

Review

Techno-Economic Analysis of Hydrogen Storage Technologies for Railway Engineering: A Review

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Abstract: According to the specific requirements of railway engineering, a techno-economic comparison for onboard hydrogen storage technologies is conducted to discuss their feasibility and potentials for hydrogen-powered hybrid trains. Physical storage methods, including compressed hydrogen (CH₂), liquid hydrogen (LH₂), and cryo-compressed hydrogen (CcH₂), and material-based (chemical) storage methods, such as ammonia, liquid organic hydrogen carriages (LOHCs), and metal hydrides, are carefully discussed in terms of their operational conditions, energy capacity, and economic costs. CH₂ technology is the most mature now but its storage density cannot reach the final target, which is the same problem for intermetallic compounds. In contrast, LH₂, CcH₂, and complex hydrides are attractive for their high storage density. Nevertheless, the harsh working conditions of complex hydrides hinder their vehicular application. Ammonia has advantages in energy capacity, utilisation efficiency and cost, especially being directly utilised by fuel cells. LOHCs are now considered as a potential candidate for hydrogen transport. Simplifying the dehydrogenation process is the important prerequisite for its vehicular employment. Recently, increasing novel hydrogen-powered trains based on different hydrogen storage routes are being tested and optimised across the world. It can be forecasted that hydrogen energy will be a significant booster to railway decarbonisation.

Keywords: hydrogen; storage technology; techno-economic analysis; railway engineering



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1. Introduction

Long-term extensive use of fossil fuels contributes to increasingly severe environment problems. Nowadays, deep decarbonisation has become a topical issue all over the world. Carbon neutral plans have been made by worldwide nations and organisations to reduce greenhouse gas (GHG) emissions and slow global warming [1–4].

Recently, the transportation sector consumed about 57 Mtoe (over 33% of the whole energy consumption) every year in the UK [5,6]. As an important component of transportation, rail transport is looking at options to replace its diesel-powered trains against the background of climate change and the need for fast and consistent decarbonisation of the entire energy system [7]. Major investment plans are underway to install and upgrade railway electrification to pave the way for a cleaner future for the railway industry [8]. Rail electrification provides numerous benefits including quicker and quieter journeys, increased capacity, and being more environmentally friendly. However, it requires giant infrastructure construction at a significant cost. For the remote routes where electrification is not economically viable, hydrogen and fuel cell technology offer complimentary sources of traction. Meanwhile, it enables trains with higher power, faster refuelling, and long endurance [9,10].

The first hydrogen-powered locomotive was developed, designed, and demonstrated in America in 2002 [7]. Its onboard hydrogen storage system is based on metal hydrides technology. A seven-year project beginning in 2003, aiming to apply hydrogen to rail heavy haul industry, was jointly conducted by America and Japan [11]. The power system of

the target locomotive includes 250 kW fuel cell stacks and 1250 kW batteries. Afterwards, Japan trialled a rail car during 2006 to 2007, which used 35 MPa CH₂ storage technology. Then, two rail cars equipped with CH₂ tanks, powered by 120 kW PEMFC and 36 kWh auxiliary batteries, continued to be tested in Japan [12].

An increasing number of hydrogen-powered trains have been put into operation in recent years. South Africa launched the world's first fuel cell-powered mining locomotive in 2012 [13]. A hydrogen-powered rail tram began to be tested from the same year in Chengdu, China, and was then put into service in 2014 [14]. On 16 September 2018, Coradia Iliint [15], manufactured by Alstom, entered service in Germany, with hydrogen storage tanks placed at the top of carriages. It has been operated on a 100 km route from Cuxhaven to Buxtehude. The UK's first hydrogen-powered train, named 'HydroFLEX' [16], was jointly developed by University of Birmingham and Porterbrook Co. It was unveiled in 2019, successfully received a mainline run in 2020, and was showcased at COP26, Glasgow, in 2021. China's first hydrogen fuel cell hybrid locomotive started trial runs for coal transport in October 2021. It announced that it was able to reduce carbon emissions by 80 kg/km per 10,000 tons' load compared with traditional diesel-powered locomotives. Researchers from East Japan Railway also tested and optimised their H₂ train, named HYBARI [17]. They installed the whole traction equipment under the floor and realised the downsizing of the power system.

