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# Partial Discharge Measurements in a High Voltage Gas Insulated Transmission Line Insulated with CO<sub>2</sub>

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**Abstract:** This paper uses practical experimentation to analyse the effect of replacing SF<sub>6</sub> with pure CO<sub>2</sub> in conventional gas insulated transmission line sections by studying partial discharge measurements taken with applied voltages up to 242 kV (rms). The results can also help in understanding the properties of new alternative gas mixtures which can be utilised with a ratio of up to and over 95% CO<sub>2</sub>. The experiments undertaken involved filling a gas insulated line demonstrator with 3 bars of CO<sub>2</sub> and applying voltages up to 242 kV in both clean conditions and particle-contaminated enclosure conditions. The results demonstrate that CO<sub>2</sub> can be used to insulate gas equipment without breakdown at high voltage, however, a higher gas-filling pressure may be needed to reduce the partial discharge found in the tests presented in this paper. Another aspect of the work showed that partial discharge (PD) measurements from internal ultra-high frequency (UHF) sensors compared with a direct measurement from a capacitive divider both clearly showed the effect of contaminating particles in CO<sub>2</sub>. However, the PD divider measurements also showed considerable external PD on the outside of the gas compartment, leading to the conclusion that UHF sensors are still regarded as having the highest sensitivity and noise immunity for gas insulated switchgear (GIS) or gas insulated transmission line (GIL) systems including when the equipment is insulated with CO<sub>2</sub>.

**Keywords:** gas insulated transmission lines (GILs); partial discharge (PD); sulphur hexafluoride (SF<sub>6</sub>), carbon dioxide (CO<sub>2</sub>); ultra high frequency (UHF) sensors

## 1. Introduction

The use of gas insulated busbars (GIB) and transmission lines (GIL) is common practice within the high voltage power industry when insulated with compressed sulphur hexafluoride (SF<sub>6</sub>) gas to enable compact electrical substations and transmit large amounts of energy across large distances or in urban locations or hard-to-reach areas such as underground river crossings that overhead power lines may not be able to facilitate. The use of SF<sub>6</sub> is increasing in the UK [1] and is facing growing scrutiny considering that it is a global warming gas with an estimated global warming potential of 23,500 times that of carbon dioxide (CO<sub>2</sub>) and an atmospheric lifetime of 3200 years, making it one of the most detrimental global warming gases known to humankind when released into the atmosphere [2,3]. Current research efforts are focusing on the replacement of SF<sub>6</sub> with alternatives such as C<sub>4</sub>F<sub>7</sub>N [4,5], C<sub>5</sub>F<sub>10</sub>O [6,7] and CF<sub>3</sub>I [8,9] in relatively small mixture quantities (1–30%) as a partial pressure gas mixture with large quantities of CO<sub>2</sub> (up to 95%) as a buffer gas making up a component gas mixture of two or three gases. It is, therefore, important that the partial discharge characteristics within high voltage gas insulated transmission lines (GIL), busbars and gas insulated switchgear (GIS) are studied in order to ensure accurate diagnostic measurement useful for the replacement of SF<sub>6</sub>

with a component gas mixture largely consisting of CO<sub>2</sub> or pure CO<sub>2</sub>. Additional beneficial research, connected to the trials of CO<sub>2</sub> as an insulation medium, in small vessels to understand streamer and breakdown characteristics has been conducted by [10] and the partial discharge (PD) inception and breakdown voltages studied at high pressure of a model spacer in [11]. This paper examines the use of non-conventional PD measurements directly coupled using a capacitive divider connected to the studied GIL and compared to conventional ultra-high frequency (UHF) sensors.

Partial discharge is primarily used as an indication of equipment degradation, detecting the state of insulation performance of the system as a whole and a method, in this research, of assessing the use of CO<sub>2</sub> as a direct replacement for SF<sub>6</sub> in practical GIB and GIL. It is also useful to note that studying the effects of pure CO<sub>2</sub> is beneficial considering that the alternative mixtures have gases that degrade over time, leading to a change in mixture ratio during an equipment's lifetime, or in the case of fault conditions, where some arcing occurs or continuous partial discharge affects the gas ratio [12]. The use of CO<sub>2</sub> in gas insulated equipment on high voltage networks, if highly widespread in the future, could prove to be a sustainable way to offset carbon emissions and use waste production of CO<sub>2</sub> from other processes in order to capture and usefully store otherwise emitted global warming gases.

## 2. Practical Test Arrangement and Methods

During the practical experimentation undertaken in this paper, full-scale gas insulated equipment, designed to be utilised with SF<sub>6</sub> as an insulation medium at a rated voltage of 420 kV on the UK network, was used to build the demonstrator shown in Figure 1 in the high voltage laboratory at Cardiff University. The normal operating conditions of this equipment when insulated with a minimum filling pressure of 2.9 bar of SF<sub>6</sub> are shown in Table 1. The voltage ratings shown in Table 1 are consistent with IEC 62771-203 equipment ratings for high voltage gas insulated equipment [13].

