C'A'}^{(s)} \right] + y^{2} \left[ x \alpha_{CA - CA'}^{(s)} + (1-x) \alpha_{C'A - C'A'}^{(s)} \right] + (1-x)y \Delta G^{0(s)}$$

$$\mu_{CA' \cdot \nu H_{2}O}^{(s)} = \mu_{C'A' \cdot \nu H_{2}O}^{0(s)} + RT \ln((1-x)(1-y)) + x^{2} \left[ y \alpha_{CA - C'A}^{(s)} + (1-y) \alpha_{CA' - C'A'}^{(s)} \right] + y^{2} \left[ x \alpha_{CA - CA'}^{(s)} + (1-x) \alpha_{C'A - C'A'}^{(s)} \right] + (1-x)y \Delta G^{0(s)}$$

$$\mu_{C'A' \cdot \nu H_{2}O}^{0(s)} = \mu_{C'A' \cdot \nu H_{2}O}^{0(s)} + RT \ln((1-x)(1-y)) + x^{2} \left[ y \alpha_{CA - C'A}^{(s)} + (1-y) \alpha_{CA' - C'A'}^{(s)} \right] + y^{2} \left[ x \alpha_{CA - CA'}^{(s)} + (1-x) \alpha_{C'A - C'A'}^{(s)} \right] + (1-x) \Delta G^{0(s)}$$

where  $\alpha_{i-j}^{(s)}$  are the regular model parameters of the binary solid solution of the corresponding syngony (see Table 3). The value of  $\Delta G^{0(s)}$  arising due to different normalization is easily obtained from the solubility products of the constituents of the solid solution. In fact,

$$\ln SP_i = \frac{\mu_i^{0(s)} - \mu_i^{0(l)}}{RT}$$
(49)

and so,

μ

$$\Delta G^{0(s)} \equiv \Delta \ln SP = \ln SP_{CA'} + \ln SP_{CA} - \ln SP_{CA} - \ln SP_{CA'}$$
(50)

### 3.2. Calculation Algorithm of Solubility Diagram of Quaternary Reciprocal Systems under Solid Solution Formation

According to the Gibbs phase rule, in a quaternary reciprocal water–salt system at T, P = const, up to three solid solutions can coexist with the liquid phase. Such solid solutions may differ in hydrate composition or in crystalline lattices, or, if the above coincide, have a miscibility gap due to diffusion instability. In general, we can distinguish approximately the same cases as for the ternary systems above.

Case I: Continuous series (field) of solid solutions without miscibility gaps.

We were unable to find examples of such diagrams among reciprocal water–salt systems, but they are known for quaternary systems with a common ion ([17], the  $Mg^{2+}, Ni^{2+}, Zn^{2+} || SO_4^{2-} - H_2O$  system at 25 °C, with the only field of crystallization of the  $Mg_xNi_yZn_{1-x-y}$ ·7H<sub>2</sub>O solid solutions) and for quaternary high-temperature solubility (fusibility) diagrams ([76], the Ga, In, P, As – Pb system at 600 °C, where a continuous field of crystallization of the  $Ga_xIn_{1-x}P_yAs_{1-y}$  solid solutions exists). However, any solubility diagram of a reciprocal system always includes exactly such elements, namely the crystallization fields of solid solutions of a certain type.

Let us consider, for example, the two-phase equilibrium in the quaternary reciprocal system K<sup>+</sup>, NH<sub>4</sub><sup>+</sup> ||Cl<sup>-</sup>, Br<sup>-</sup> – H<sub>2</sub>O at 25 °C between a liquid phase and the ternary reciprocal solid solutions based on the cubic face-centered lattice,  $K_x^+$  (NH<sub>4</sub><sup>+</sup>)<sub>1-x</sub>Cl<sub>y</sub><sup>-</sup> Br<sub>1-y</sub><sup>-(cfc)</sup>. According to the phase equilibrium conditions, one can write