Developing high-density hydrogen storage technologies with acceptable cost and reliable security is always the key issue for hydrogen-powered vehicles [18,19]. At present, hydrogen storage technologies can be catalysed into two main groups. The first category is physical storage methods, including compressed gas hydrogen (CH₂), cold-compressed hydrogen, liquid/cryogenic hydrogen (LH₂), and cryo-compressed hydrogen (CCH₂). Another group is material-based (chemical) storage, including adsorption and absorption. Several storage technologies have been tested for onboard power systems and have shown their different characteristics. CH₂ storage technology [20–22] is the most well-established now, whose normal storage pressures are 35 MPa and 70 MPa. Its gravimetric and volumetric density can achieve 5.5 wt% and 3.6 MJ/L, respectively, but it still does not reach the final targets set by DOE (Department of Energy, America). Storage capacity of LH₂ and CCH₂ is close to the target, and they are regarded as the potential technologies to achieve the goals [18,23–25]. Nevertheless, due to unavoidable heat leakage, LH₂ cannot be stored without loss for a long time. Liquefaction and a high standard for insulation also raise its energy consumption during production and raise the total cost of ownership for vehicles. CCH₂ combines the advantages of long dormancy time from CH₂ and high storage density from LH₂. Low technology maturity and infrastructure to be constructed slows its large-scale onboard application. Intermetallic compounds [26] are used in many industry areas but their low hydrogen storage capacities (<2 wt%), slow kinetics, and complicated activation procedures make them hard to be vehicle-mounted hydrogen carriers. In contrast, complex hydrides [27] overcome the drawback on the storage capacities, but it is necessary to lower their operating conditions before onboard use. Similarly, chemical hydrides and magnesium-based alloys [28–30] have favourable hydrogen storage capacities. However, chemical hydrides are irreversible, which means it is difficult to refuel them quickly. Mg-based alloys have poor thermodynamic and kinetic properties, increasing the difficulty of their dehydrogenation process. Ammonia catches increasing attention now for its high hydrogen capacity and relatively convenient storage. Moreover, it can be utilised through three ways, direct combustion, fuel cells (after dehydrogenation and purification), and direct fuel cells. Diversified utilisation methods mean that ammonia can adapt to different industrial demands and transportation requirements [31,32]. Liquid organic hydrogen carriers (LOHCs) are discussed a lot for hydrogen transportation because of their large hydrogen storage capacity. Simplifying their operation conditions is a prerequisite before they can efficiently be used as the hydrogen carriers for trains. The dehydrogenation process, refuelling time, and safety issues are the concerns for their onboard utilisation.

Apart from the technologies mentioned above, some other storage methods receive continued attention as well, such as hydrate hydrogen, physisorption-based storage, and

composite storage. At present, the hydrogen storage capacity of hydrate hydrogen storage is lower than 1 wt% in most cases, and their operation pressure is too high, which restricts its onboard application [33]. For physisorption-based materials, the Department of Energy (DOE), America, published a summative report on hydrogen sorption [34,35]. They have acceptable hydrogen capacity but low temperature (usually 77 K) and high pressure is a must. For the composite storage mode, it includes a metal hydrides compressor and cryo-adsorption on active carbon or porous materials, etc. [36–39]. Improvement of the hydrogen capacity is attained to some extent but is accompanied by a more complicated system and a rise in cost. Most of these technologies are in their lab stage. There are few relative data sources in the industry that can be found now. Hence, we do not spend much time discussing these methods and just focus on the mainstream hydrogen storage technologies discussed in the last paragraph.

In this paper, existing hydrogen-powered trains are presented and discussed. Most of them are equipped with 35 MPa CH₂ with Type III tanks. Moreover, different types of hydrogen storage technologies are evaluated for the hydrogen storage density, economic cost, operation conditions, and development prospect. Furthermore, according to specific requirements for railway engineering, suggestions on the promising hydrogen storage methods for next-generation hydrogen-powered locomotives are provided.

2. Compressed Hydrogen Storage

Currently, compressed gas hydrogen technology is the most well-established among all the hydrogen storage technologies. It involves the physical storage of compressed hydrogen in high-pressure vessels and operates at high pressures, as high as 70 MPa. Its mature upstream and middle supply chain, including the production plants and refuelling stations, enable high-pressure hydrogen refuelling with relatively fast speeds and strong compatibility for vehicles. There are four standard types of CH₂ vessels, as shown in Table 1:

Table 1. Different types of compressed gas hydrogen tanks [40,41].