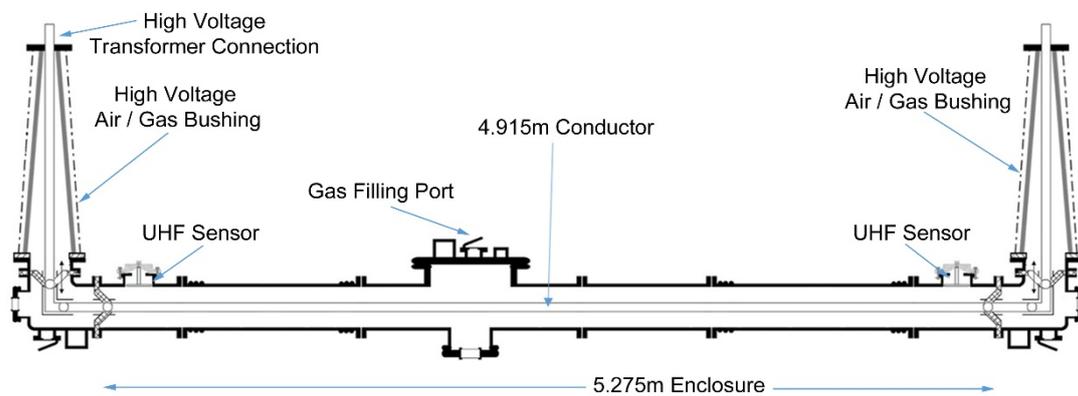
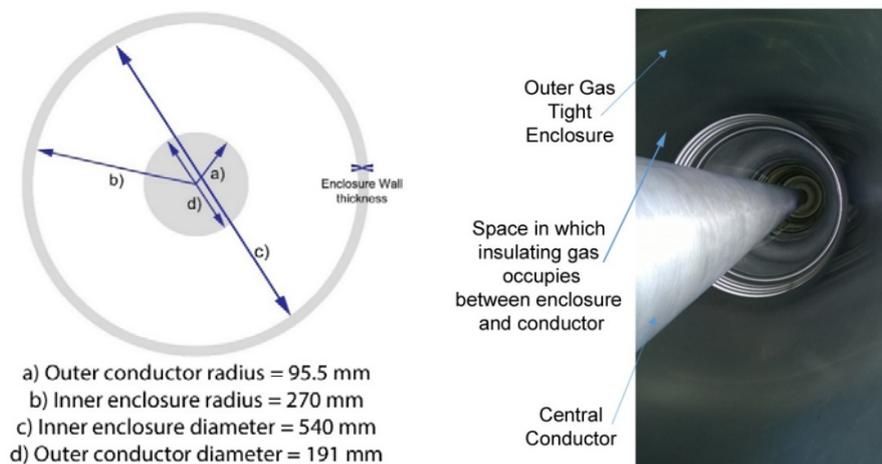


**Figure 1.** Gas insulated line demonstrator constructed and installed at Cardiff University.

The gas insulated line demonstrator was constructed of the sections shown in Figure 2, with connecting elbow joints either end allowing the use of two high voltage bushings. The central gas zone consisted of a 4.915 m central conductor suspended between two epoxy resin cone spacers which seal the gas zone at both ends. This central section of the gas insulated line demonstrator also contains two UHF capacitive plate sensors at both ends of the GIL section and is equipped with a gas-filling port. The outer enclosure length of this section is 5.275 m in length. The dimensions of the outer conductor and inner enclosure of the constructed gas insulated line demonstrator are shown in Figure 3.

**Table 1.** Specifications of the gas insulated demonstrator at Cardiff when filled with pure SF<sub>6</sub> [13].

Specification	Abbreviation	IEC 62271-203 (2003) Equipment Rating
Rated voltage/rated frequency	Ur/fr	420 kV/50 Hz
Power frequency withstand voltage	Ud	650 kV
Lightning impulse withstand voltage	Up	1425 kV
Switching impulse withstand voltage	Us	1050 kV
Rated auxiliary voltage	Ua	125 V d.c.
Nominal current—busbars and bays	Ir	4000 A
Short-time withstand current/duration	Ik/tk	63 kA/1 s
Peak withstand current	Ip	157 kA
CB SF <sub>6</sub> gas pressure: filling/alarm/minimum (at 20 °C)	Pre/Pae/Pme	7.5/6.8/6.5 bar
GIS SF <sub>6</sub> gas pressure: filling/alarm/minimum (at 20 °C)	Pre/Pae/Pme	3.5/3.1/2.9 bar

**Figure 2.** Gas insulated line demonstrator sections and dimensions.**Figure 3.** Gas insulated line inner conductor and outer enclosure dimensions.