$$\begin{cases}
\ln a_{\text{KBr}}^{(l)} = \ln SP_{\text{KBr}}^{(cfc)} + \ln(xy) + \frac{\alpha_{\text{K-NH}_4}^{(cfc)}}{RT} (1-x)^2 + \frac{\alpha_{\text{Cl-Br}}^{(cfc)}}{RT} (1-y)^2 + \\
(1-x)(1-y) \,\Delta \ln SP^{(cfc)} \\
\ln a_{\text{KCl}}^{(l)} = \ln SP_{\text{KCl}}^{(cfc)} + \ln(x(1-y)) + \frac{\alpha_{\text{K-NH}_4}^{(cfc)}}{RT} (1-x)^2 + \frac{\alpha_{\text{Cl-Br}}^{(cfc)}}{RT} y^2 - \\
(1-x)y \,\Delta \ln SP^{(cfc)} \\
\ln a_{\text{NH}_4\text{Cl}}^{(l)} = \ln SP_{\text{NH}_4\text{Cl}}^{(cfc)} + \ln(((1-x)y) + \frac{\alpha_{\text{K-NH}_4}^{(cfc)}}{RT} x^2 + \frac{\alpha_{\text{Cl-Br}}^{(cfc)}}{RT} (1-y)^2 - \\
x(1-y) \,\Delta \ln SP^{(cfc)}
\end{cases}$$
(51)

where

$$\begin{cases} \alpha_{\rm K-NH_4}^{(cfc)} = y \alpha_{\rm KCl-NH_4Cl}^{(cfc)} + (1-y) \alpha_{\rm KBr-NH_4Br}^{(cfc)} \\ \alpha_{\rm Cl-Br}^{(cfc)} = x \alpha_{\rm KCl-KBr}^{(cfc)} + (1-x) \alpha_{\rm NH_4Cl-NH_4Br}^{(cfc)} \end{cases}$$
(52)

and

$$\Delta \ln SP^{(cfc)} = \ln SP^{(cfc)}_{\rm KBr} + \ln SP^{(cfc)}_{\rm NH_4Cl} - \ln SP^{(cfc)}_{\rm NH_4Br} - \ln SP^{(cfc)}_{\rm KCl}$$
(53)

The fourth equation  $(\ln a_{\text{NH}_4\text{Br}}^{(l)} = \cdots)$  in the system (51) is omitted because it is a linear combination of the first three due to condition (45).

The system of Equation (51) contains five independent variables. Three of them correspond to the composition of the liquid phase (for example, molalities of any three salts, with the fourth molality linked to them by Equation (44) or via the electroneutrality equation), and the other two correspond to solid solution composition. Thus, we describe a bivariate surface of two-phase equilibrium.

We can introduce up to two additional conditions in the numerical solution of the system (51). For example, we can calculate a water isoactivity line in the field of solid solution crystallization by specifying the value  $a_w$ , or calculate the diagonal cross section of the diagram by setting  $y_{K^+}^{(l)} = y_{Cl^-}^{(l)}$ , etc.

When using a solid solution model other than the regular one, the problem to be solved is not essentially different.

Case II: Series of solid solutions with miscibility gaps due to diffusion instability.

The solubility diagram in this case consists of two fields, corresponding to the crystallization of two solid solutions with the same qualitative composition, and one monovariant curve corresponding to the three-phase equilibrium of the saturated liquid solution with both solid solutions. System (51) is still valid for each of the fields. The monovariant curve can be calculated either by solving the system of six nonlinear equations (three for each solid solution), or as follows.

The loss of diffusion stability in the ternary reciprocal solution corresponds to the condition

$$\frac{\frac{\partial^2 G^{(s)}}{\partial x_1^2}}{\frac{\partial^2 G^{(s)}}{\partial x_2 \partial x_1}} \frac{\frac{\partial^2 G^{(s)}}{\partial x_1 \partial x_2}}{\frac{\partial^2 G^{(s)}}{\partial x_2^2}} = 0$$
(54)

where  $G^{(s)}$  is that part of the average molar Gibbs potential of solid solutions whose second derivatives of the composition are nonzero. In our case,

$$\frac{G^{(s)}}{RT} = xy\ln(xy) + x(1-y)\ln(x(1-y)) + (1-x)y\ln((1-x)y) + (1-x)(1-y)\ln((1-x)(1-y)) + \frac{\alpha^{(s)}_{C-C'}}{RT}x(1-x) + \frac{\alpha^{(s)}_{A-A'}}{RT}y(1-y)$$
(55)

This equation yields two monovariant curves corresponding to the marginal compositions of solid solutions.

As an example, we can point to the quaternary high-temperature solubility diagram of the Ga, In, As, Sb – Pb system at 500 °C, where the field of crystallization of the Ga<sub>x</sub>In<sub>1-x</sub>As<sub>y</sub>Sb<sub>1-y</sub> solid solutions with the lattice of sphalerite has a miscibility gap.

Case III: Two series of solid solutions of the same qualitative composition with different crystal lattice structures.