Type	Materials	Features	Typical Pressure (MPa)	Cost (USD/kg)	Gravimetric Density (wt%)
I	All-metal construction	Heavy, internal corrosion	17.5–20	83	1.7
II	All-metal hoop-wrapped composite cylinders	Heavy, short life due to internal corrosion	20–30	86	2.1
III	Fully wrapped composite cylinders with metallic liners	Lightness, high burst pressure, no permeation, galvanic corrosion between liner and fibre (CF)	35–70	567	5–5.5
IV	All-composite construction	Lightness, lower burst pressure. High durability against repeated charging. Simple manufacturability	35–70	633	5–5.7 (Toyota data)

Because of the low H₂ gravimetric capacity of Type I and Type II, they are not suited for vehicular use. Type III and type IV vessels are widely employed for H₂-powered vehicles now. Type III vessels are composed of a metal liner with full composite overwrap, generally aluminium, with a carbon fibre composite. Type IV vessels have an all-composite construction featuring a polymer (typically high-density polyethylene) liner with carbon fibre or hybrid carbon/glass fibre composite. Type III cylinders with 35 MPa storage pressure are usually equipped on heavy-loaded vehicles, from commercial buses, trucks, to

locomotives. Type IV cylinders with 70 MPa storage pressure are employed for light-duty vehicles, mostly cars, such as the Toyota Mirai. A comparison between the two storage pressure types is shown in Table 2:

Table 2. Summary results of assessment for CH₂ storage system compared to DOE targets [42,43].

Performance and Cost Metric	Units	35 MPa	70 MPa	2020 Targets	2025 Targets	Ultimate
System gravimetric capacity	Wt %	5.5	5.2	4.5	5.5	6.5
System volumetric capacity	g-H ₂ /L	17.6	26.3	30	40	50
Storage system cost	USD/kWh	15.4	18.7	10	9	8
WTT efficiency (LHV)	%	56.5	54.2	60	60	60

It can be found from Table 2 that the system gravimetric capacity of CH₂ technology can mostly meet requirements of DOE (2025), but its system volumetric capacity is still far from the final target. Another unexpected result is that the gravimetric capacity of a 70 MPa storage vessel is less than that of a 35 MPa system. To withstand higher pressure, more CF must be wrapped around tanks, which increases its self-weight and raises its cost. Reducing the storage system cost is another focus point on the aspect of the industrial mass production. As shown in Figure 1, cost of CF and balance of plant (BOP) accounts for a large proportion of the total cost. Hopefully, it is predicted by DOE that the system cost will drop from 22.94 USD/kWh (10 k systems per year) to 14.07 USD/kWh (500 k systems per year).

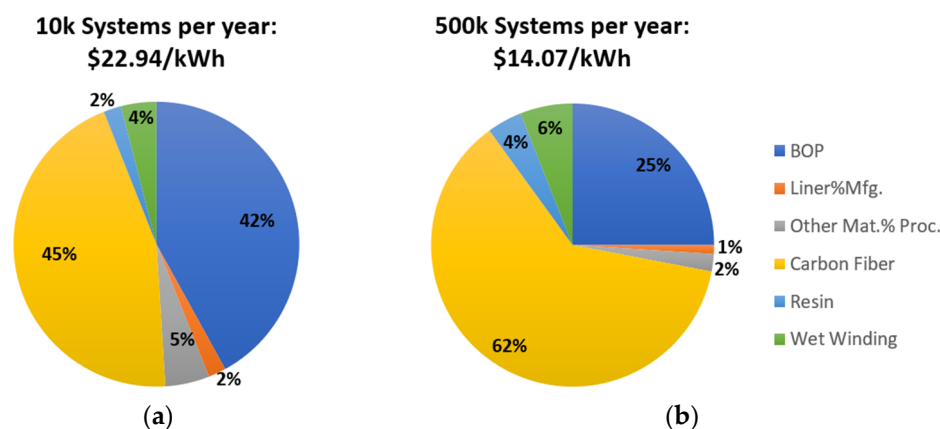


Figure 1. Cost breakdown for type IV 700 bar H₂ single tank storage systems with 5.6 kg usable (from DOE): (a) 10 k systems per year; (b) 500 k systems per year [44].