Considering that the gas insulated line demonstrator has an outer conductor diameter of 191 mm and an inner enclosure diameter of 540 mm it can be calculated that the outer conductor radius ( $R_a$ ) is 95.5 mm and the inner enclosure radius ( $R_b$ ) is 270 mm. Using the dimensions shown in Figure 3, it can be verified that the dimensions are close to the desired theoretical values, as is normally considered when designing gas insulated equipment in order to create a near-uniform electric field distribution which helps the insulation performance of the insulating gas under applied voltage conditions:

$$\ln\left(\frac{R_b}{R_a}\right) = \ln\left(\frac{270}{95.5}\right) = 1.039 \quad (1)$$

$$\ln\left(\frac{R_b}{R_a}\right) = 1 \quad \text{is the ideal} \quad (2)$$

Considering the IEC/BS EN standard 62771-203 [13] and 62271-204 [14], which recommend the same method for partial discharge detection for both gas insulated transmission lines and switchgear, the test voltages shown in Table 2 were used for practical testing to show system rating voltage responses. To conform with the standards, a pre-stress voltage would normally be applied before a PD measurement is taken. However, in these experiments, this was not possible due to the available transformer rating limitations. For a system with a solidly earthed neutral, the applied test voltage for partial discharge measurement ( $U_{pd-test}$ ) to a single-phase enclosure design, such as the gas insulated line demonstrator used in this work, is calculated using the following equation [13] and applied for any time greater than 1 min:

$$U_{pd-test} = 1.2 U_r / \sqrt{3} \quad (3)$$

**Table 2.** Gas insulated line demonstrator partial discharge test voltage levels.

Gas Insulated Line Demonstrator Rated Voltage	$U_r$ Nominal System Phase to earth Voltage	$U_{pd-test}$ Test Voltage for PD Measurement $U_{ph-test} (>1 \text{ min})$
300 kV	173 kV	208 kV
362 kV	209 kV	251 kV
400 kV	231 kV	277 kV
420 kV	242 kV <sup>1</sup>	291 kV

<sup>1</sup> Maximum applied voltage achieved during practical testing was 242 kV due to external PD.

It is also important to note that, as described in [13,14], the maximum permissible partial discharge level is 5 pC at the voltages specified in Table 2. However, in these experiments, an oil-filled transformer was used to apply the voltage, which means that the system as a whole may be considered acceptable if the discharge level does not exceed 10 pC, as the PD of the transformer is included in the measured result.

Using the IEC/BS EN 60270 for high voltage partial discharge test techniques [15], the upper ( $f_1$ ) and lower frequency ( $f_2$ ) limits of the wide band partial discharge equipment (coupled to the high voltage capacitive divider capacitors or power separation filter), as determined suitable for high voltage equipment, can be set as follows:

$$30 \text{ kHz} \leq f_1 \leq 100 \text{ kHz} \quad (4)$$

$$f_2 \leq 1 \text{ MHz} \quad (5)$$

$$100 \text{ kHz} \leq f_2 \leq 900 \text{ kHz} \quad (6)$$

For the following practical tests, the measurement system (Omicron MPD 540) shown in Figure 4a was set to the following values:

$$f_1 = 30 \text{ kHz}, f_2 = 130 \text{ kHz},$$

$$\text{Frequency integration} = 80 \text{ kHz} \pm 50 \text{ kHz}.$$

These values were set using a trial and error method which identifies the frequency range that can be used without including specific noise or outside interference detected by the system in and around the laboratory.

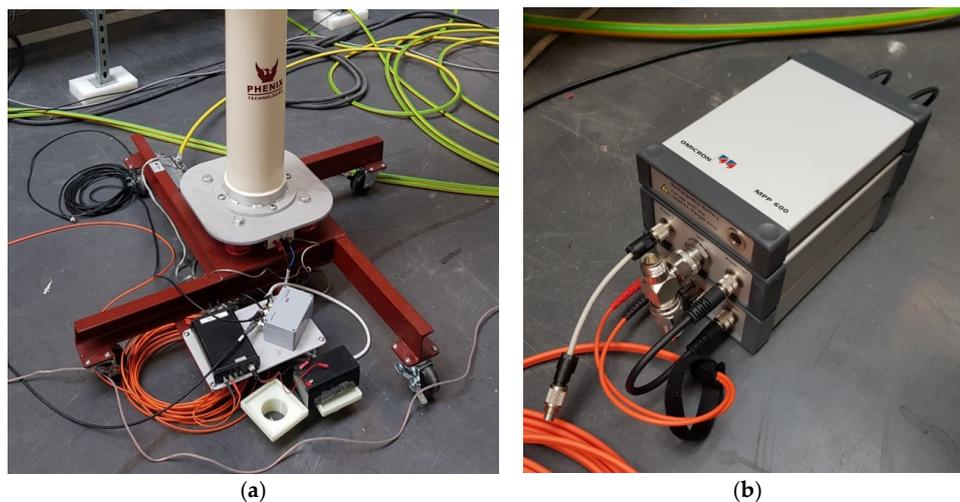
Figure 4b shows the signal conditioning used to couple the UHF sensors to the PD measurement system (Omicron UHF 620 and MPD 600). While the bandwidth of the UHF sensor is in the range of 2 GHz, measurements were converted to a lower frequency range for compatibility with the phase

resolved analysis system (the results of which are shown in Section 3). The recorded frequency range of this apparatus was as follows:

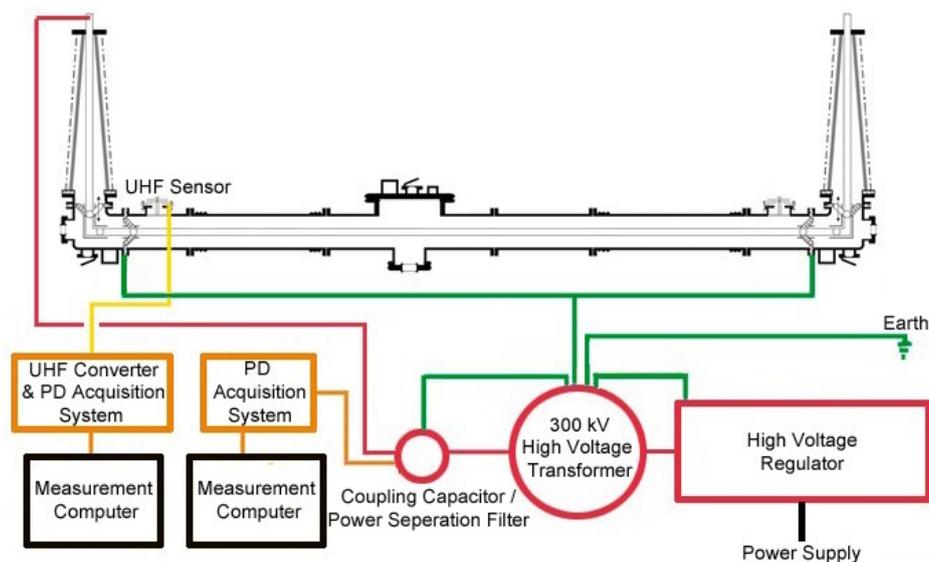
$$f_1 = 399.3 \text{ MHz}, f_2 = 400.8 \text{ MHz},$$

$$\text{Frequency integration} = 400 \text{ MHz} \pm 750 \text{ kHz}.$$

The arrangement of all equipment used to carry out the practical tests undertaken in this paper are shown in Figure 5. The gas insulated demonstrator was filled with 3 bar of CO<sub>2</sub>, with a technical specification of 99.8% CO<sub>2</sub> [16]. The gas insulated demonstrator was tested as both a clean system and as a particle-filled system with 10 × 1 mm diameter stainless steel spheres placed as free floating particles within the central gas insulated enclosure [17].



**Figure 4.** (a) Optically isolated partial discharge (PD) equipment coupled to a coupling capacitor of 1 nF or power separation filter; (b) ultra high frequency (UHF) capacitive sensor coupled with optically isolated PD measurement equipment.



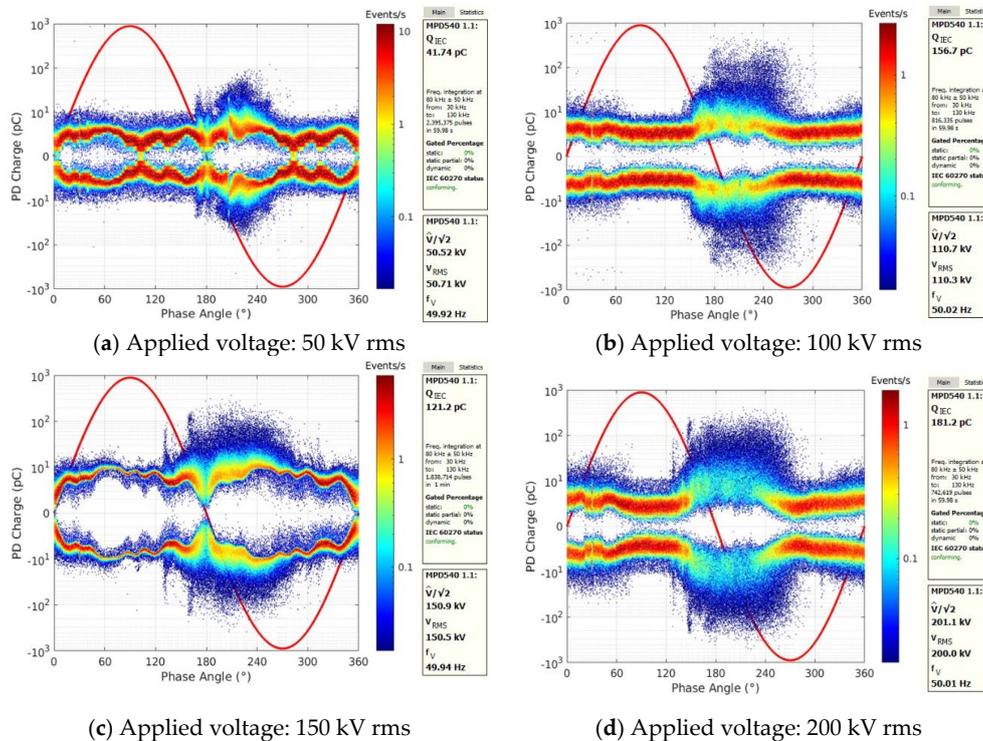
**Figure 5.** Practical test arrangement including gas insulated line demonstrator, partial discharge acquisition equipment, measuring computers and high voltage transformer.