A perfect example is the solubility diagram of the considered quaternary system  $K^+$ ,  $NH_4^+ ||Cl^-$ ,  $Br^- - H_2O$  at 25 °C. It consists of two bivariant fields of solid solutions that crystallize in cubic face-centered (*cfc*) and cubic (*cub*) lattices, and one monovariant curve corresponding to the crystallization of both solid solutions,  $K_x(NH_4)_{1-x}Cl_y Br_{1-y}^{(cfc)}$  and  $K_x(NH_4)_{1-x}Cl_y Br_{1-y}^{(cub)}$ .

Again, system (51) is valid for each of the fields, while the monovariant curve can be obtained by solving the system of six nonlinear equations (three for each solid solution). Alternatively, one can solve a system of three nonlinear equations with respect to the four variables corresponding to the compositions of equilibrium solid solutions,  $(x^{(cfc)} \equiv x_1, y^{(cfc)} \equiv y_1)$  and  $(x^{(cub)} \equiv x_2, y^{(cub)} \equiv y_2)$ :

$$\begin{cases} \ln SP_{\rm KCl}^{(cfc)} + \ln(x_1y_1) + \frac{\alpha_{\rm K-NH_4}^{(cfc)}}{RT} (1-x_1)^2 + \frac{\alpha_{\rm Cl-Br}^{(cfc)}}{RT} (1-y_1)^2 + \\ (1-x_1)(1-y_1) \Delta \ln SP^{(cfc)} = \\ \ln SP_{\rm KCl}^{(cub)} + \ln(x_2y_2) + \frac{\alpha_{\rm K-NH_4}^{(cub)}}{RT} (1-x_2)^2 + \frac{\alpha_{\rm Cl-Br}^{(cub)}}{RT} (1-y_2)^2 + \\ (1-x_2)(1-y_2) \Delta \ln SP^{(cub)} \\ \ln SP_{\rm KBr}^{(cfc)} + \ln(x_1(1-y_1)) + \frac{\alpha_{\rm K-NH_4}^{(cfc)}}{RT} (1-x_1)^2 + \frac{\alpha_{\rm Cl-Br}^{(cfc)}}{RT} y_1^2 - \\ (1-x_1)y_1 \Delta \ln SP^{(cfc)} = \\ \ln SP_{\rm KBr}^{(cub)} + \ln(x_2(1-y_2)) + \frac{\alpha_{\rm K-NH_4}^{(cub)}}{RT} (1-x_2)^2 + \frac{\alpha_{\rm Cl-Br}^{(cub)}}{RT} y_2^2 - \\ (1-x_2)y_2 \Delta \ln SP^{(cub)} \\ \ln SP_{\rm NH_4Cl}^{(cfc)} + \ln((1-x_1)y_1) + \frac{\alpha_{\rm K-NH_4}^{(cfc)}}{RT} x_1^2 + \frac{\alpha_{\rm Cl-Br}^{(cfc)}}{RT} (1-y_1)^2 + \\ x_1(1-y_1) \Delta \ln SP^{(cfc)} = \\ \ln SP_{\rm NH_4Cl}^{(cub)} + \ln(((1-x_2)y_2) + \frac{\alpha_{\rm K-NH_4}^{(cub)}}{RT} x_2^2 + \frac{\alpha_{\rm Cl-Br}^{(cub)}}{RT} (1-y_2)^2 + \\ x_2(1-y_2) \Delta \ln SP^{(cub)} \end{cases}$$
(56)

This system reflects the trivial fact that *cub* and *cfc* solid solutions are in equilibrium with each other regardless of their equilibrium with the saturated liquid solution.

The results of the calculation of the solubility diagram are presented in the next section.

Case IV: Two series of solid solutions of different hydrate compositions.

This case resembles the previous one. Again, system (51) is valid for each of the fields of each solid solution, and the monovariant curve can be obtained by solving the system of six nonlinear equations. However, a system of equations similar to (56) cannot be used due to the appearance of additional terms related to the solvent activity in the liquid phase (compare with Equation (43)).

Case V: Series of solid solutions on the base of a ternary compound.

An example of a system with the formation of reciprocal solid solutions based on a compound is the K<sup>+</sup>, NH<sub>4</sub><sup>+</sup>, Mg<sup>2+</sup>  $||Cl^-, Br^- - H_2O$  system at 25 °C, where potassium-ammonium-chloride-bromide carnallite (K<sub>x</sub>(NH<sub>4</sub>)<sub>1-x</sub>·MgCl<sub>2y</sub>Br<sub>2-2y</sub>·6H<sub>2</sub>O) crystallizes. The field of its crystallization is also described by a system of equations similar to (51).