Recently revealed hydrogen-powered trains all adopt CH₂ hydrogen storage technology, including HydroFLEX (2019) [6,16,45,46], CRRC (2021), and Coradia iLint, Alstom (2018) [47,48], as shown in Table 3.

A key issue for CH₂-powered train designs is the arrangement for mounting its new power system, including the hydrogen storage system, fuel cell system, auxiliary power, electric motors, etc. A large space is required to place high-power proton exchange membrane fuel cell (PEMFC) stacks, as well as the hydrogen storage system. Because of requirements for long range use, quantities of hydrogen must be taken to ensure enough power is provided. The drawback of the hydrogen storage capacity of CH₂ results in multi-groups hydrogen tanks needing to be installed. To tackle the problem of space arrangement, the Coradia iLint train places PEMFC stacks and hydrogen tanks above its carriages, as shown in Figure 2. HydroFLEX 1.0 changes its original PMOS carriage to a power system carriage, as shown in Figure 3, installing fuel cell systems, four Luxfer W205N Type III hydrogen tanks, batteries, control system, and electric motors, etc. The arrangement reduces passenger accommodation, but it is deemed to be within tolerance

for passenger crush loading. Noticeably, the next-generation HydroFLEX will use more hydrogen storage tanks to enlarge its range, which has a considerable influence on the space assignment. Miniaturisation and lightweight design for the power system is necessary for current locomotives, but it is still a problem remaining to be solved with current CH₂ storage technology.

Table 3. Recently revealed hydrogen-powered trains.

Hydrogen-Powered Trains	HydroFLEX 1.0	CRRC Datong	Coradia iLint
Manufacturer	Porterbrook and University of Birmingham, UK, 2019	CRRC, China, 2021	Alstom, Germany, 2018
Type	Passenger locomotive	Freight locomotive	Passenger train
Hydrogen storage method	35 MPa CH ₂ vessel	35 MPa CH ₂ vessel	35 MPa CH ₂ vessel
Fuel cell	PEMFC (400 kW)	PEMFC (400 kW)	PEMFC
Auxiliary power	Battery (400 kW)	Battery (1000 kW)	Battery

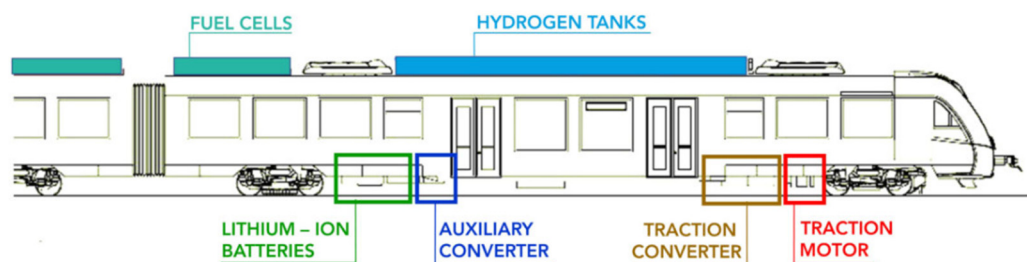


Figure 2. Diagram of Coradia iLint train, Alstom, propulsion system [49].

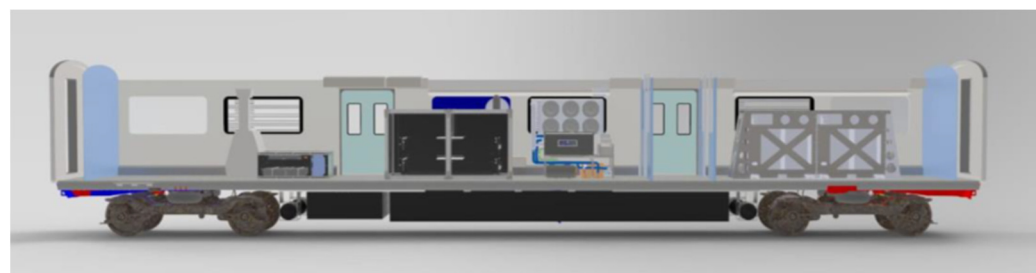


Figure 3. Design of HydroFLEX’s pantograph motor open second (PMOS) carrier.