### 3. Results

This section gives a description of the experimental results for both the clean gas insulated line demonstrator filled with pure CO<sub>2</sub> and a system with artificial particle contamination to show their effects on PD measurements and CO<sub>2</sub> insulation.

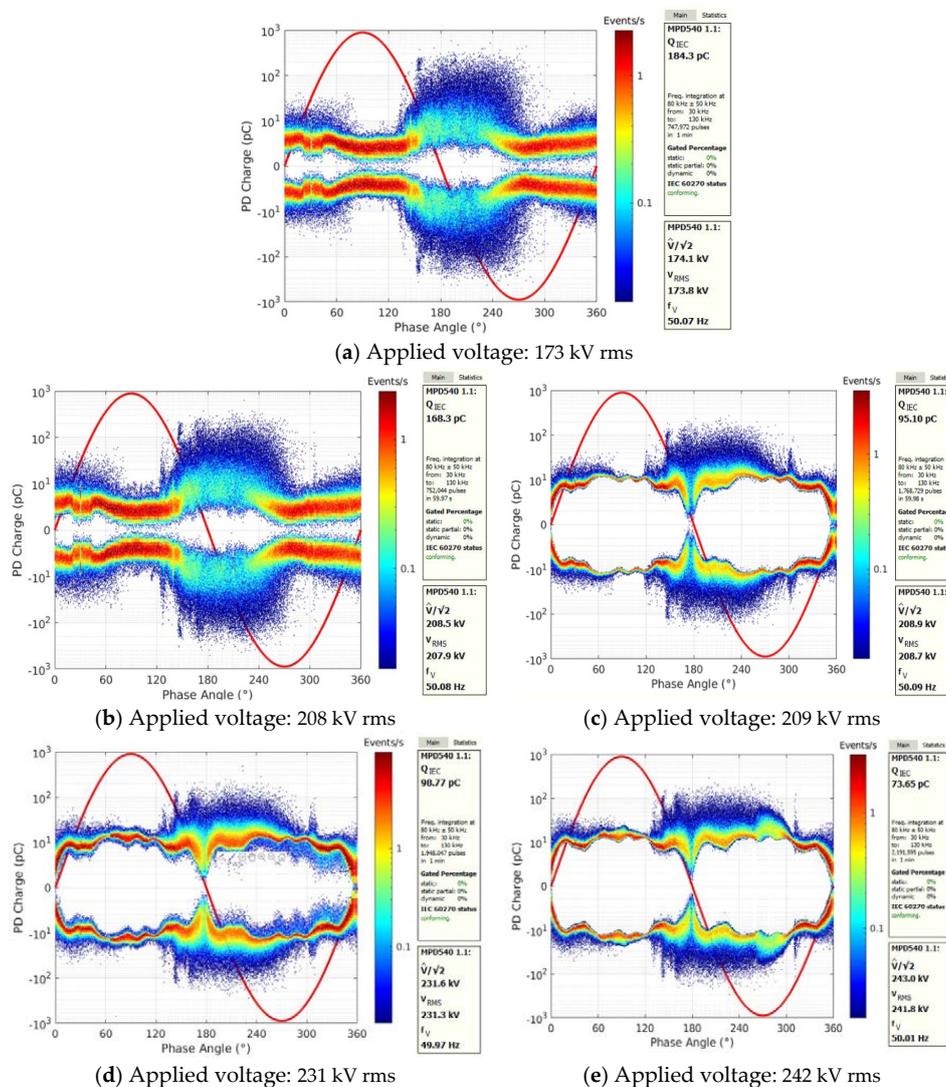
#### 3.1. Partial Discharge Measurement—Clean System