# 4. Results for the Diagram of Solubility of Quaternary Reciprocal System $K^+, NH_4^+ ||Cl^-, Br^- - H_2O$ at 25 $^\circ C$

The results of the calculation of the solubility diagram of this system in comparison with the available experimental data [77] are shown in Figure 16. There is excellent agreement between the calculation and experiment. Figures 16–20 show the results of solving the system of Equation (56) with the imposition of additional conditions: isoconcentrates of cations and anions as well as water isoactivity lines.



**Figure 16.** Solubility diagram of the system  $K^+$ ,  $NH_4^+ ||Cl^-$ ,  $Br^- - H_2O$  at 25 °C in solvent-free concentration space (Janecke indexes). Gray circles denote experimental data [77], and straight segments are tie lines. The minimum of water activity is designated by black points.



**Figure 17.** Isoconcentrates of potassium ( $Y_K$ , "vertical" thin curves) and chlorine ( $Y_{Cl}$ , "horizontal" dotted curves) in the liquid phase of the K<sup>+</sup>, NH<sub>4</sub><sup>+</sup> ||Cl<sup>-</sup>, Br<sup>-</sup> – H<sub>2</sub>O system at 25 °C.



**Figure 18.** The K<sup>+</sup>, NH<sub>4</sub><sup>+</sup>  $||Cl^-, Br^- - H_2O$  system at 25 °C: water isoactivity lines (thin solid curves) in the variables of liquid phase. The dotted curves  $(A_1^{(3)} - A^{(4)} \text{ and } A^{(4)} - A_2^{(3)})$  indicate the lines of incomplete alyotropes.



**Figure 19.** Fragment of solubility diagram of the K<sup>+</sup>, NH<sub>4</sub><sup>+</sup> ||Cl<sup>-</sup>, Br<sup>-</sup> – H<sub>2</sub>O system at 25 °C: water isoactivity lines in the field of crystallization of the  $K_x(NH_4)_{1-x}Cl_y Br_{1-y}^{(cfc)}$  solid solutions in the concentration variables of the latter. The designations are the same as in Figure 18.



**Figure 20.** Fragment of solubility diagram of the K<sup>+</sup>, NH<sub>4</sub><sup>+</sup>  $||Cl^-, Br^- - H_2O$  system at 25 °C: water isoactivity lines in the field of crystallization of the K<sub>x</sub>(NH<sub>4</sub>)<sub>1-x</sub>Cl<sub>y</sub> Br<sub>1-y</sub><sup>(cub)</sup> solid solutions in the concentration variables of the latter. The designations are the same as in Figure 18.

All diagrams are shown in the Janecke coordinate system, i.e., as projections of volumetric figures on the plane of the salt components, or in other words, in the solvent-reduced (solvent-free) concentration space:

$$\begin{cases} Y_{\rm K} = \frac{m_{\rm K^+}}{m_{\rm K^+} + m_{\rm NH_4^+}} \\ Y_{\rm Cl} = \frac{m_{\rm Cl^-}}{m_{\rm Cl^-} + m_{\rm Br^-}} \end{cases}$$
(57)

where  $m_i$  denotes molalility of ion *i*, and  $m_{K^+} + m_{NH_4^+} = m_{Cl^-} + m_{Br^-}$ , according to the electroneutrality equation.

As noted above, the system contains two crystallization fields of ternary reciprocal solid solutions with cubic face-centered and cubic lattices and the monovariant curve of their cocrystallization. The monovariant curves of liquidus and solidus have extremums (minima) of water activity, i.e., there is an incomplete (or conditional) alyotrope. In the solvent-free concentration space, the figurative points of the liquid solution and both solid phases belong to the same straight line at the alyotrope point.

#### 5. Applicability of Analogues of Gibbs–Roozeboom Rules and Gibbs–Konovalov Laws to Multicomponent Systems

Second Rule (Law). As noted already, the analogue of the second law, like its prototype, is universal, and valid for systems with an arbitrary number of components in any way of changing the composition. We will not discuss it further.

#### 5.1. Motion along the Open Evaporation–Crystallization Curves at T = const and P = const

First Rule (Law). The equation of the open evaporation–crystallization process (in other words, the mass balance equation) in the condition of two-phase equilibrium (*s*–*l*) in the solvent-reduced concentration space has the form:

$$\vec{dY}^{(l)} = -(\vec{Y}^{(s)} - \vec{Y}^{(l)})dM^{(s)}$$
(58)

where  $dM^{(s)}$  is the mass of the solid solution in moles (without taking into account the solvent content), which is formed from 1 mole of liquid phase during evaporation. This means in scalar form:

$$\left(\frac{dy_i^{(l)}}{dy_j^{(l)}}\right)_{T,P,evar-cryst} = \frac{y_i^{(s)} - y_i^{(l)}}{y_j^{(s)} - y_j^{(l)}}$$
(59)

or (numbers *k* and *q* are arbitrary)

$$dy_k^{(l)} = \frac{y_k^{(s)} - y_k^{(l)}}{y_q^{(s)} - y_q^{(l)}} dy_q^{(l)}$$
(60)