To summarise, compressed gas hydrogen storage technology is unmatched in the aspect of maturity, which makes it the most popular for onboard applications now. Nevertheless, low hydrogen capacity will restrict its further application on heavy-load locomotives. The requirements of long-range and high-power heavy haul railways result in the locomotive needing to be equipped with multiple groups of hydrogen tanks. This brings a larger space occupation and complex gas supply line, which affect its safety, stability, and economics. Enlarging its storage density and reducing its cost will continuously be important research points in the future.

3. Liquid Hydrogen Storage

Historically, liquid hydrogen storage technology has been the preferred method to increase hydrogen density for bulk transport and storage [50]. The density of liquid

hydrogen is 70.78 kg/m^3 . Current technology can refrigerate hydrogen to a temperature of 20 K to be stored in vacuum-insulated vessels at 0.6 MPa [51]. It has great superiority over CH_2 storage on the system volumetric storage capacity, which can reach up to 36.6 kg/m^3 . Another typical advantage of LH_2 is its relatively low cost in most aspects. DOE presented a report in 2020, which compares the cost of the whole industry chain between CH_2 and LH_2 based on some specific scenarios as shown in Table 4. Indeed, the liquefaction process consumes large quantities of energy. Moreover, LH_2 costs less than CH_2 in other processes. Fortunately, according to R.K Ahluwalia [52], large scale production with large plants will reduce its production cost, the liquefaction capital cost will drop to 2500 USD/kg per day when its yield finally rises to 100 k tons per day.

Table 4. Cost comparison between CH_2 and LH_2 based on the specific scenarios (USD/kg) [53].

Pathway	H ₂ Production	Storage (Plant)	Liquefaction	Terminal	Transmission	Distribution	Dispensing (LDV)	Total Cost
CA(CH_2)	1.64	0.23	-	1.14	-	0.89	2.27	6.17
CA (LH_2)	1.64	-	2.86	0.31	-	0.30	1.94	7.05
TX to CA (LH_2)	0.89	0.31	2.15	0.33	1.10	0.30	1.94	7.02

Considering its energy storage density, cryogenic liquid hydrogen storage is an ideal method for heavy-duty vehicles. However, its gravimetric capacity is not completely satisfactory, owing to the high demand for insulation. Thick thermal insulation materials need to be wrapped in an LH_2 vessel, causing a large cost, space, and gravity occupation. Moreover, the liquefaction process requires 4–10 kW/h per kilogram, accounting for over 30% of the energy stored, theoretically, more than twice than H_2 compression. This percentage is even higher while in practical production. Another challenge for LH_2 application is that it is difficult for long term storage, with 0.2–0.3% d-1 loss in well-insulated tankers and up to 3% d-1 in vehicle-mounted vessels [54]. Under cryogenic conditions, spontaneous ortho-to-para conversion would release non-negligible heat, e.g., 702 kJ/kg at 20 K [55], which would promote hydrogen evaporation. Although well insulated, absorbing heat from the atmosphere is unavoidable because of the huge temperature difference between the inner tank and the atmosphere. Inner pressure rises quickly as LH_2 vaporises. Venting measures must be taken to prevent danger. Furthermore, more attention should be paid to its refuelling technology. The gas–liquid two-phase flow exists while filling, which slows its filling speed. It is a non-negligible problem when LH_2 -powered systems are mounted on locomotives [56].

LH_2 is always mentioned in hydrogen transport because of its high H_2 capacity and low transport cost, especially in marine environments. In 2019, Kawasaki Heavy Industries, Japan, launched the world's first liquid hydrogen transport ship, Suiso Frontier [57]. It has a mounted 1250-cubic-meter, vacuum-insulated double-shell-structure stainless steel LH_2 cargo tank, specially developed by Harima Works.