The first experimental tests undertaken using the gas insulated line demonstrator, filled with 3 bars of CO<sub>2</sub>, are shown in Figure 6 at applied AC voltages of 50 kV, 100 kV, 150 kV and 200 kV (rms). The PD measurements shown in Figure 6 are representative of the full system including the AC oil-filled transformer, the CO<sub>2</sub> gas-filled bushings and the central section of the gas insulated line when measured using the coupling capacitor directly connected to the AC voltage transformer. The results indicate that the system as a whole has a peak apparent charge of approximately 10 pC but as the voltage was increased, a PD level up to 100 pC can be seen. It was found that the largest PD signals, occurring at approximately the 3rd quadrant of the AC waveform, were largely a result of external PD around the outside of one of the air bushings at the end of the gas insulated line demonstrator. The end of the bushing was approximately 1.5 m away from the external wall of the lab and hence the PD generated could not be reduced. This external PD was found to occur at the connection point of an air bushing and was located using a UV camera that is capable of detecting corona in daylight. The rest of the AC cycle shows lower PD levels averaging less than or approximately 10 pC, even though this gas insulated equipment is filled with CO<sub>2</sub> instead of SF<sub>6</sub> which has a much higher dielectric strength. It also shows that, even though the equipment is filled to 3 bar of CO<sub>2</sub>, which is 0.5 bar below the normal filling pressure of this equipment when filled with SF<sub>6</sub> and close to the minimum allowed pressure of the equipment when in service, this pressure of CO<sub>2</sub> is still able to insulate the equipment up to 200 kV rms.



**Figure 6.** PD measurement of a gas insulated line demonstrator filled with 3 bar CO<sub>2</sub>—clean system—measured directly with the high voltage divider coupling capacitor at applied rms voltages of (a) 50 kV, (b) 100 kV, (c) 150 kV, and (d) 200 kV. Close investigation of the PD measurement indicated that high activity regions in the 1st and 3rd quadrants were found to be external discharges around the connecting air bushings.

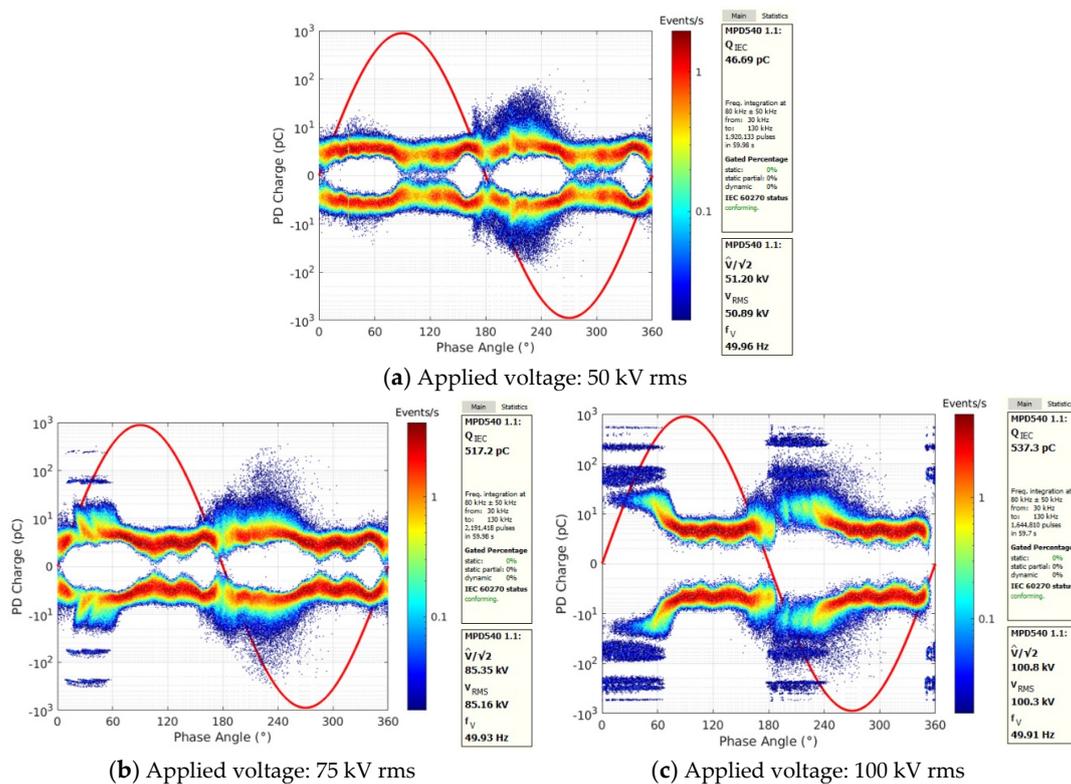
PD measurements were also undertaken for the gas insulated line demonstrator filled with 3 bar CO<sub>2</sub> at the phase-to-earth system voltages and the calculated PD measurement voltage shown in Table 2. The maximum permissible voltage applied to the demonstrator was 242 kV due to external PD on the outside of the air insulated bushing. This meant that the tests, shown in Figure 7, were able to demonstrate the performance of the clean system at a rated line voltage of 300 kV rms using the phase-to-earth voltage of 173 kV rms and the PD measurement voltage of 208 kV rms. For the other rms voltage ratings of 362, 400 and 420 kV, the tests undertaken demonstrated the performance of the clean gas insulated line at the phase-to-earth voltage ratings only of 209, 231 and 242 kV, respectively, as shown in Figure 7, and could not be performed at the PD measurement voltage level. The results show that the gas insulated line filled with CO<sub>2</sub> at 3 bar can insulate the conductor to the enclosure gas gap distance without a breakdown of the gas at 242 kV rms. However, there is still significant and increasing external PD from the outside of the air bushing centered at approximately 200° of the AC waveform. The results also seem to show that additional PD artefacts appear outside the 125–285° window, with a potential area of partial discharge activity located approximately around 300° from 208 kV onwards. This PD activity is indicative of external PD such as corona or surface discharge, it could be across the surface of the cone insulating spacer, but is likely to be a continuation of the external PD seen at lower voltages.