As stated earlier, the van der Waals differential equation in the metric of incomplete Gibbs potential (8) and in the liquid phase variables has the form

$$(\overset{\rightarrow}{\Upsilon}^{(l)} - \overset{\rightarrow}{\Upsilon}^{(s)})\hat{G}^{[w](l)}d\overset{\rightarrow}{\Upsilon}^{(l)} = n_w^{[w](l\to s)}d\mu_w$$
(61)

Let us convert this equation to the scalar form and substitute (60):

$$-\sum_{i}\sum_{k}\left(y_{i}^{(s)}-y_{i}^{(l)}\right)\hat{G}^{[w](l)}\left(y_{k}^{(s)}-y_{k}^{(l)}\right)=n_{w}^{[w](l\to s)}\left(y_{q}^{(s)}-y_{q}^{(l)}\right)\frac{d\mu_{w}}{dy_{q}^{(l)}}$$
(62)

Since the double sum in the left part is greater than zero according to the stability criteria, and  $n_w^{[w](l \to s)}$  is less than zero according to the physical sense,

$$\left(d\mu_w/dy_q^{(l)}\right)_{T,P,evar-cryst} > 0 \text{ if } y_q^{(s)} > y_q^{(l)}$$
(63)

We proved the analogue of the first rule (law) for diagrams of solubility under the formation of solid solutions in a multicomponent (reciprocal) system:

When moving along a curve of open evaporation–crystallization in a multicomponent (reciprocal) system at constant pressure and temperature, the chemical potential of the solvent increases as the reduced (calculated without taking into account the solvent) content in the solid solution of the component—whose solventless content in the solid solution is higher than in the liquid solution—increases.

In exactly the same way, we can obtain the corresponding rules for motion along a curve of open crystallization on multicomponent (reciprocal) diagrams of fusibility and along curves of open evaporation on multicomponent diagrams of vapor–liquid.

Third Rule (Law). Let us write Equation (62) in the solid phase composition variables

$$-\sum_{i}\sum_{k}\left(y_{i}^{(l)}-y_{i}^{(s)}\right)\hat{G}^{[w](s)}\left(y_{k}^{(l)}-y_{k}^{(s)}\right) = n_{w}^{[w](s\to l)}\left(y_{q}^{(l)}-y_{q}^{(s)}\right)\frac{d\mu_{w}}{dy_{q}^{(s)}}$$
(64)

and divide one by the other. We immediately obtain

$$\left(\frac{dy_q^{(l)}}{dy_q^{(s)}}\right)_{T,P,evar-cryst} = -\frac{n_w^{[w](s\to l)}}{n_w^{[w](l\to s)}}$$
(65)

Since  $n_w^{[w](l \to s)}$  and  $n_w^{[w](s \to l)}$  always have opposite signs according to physical sense,

$$\left(dy_q^{(l)}/dy_q^{(s)}\right)_{T,P,evar-cryst} > 0 \tag{66}$$

This is an analogue of the third rule (law) for diagrams of solubility under the formation of solid solutions in a multicomponent (reciprocal) system:

Compositions of liquid and solid solutions calculated without taking into account the solvent always change in the same direction when moving along a curve of open evaporation–crystallization in multicomponent (reciprocal) system at constant pressure and temperature.

Of course, corresponding rules for motion along a curve of open crystallization on multicomponent (reciprocal) diagrams of fusibility and along curves of open evaporation on multicomponent diagrams of vapor–liquid are also valid, mutatis mutandis.

Let us illustrate the above with the solubility diagram of the K<sup>+</sup>, NH<sub>4</sub><sup>+</sup>  $||Cl^-, Br^- - H_2O$  system at 25 °C. Figure 21 shows the calculation of open evaporation curves, and Figures 22 and 23 present examples of phase diagrams when moving along such curves.