There are no existing LH_2 -powered locomotives yet, though LH_2 has been used in the military and aerospace fields for a long time. The onboard LH_2 -based system is well established by Linde as shown in Figure 4. Therefore, LH_2 -powered trains can be considered as a great challenge, as well as a commercial opportunity. This is noticed by some institutions and corporations, such as the Korean Railroad Research Institute (KRRRI) and Wabtec from the US [58]. KRRRI announced details of a project to develop the world's first liquefied hydrogen-based traction system in 2021. The project aims to develop a liquefied hydrogen hybrid propulsion system, high-insulation cryogenic storage technology, and a fast-refuelling technology. The LH_2 -fuel cell system will support operation at up to 150 km/h and offer a range of 1000 km as well as reduce refuelling times by 20% compared with 70 MPa compressed hydrogen trains. Similarly, in heavy-duty fields, a prototype long-haul truck named Mercedes-Benz Trucks-GenH2 [59] received approval from German authorities for road use, with a range of up to 1000 km.

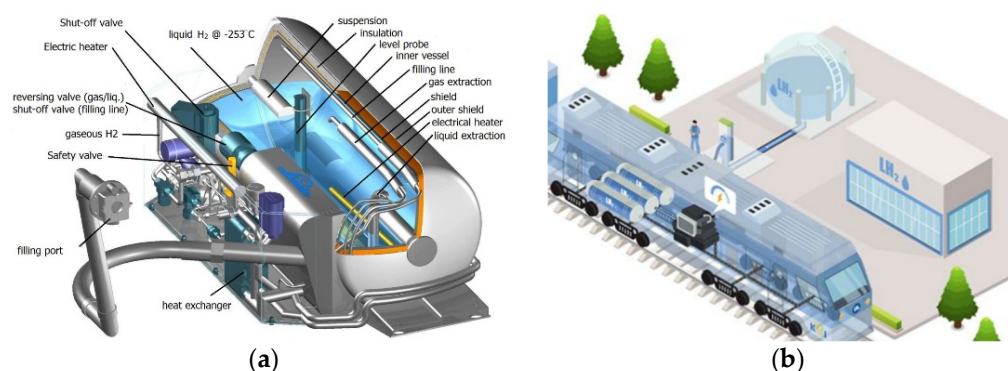


Figure 4. (a) Liquid hydrogen storage system from Linde [60]; (b) Schematic of the LH₂-hybrid train and the charging infrastructure presented by KRRI.

From a technical point of view, LH₂ storage technology is favourable for its high storage capacity, especially for heavy-loaded vehicles. Because of the large liquefaction consumption and short dormancy time, much effort is needed to conquer these challenges for onboard applications. Additionally, transporting hydrogen over a long range by LH₂ technology is a good choice and is feasible because of its high purity and hydrogen capacity. Comprehensively speaking, rail transit equipment based on LH₂ is basically consistent with heavy-duty vehicles in the equipment route of hydrogen filling and supply. Due to the higher requirements of power, longer endurance, and lower refuelling flexibility of railway transit equipment, higher demand on hydrogen storage efficiency is raised to reduce the filling frequency. Under the premise of the complete LH₂ infrastructure, setting up special LH₂ refuelling equipment along the track to provide special filling services is an important prerequisite for the development of LH₂ railway transit.

4. Cryo-Compressed Hydrogen Storage

Cryo-compressed hydrogen storage (CCH₂) refers to the storage of H₂ at cryogenic temperature in a vessel that can be pressurised (nominally 25–30 MPa) [61–63]. As shown in Figure 5, the volumetric storage capacity of liquid hydrogen rises with pressure increases. For example, when the pressure of LH₂ rises from 0.1 MPa to 23.7 MPa at 21 K, its density increases from 70 g/L to 87 g/L, and the gravimetric capacity also reaches 7.4 wt%. Compared with CH₂ storage technology, CCH₂ storage technology is superior for its H₂ storage capacity, which has the potential to reach the target set by DOE. In contrast to LH₂ technology, CCH₂ overcomes the limitation of dormancy time, which is three times that of LH₂.

Lawrence Livermore National Laboratory (LLNL), California, developed a novel CCH₂ vessel and the onboard storage and supply system for fuel cell stacks as shown in Figure 6 [24,64,65]. Temperature and pressure management of this system is carefully treated because of the high-pressure and cryogenic characteristics of CCH₂. Compared to the Type III 35 MPa H₂ system, the 50 MPa CCH₂ storage system can achieve 91%, 175%, and 21% improvement in gravimetric capacity, volumetric capacity, and system cost reduction, respectively. Meanwhile, it enables the loss-free dormancy exceeding over 7 days with an initial 85% load. According to these attractive performances, many researchers participate in promoting the development of CCH₂ technology [66–68]. Optimisation designs for onboard CCH₂ storage systems are made to enlarge its energy utilisation efficiency. LLNL and Argonne National Laboratory (ANL) have made simulations for CCH₂ storage systems for freight and regional locomotives to validate their feasibility in railway engineering. With the annual production of CCH₂ systems rising to 500 k, its system cost will reduce to 14.93 USD/kWh [69]. BMW AG (Munich, Germany) released its prototype cryo-compressed cars for testing, as shown in Figure 7. The vessel was tested by LLNL from 2017 to 2018. No degradation of the vessel was observed after 1000+ cycles to 30 MPa [70,71].