**Figure 7.** PD measurement of a gas insulated line demonstrator filled with 3 bar CO<sub>2</sub>—clean system—measured directly with a HV coupling capacitor for shown system rms voltages.

### 3.2. Partial Discharge Measurement—Particle-Contaminated System

In the next set of tests, ten  $\times$  1 mm diameter stainless steel spheres [17] were placed inside along the whole length of the central enclosure of the gas insulated line demonstrator in order to simulate the effect of metal particles and the type of PD pattern these may cause in a gas insulated line filled with CO<sub>2</sub> instead of SF<sub>6</sub>. Figure 8 shows the PD results for applied rms voltages of 50, 75 and 100 kV to the system with the presence of particle contamination. The PD measurements of the particle-contaminated gas insulated line at 3 bar CO<sub>2</sub> were achieved using the high voltage arm of a divider as the coupling capacitor. The effect of the particles on the system, shown in Figure 8a, can be compared to the clean system in Figure 6a, and there was a negligible amount of PD on the rising half of the positive AC cycle but otherwise little difference. In Figure 8b, the system contaminated with particles at 75 kV is shown, and considerable PD was detected on the rising half of the positive AC cycle. In Figure 8c, the voltage applied to the contaminated gas insulated line was increased to 100 kV, and it can be observed that there is significant PD in the measured PD frequency range on both rising edges of the positive and negative cycles of the AC waveform. It is likely that the measurements appear as clusters at certain orders of magnitude because of a capacitive effect, likely due to the particles bouncing on the inside of the enclosure of the gas insulated line section but not as free-floating particles, as explained in the next section on UHF measurements.

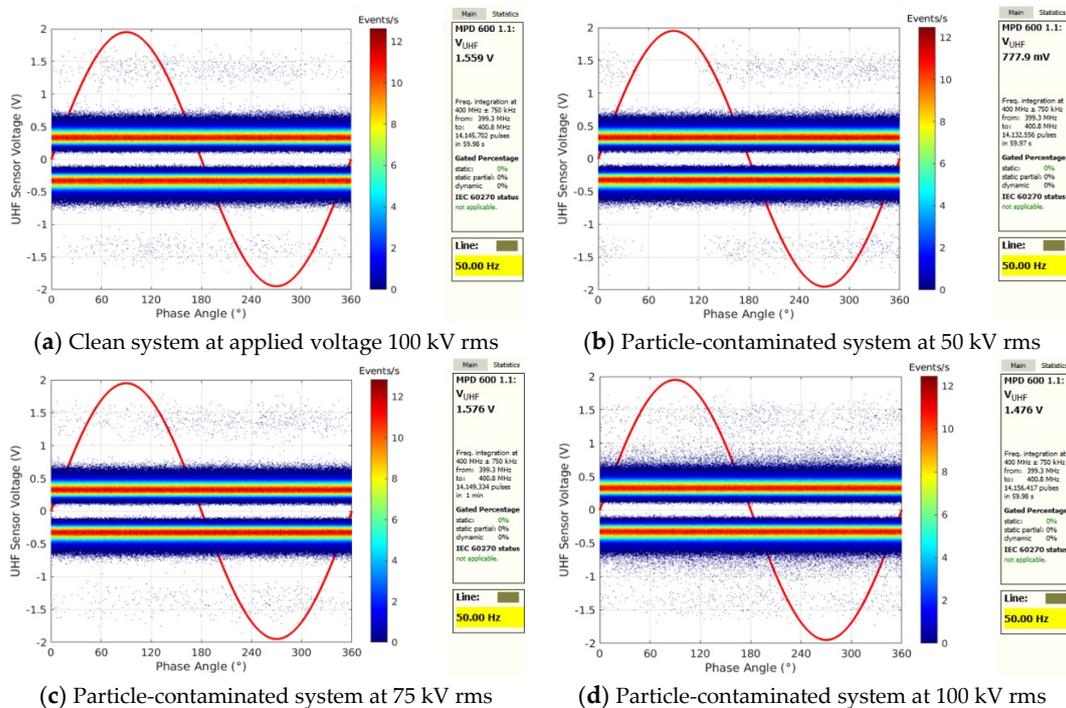


**Figure 8.** PD measurement of the gas insulated line demonstrator filled with 3 bar CO<sub>2</sub>—particle-contaminated system—measured directly with a HV coupling capacitor.