### 5.2. Motion along the Curves of Incomplete Extrema of Solvent Chemical Potential at T = const and P = const

Let us denote the belonging to the curve of incomplete extrema of the chemical potential of the solvent (or the partial pressure of the solvent) as "inex". It is known that in the quaternary system, the inex curve is a set of touch points of solvent isotherm–isobar–isopotentials by concentration sections (see Figure 24). Mathematically,

$$\begin{cases} \left(\overrightarrow{Y}^{(l)} - \overrightarrow{Y}^{(s)}\right) \widehat{G}^{[w](l)} d\overrightarrow{Y}^{(l)} = 0\\ dy_a^{(l)} = 0 \end{cases}$$
(67)

where *a* denotes the salt component of the quaternary system (the ion in the reciprocal system), which is absent in the ternary alyotrope and appears only in the incomplete quaternary pseudoalyotropes.



**Figure 21.** Isotherm–isobars of open evaporation–crystallization in the field of crystallization of the  $K_x(NH_4)_{1-x}Cl_y Br_{1-y}^{(cfc)}$  solid solutions in the K<sup>+</sup>,  $NH_4^+ ||Cl^-, Br^- - H_2O$  system at 25 °C are solid curves. Other designations are as above.



**Figure 22.** Liquidus (upper) and solidus (bottom) curves when moving along the open evaporation–crystallization curve from the point of ternary alyotrope  $A_2^{(3)}$  to the point of incomplete quaternary alyotrope  $A^{(4)}$  in the field of crystallization of the  $K_x(NH_4)_{1-x}Cl_y Br_{1-y}^{(cfc)}$  solid solutions in the K<sup>+</sup>, NH<sup>+</sup><sub>4</sub>||Cl<sup>-</sup>, Br<sup>-</sup> – H<sub>2</sub>O system at 25 °C.



**Figure 23.** Liquidus (upper) and solidus (bottom) curves when moving along the open evaporation–crystallization curve to the point of incomplete quaternary alyotrope  $A^{(4)}$  in the field of crystallization of the  $K_x(NH_4)_{1-x}Cl_y Br_{1-y}^{(cfc)}$  solid solutions in the  $K^+$ ,  $NH_4^+$ || $Cl^-$ ,  $Br^- - H_2O$  system at 25 °C.



**Figure 24.** Incomplete extrema curves in the field of crystallization of the  $K_x(NH_4)_{1-x}Cl_y Br_{1-y}^{(cfc)}$  and  $K_x(NH_4)_{1-x}Cl_y Br_{1-y}^{(cub)}$  solid solutions in the system K<sup>+</sup>, NH<sub>4</sub><sup>+</sup> ||Cl<sup>-</sup>, Br<sup>-</sup> - H<sub>2</sub>O at 25 °C are dashed lines. The dotted straight lines indicate the concentration sections.

First Rule (Law). For the curve of incomplete extrema, we can easily obtain

$$\frac{\Delta_2^{[w](l)}}{G_{22}^{[w](l)}} \left( y_a^{(s)} - y_a^{(l)} \right) = n_w^{[w](s \to l)} \left( \frac{d\mu_w}{y_a^{(l)}} \right)_{T,P,inex}$$
(68)

Since  $\left(\Delta_2^{[w](l)}/G_{22}^{[w](l)}\right) > 0$ , according to the stability criteria, and  $n_w^{[w](s \to l)} > 0$ , according to the physical sense,

$$\left(d\mu_w/dy_a^{(l)}\right)_{T,P,inex} > 0 \text{ if } y_a^{(s)} > y_a^{(l)}$$
 (69)

In other words, when moving along the inex curve in a quaternary (reciprocal) system at constant pressure and temperature, the chemical potential of the solvent increases as the reduced (calculated without taking into account the solvent) content in the solid solution of the component—which is absent in the ternary alyotrope, and appears only in the incomplete quaternary pseudoalyotropes whose solventless content in the solid solution is higher than in the liquid solution—increases.

Third Rule (Law). Again, we can rewrite Equation (68) in solid solution variables and divide these two equations by each other:

$$-\frac{G_{22}^{[w](s)}}{G_{22}^{[w](l)}} = \frac{n_w^{[w](s \to l)}}{n_w^{[w](l \to s)}} \left(\frac{y_a^{(l)}}{y_a^{(s)}}\right)_{T,P,inex}$$
(70)

and

$$\left(\frac{y_a^{(l)}}{y_a^{(s)}}\right)_{T,P,inex} > 0 \tag{71}$$

In other words, in liquid and solid solutions, the solventless content of the salt (the ion in the reciprocal system) component of the system, which is absent in the ternary alyotrope and appears only in the incomplete quaternary pseudoalyotropes, always changes in the same direction when moving along a incomplete extreme curve in a quaternary (reciprocal) system at constant pressure and temperature.

Illustrations of the rules considered are shown in Figures 25–27.