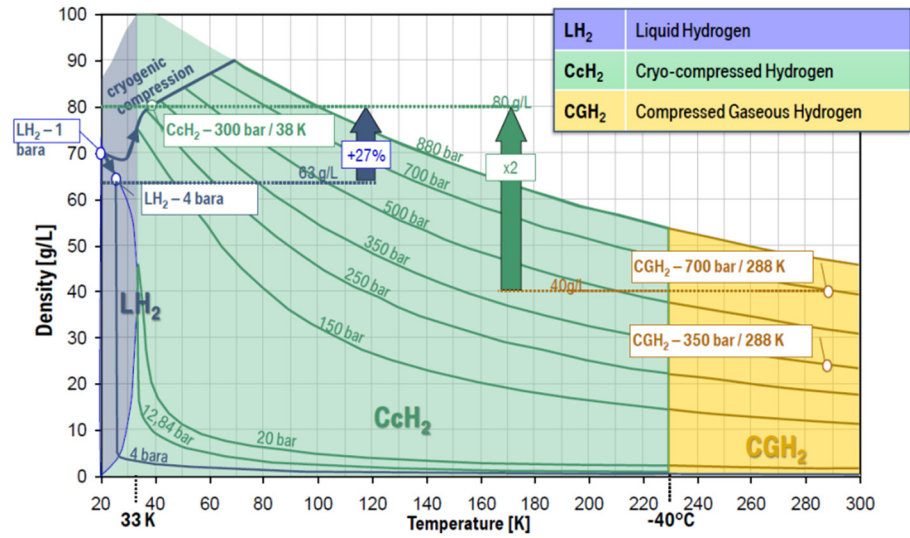


Figure 5. Hydrogen density versus pressure and temperature from BMW. Reprinted/adapted with permission from Ref. [62], copyright 2017 Elsevier.

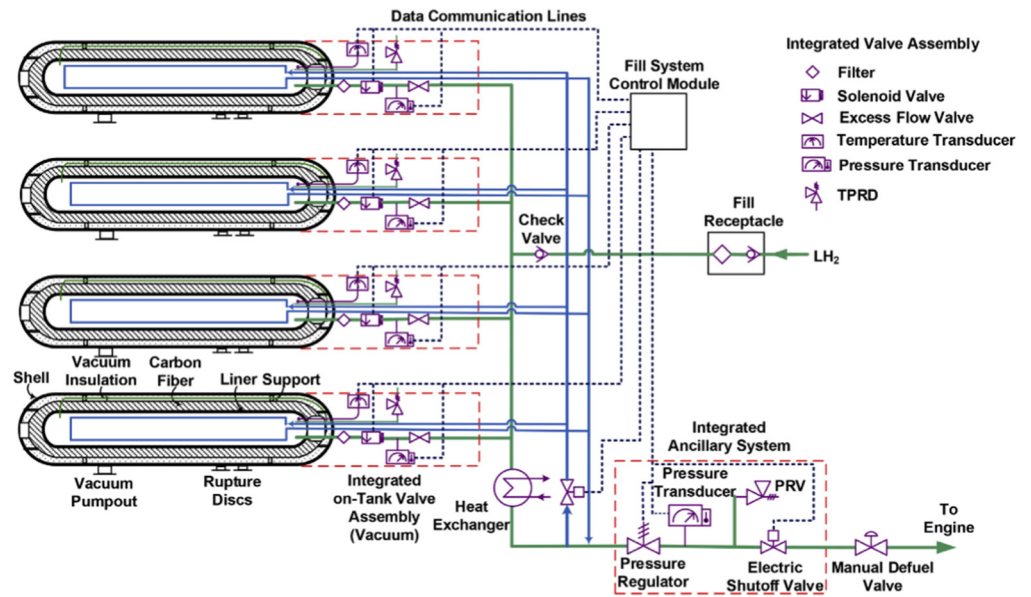


Figure 6. Onboard cryo-compressed hydrogen storage and supply system, LLNL. Reprinted/adapted with permission from Ref. [24], copyright 2018 Elsevier.