### 3.3. UHF Partial Discharge Measurement—Clean and Particle-Contaminated System

During experimentation with the gas insulated line, measuring partial discharge with a wide band measurement system coupled with the HV arm of a divider as the coupling capacitor directly to the transformer, significant effects of PD external to the test GIL were observed. Therefore, it was decided to utilise the UHF sensor signals in order to mitigate some of the effects arising from external PD as seen in Figures 6–8. In order to obtain UHF measurements, a capacitive plate sensor was placed within the enclosure of the gas insulated line. This was then attached to a device which lowers the

bandwidth and allows for direct recording from the higher frequency UHF sensor at the same time as the HV arm of a divider with coupled capacitive measurements, as shown in Figure 8. UHF data from the gas insulated line demonstrator as a clean system filled with 3 bar CO<sub>2</sub> with an applied voltage of 100 kV is shown in Figure 9a.



**Figure 9.** PD measurement of a gas insulated line demonstrator filled with 3 bar CO<sub>2</sub> measured using a capacitively coupled UHF sensor.

When the results of the UHF measurements for the clean system, shown in Figure 9a, are compared with the results of the contaminated system in Figure 9 (b) 50 kV, (c) 75 kV and (d) 100 kV, it can be seen that the measured PD with the presence of metallic particles is visible between the system background noise and the PD level shown above 1.25 V. In Figure 9d, the effect of the PD caused by the metal particles is the most visible when compared to Figure 9a, which is the clean system at the same 100 kV applied voltage. The particle-contaminated system shows much more recorded PD just above the background noise of the system and before 1.25 V, whereas the clean system PD recordings have a clear gap between the background PD and the PD above 1.25 V. This repetitive pattern is not consistent with those of free conducting particles in gas insulated equipment where a particle becomes charged by induction under the influence of the power-frequency electric field, this particle then lifts off as the induced charge overcomes the particles weight. Eventually, a free floating particle discharges as charge is exchanged between the particle and the enclosure. Following this, the particle falls and bounces on the enclosure and the sequence may repeat [18]. At the peak of the AC wave, the electric field is highest, so free particles will gain the highest charge which proportional to the value of voltage at that point and so the PD pattern shape will form an envelope inside the AC wave, as shown in [19]. The observed PD patterns shown in Figure 9 are consistent with the expected behaviour of free metallic particles in SF<sub>6</sub> insulated GIL free motion, where particles bounce on the outer enclosure of a section [20]. Bouncing particles on the enclosure do not form an AC wave envelope as a particle does during liftoff but rather PD across all phase angles, which is similar to those seen in the findings in this paper. This would be considered a more severe discharge than particles at a pre-liftoff stage of motion, where PD amplitudes tend to be enveloped by the shape of the AC reference wave. This also indicates that the particles measured in Figure 9d are bouncing on the inner enclosure of the gas insulated line demonstrator at an

applied voltage of 100 kV rms but do not present a deleterious threat to the insulation system at these voltages unless they become trapped in the spacer–chamber junction. The noise immunity and density of UHF measurements are evident in the system’s ability to detect and identify these low-amplitude discharges despite external effects on the connecting equipment.

#### 4. Discussion and Conclusions

This research demonstrates the use of pure CO<sub>2</sub> as an insulation medium in high voltage gas insulated equipment including transmission lines and switchgear, and it could also potentially be useful in benchmarking the PD characteristics and phase-resolved partial discharge (PRPD) patterns of future gas insulation mixtures that are currently being trialed to replace SF<sub>6</sub>, as many of these consist of high ratios of CO<sub>2</sub>. The experimentation undertaken shows the effectiveness of pure CO<sub>2</sub> to insulate high voltage equipment, previously designed for use with SF<sub>6</sub>, up to a voltage of 242 kV rms. However, it is possible to conclude that this system likely has more partial discharge than the same system insulated with SF<sub>6</sub> at the same pressure. It is also likely that increasing the total filling pressure of CO<sub>2</sub> may improve the system’s PD performance when compared to the results presented in this paper, including its use at voltages greater than 242 kV rms. It was demonstrated that a capacitively coupled PD measurement through a divider’s HV capacitors can show bouncing particles in gas insulated equipment as well as UHF. The results confirm the usefulness of an internal UHF sensor to mitigate external noise effects from system PD, demonstrating that it is an effective tool for continued use in this type of application. Future research will determine the PD system response of other natural atmospheric gases filled in conventional high voltage gas insulated equipment including increased pressure ratings.

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