**Figure 25.** Liquidus and solidus curves when moving along incomplete extrema curve in the fields of crystallization of the  $K_x(NH_4)_{1-x}Cl_y Br_{1-y}^{(cfc)}$  and  $K_x(NH_4)_{1-x}Cl_y Br_{1-y}^{(cub)}$  solid solutions in the system  $K^+$ ,  $NH_4^+||Cl^-$ ,  $Br^- - H_2O$  at 25 °C.



**Figure 26.** Metastable liquidus and solidus curves when moving along incomplete extrema curve in the field of crystallization of the  $K_x(NH_4)_{1-x}Cl_y Br_{1-y}^{(cfc)}$  solid solutions in the system  $K^+, NH_4^+ ||Cl^-, Br^- - H_2O$  at 25 °C.

 $\mathcal{Y}_{\mathrm{K}^{+}}$ 

0.6

0.8

1.0

0.4

0.2

0.0



**Figure 27.** Metastable liquidus and solidus curves when moving along incomplete extrema curve in the field of crystallization of the  $K_x(NH_4)_{1-x}Cl_y Br_{1-y}^{(cub)}$  solid solutions in the system  $K^+, NH_4^+ ||Cl^-, Br^- - H_2O$  at 25 °C.

Again, the corresponding rules for motion along a curve of incomplete extrema on ternary (reciprocal) diagrams of fusibility and of vapor–liquid are also valid.

There are two particular points to be made about the analogues of the first and third laws in this case. First, it is impossible to formulate such analogues for those components (ions) of the system that are involved in the ternary alyotrope; Laws I and III are invalid for them. Second, it is impossible to generalize Laws I and III to arbitrary *n*-component systems ( $n \ge 5$ ).

#### 5.3. Motion along the Curves of Thermodynamic Simplification

Thermodynamic simplification curves are lines along which the chemical potentials of two of the three components (in the case of ternary systems) change by equal amounts. Mathematically,

$$D\mu_i^{(k)} = D\mu_i^{(k)}$$
(72)

where  $D\mu_i^{(k)}$  is the differential of the chemical potential of the *i*-th component of phase *k*, which takes into account changes in the concentration variables of the phase composition, but not changes of *T* or *P*. We will denote such curves as " $ts_{ij}$ ".

Let us introduce a thermodynamic simplification curve (e.g., *ts*<sub>23</sub>) in a reduced concentration space, and the incomplete Gibbs potential metric

$$d(\mu_2)_{T,P} = d(\mu_3)_{T,P} \text{ or } d(\mu_2 - \mu_3)_{T,P} = 0 \text{ or } d\left(\frac{\partial G^{[w]}}{\partial y_2}\right)_{ts_{23}} = 0$$
 (73)

We have omitted the phase index because this equation can be written in both liquid (*l*) and solid (*s*) phase variables according to the phase equilibrium conditions, i.e.,  $ts_{23}^{(l)} \equiv ts_{23}^{(s)}$ . Moreover, the last equality in (73) means that

$$G_{12}^{[w](l)}dy_1^{(l)} + G_{22}^{[w](l)}dy_2^{(l)} = 0$$
(74)

and

$$G_{12}^{[w](s)}dy_1^{(s)} + G_{22}^{[w](s)}dy_2^{(s)} = 0$$
(75)

It is worth noting that thermodynamic simplification curves, unlike, for example, incomplete extrema curves, fill the entire concentration space of the system (see Figures 28 and 29).



**Figure 28.** Curves of thermodynamic simplification  $ts_{K^+, NH_4^+}$  in solubility diagram of the quaternary reciprocal system K<sup>+</sup>, NH<sub>4</sub><sup>+</sup> ||Cl<sup>-</sup>, Br<sup>-</sup> – H<sub>2</sub>O at 25 °C in the variables of liquid phase (solid lines) and of the K<sub>x</sub>(NH<sub>4</sub>)<sub>1-x</sub>Cl<sub>y</sub> Br<sub>1-y</sub><sup>(cfc)</sup> solid solutions (dotted lines).



**Figure 29.** Curves of thermodynamic simplification  $ts_{Cl^-,Br^-}$  in solubility diagram of the quaternary reciprocal system K<sup>+</sup>, NH<sub>4</sub><sup>+</sup> ||Cl<sup>-</sup>, Br<sup>-</sup> – H<sub>2</sub>O at 25 °C in the variables of liquid phase (solid lines) and of the K<sub>x</sub>(NH<sub>4</sub>)<sub>1-x</sub>Cl<sub>y</sub> Br<sub>1-y</sub><sup>(cfc)</sup> solid solutions (dotted lines).

*First Rule (Law).* Substituting (73)–(75) into the van der Waals Equation (61) after simple transformations gives

$$n_{w}^{[w](l\to s)} \left(\frac{d\mu_{w}}{dy_{1}^{(l)}}\right)_{ts_{23}} G_{22}^{[w](l)} = \left(y_{1}^{(s)} - y_{1}^{(l)}\right) \Delta_{2}^{[w](l)}$$
(76)

where  $\Delta_2^{[w](l)} = \begin{vmatrix} G_{11}^{[w](l)} & G_{12}^{[w](l)} \\ G_{21}^{[w](l)} & G_{22}^{[w](l)} \end{vmatrix} > 0$ , according to the stability criteria of the liquid phase, and  $G_{22}^{[w](l)} > 0$  and  $n_W^{[w](l \to s)} < 0$ , according to the physical sense. So,

$$\left(d\mu_w/dy_1^{(l)}\right)_{ts_{23}} > 0 \text{ if } y_1^{(s)} > y_1^{(l)}$$
 (77)

In other words, when moving along a curve of thermodynamic simplification in a quaternary (reciprocal) system, the chemical potential of the solvent increases as the reduced (calculated without taking into account the solvent) content in the solid solution of the component—whose solventless content in the solid solution is higher than in the liquid solution if such a component does not participate in the condition of thermodynamic simplification—increases.

Third Rule (Law). In exactly the same way as above, we obtain

$$\left(\frac{dy_1^{(s)}}{dy_1^{(l)}}\right)_{ts_{23}} = -\frac{G_{22}^{[w](s)}}{G_{22}^{[w](l)}} \frac{\Delta_2^{[w](l)}}{\Delta_2^{[w](s)}} \frac{n_w^{[w](s\to l)}}{n_w^{[w](l\to s)}} > 0$$
(78)

In other words, when moving along a curve of thermodynamic simplification in a quaternary (reciprocal) system, the content of component—which does not participate in the condition of thermodynamic simplification—changes in liquid and solid solutions in the same direction.

Illustrations of these rules are shown in Figures 30 and 31.



**Figure 30.** Metastable liquidus and solidus curves when moving along a thermodynamic simplification curve in the field of crystallization of the  $K_x(NH_4)_{1-x}Cl_y Br_{1-y}^{(cfc)}$  solid solutions in the system  $K^+, NH_4^+ ||Cl^-, Br^- - H_2O$  at 25 °C. Incomplete quaternary pseudoalyotrope is denoted as  $A^{(4)}$ .



**Figure 31.** Metastable liquidus and solidus curves when moving along a thermodynamic simplification curve in the field of crystallization of the  $K_x(NH_4)_{1-x}Cl_y Br_{1-y}^{(cfc)}$  solid solutions in the system  $K^+, NH_4^+ ||Cl^-, Br^- - H_2O$  at 25 °C. Incomplete quaternary pseudoalyotrope is denoted as  $A^{(4)}$ .

The following is important:

One cannot formulate analogues of Laws I and III for those components that are involved in the thermodynamic simplification condition;

One cannot extend these laws to more component solubility diagrams.

#### 6. Conclusions

Isobaric fusibility diagrams of binary systems with solid solutions in variables "temperature–composition", liquid–vapor diagrams of binary systems (in variables "temperature–composition" at constant pressure or in variables "pressure–composition" at constant temperature), and solubility diagrams of ternary systems with solid solutions in variables "chemical potential (or activity) of solvent–Janecke indexes of dissolved components" at *T*, *P* = const are topologically isomorphic.

This isomorphism is a consequence of the complete isostructurality of the systems of differential van der Waals phase equilibrium shift equations in correspondingly binary and ternary systems under the specified conditions and concentration variables.

All of the aforementioned phase diagrams are governed by Gibbs–Konovalov laws and Gibbs–Roozeboom rules or their analogues.

The mentioned topological isomorphism can be extended to the fusibility diagrams of ternary systems with solid solutions, liquid–vapor diagrams of ternary systems, and solubility diagrams of the quaternary systems with solid solutions if the composition of one of the equilibrium phases changes along the following monovariant curves: open evaporation or crystallization, partial extrema, thermodynamic simplification. In these cases, analogues of Gibbs–Konovalov laws and Gibbs–Roozeboom rules are also valid.

In the case of composition changes along the monovariant curves of open phase processes (open evaporation and/or crystallization) in systems with an arbitrary number of components, there also is the isomorphism of different types of phase diagrams and governance of the latter by analogues of Gibbs–Konovalov laws and Gibbs–Roozeboom rules.

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