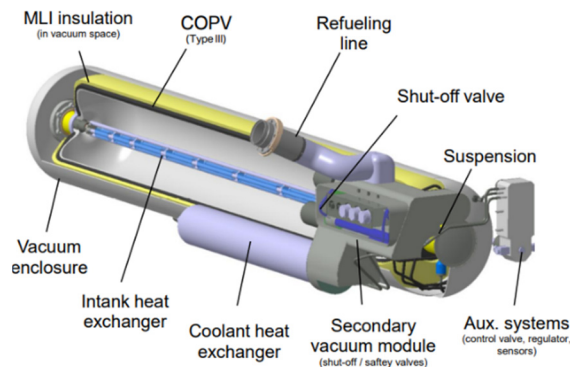


Figure 7. Schematic of CcH₂ storage vessel from BMW.

Detailed cost comparison among CcH₂, CH₂, and cold-cH₂ has been conducted by DOE, 2018 [72]. The results are shown in Table 5. It can be seen that 350 bar and 500 bar CcH₂ storage vessels have a price advantage compared with 350 bar CH₂ storage vessels because of its lower requirement for composites (mainly CF).

Table 5. Storage system cost comparison between CH₂, Cold-cH₂, and CcH₂ (USD/kWh).

	350 Bar CcH ₂	500 Bar CcH ₂	700 Bar CcH ₂	350 Bar CH ₂	Cold-CH ₂
Liner	1.03	1.01	0.99	0.21	1.58
Composite	3.25	4.70	7.12	9.79	8.86
Insulation and containment vessel	3.48	3.21	2.92	0.00	3.05
BOP	3.84	3.85	3.85	3.25	3.45
Assembly and other	0.04	0.04	0.04	0.12	0.04
System cost	11.65	12.82	14.92	13.38	16.97
(USD/kWh)	[−2.32, +2.90]	[−2.32, +2.90]	[−2.78, +3.61]	[−3.44, +5.73]	[−0.81, +1.59]

To conclude, CcH₂ storage combines the advantages of CH₂ storage and LH₂ storage, which results in a high hydrogen storage capacity and long loss-free dormancy time. Core components of the CcH₂ storage system have experimentally validated the requirements of high-density storage, rapid refuelling (without H₂ loss), safety, and structural durability. However, this technology is still in its prototype stage. Relevant international standards need to be formulated. Infrastructure and supporting facilities will reduce its cost in the future. It can be forecasted that CcH₂ is a prospective option for hydrogen-powered hybrid trains in the future.

5. Liquid Organic Hydrogen Carriers (LOHCs)

In 2021, Siemens Mobility and the Helmholtz Institute Erlangen-Nuremberg for Renewable Energy (HI ERN), Germany, declared to jointly retrofit Vectron mainline locomotives' power system with LOHCs technology [73], which indicates that LOHCs technology could be another candidate for railway engineering.

LOHCs are liquids or low-melting solids that can be reversibly hydrogenated and dehydrogenated under specific conditions with the assistance of catalysts [74]. Though their application on mobility is still under discussion, LOHCs are usually considered as a promising solution for hydrogen transportation over a long distance, which are better than physical storage methods in terms of power consumption and cost [75,76].

Properties of several LOHCs are listed in Table 6. Their hydrogen gravimetric capacities range from 6 wt% to 8 wt%, superior to CH₂ storage. Moreover, LOHCs are favourable for their relatively low cost, high degree of safety, and excellent reversibility [75,77,78]. Some researchers consider toluene-MCH as one of the most feasible H₂ carriers among LOHCs because of its relative maturity [79,80]. It was initially tested in the Euro-Quebec Hydro-Hydrogen project in the 1980s. Relevant regulations for storage and transportation have not yet been established. Additionally, its hydrogenation and dehydrogenation cycle has been successfully demonstrated by Chiyoda Corporation, Japan.

A.T. Wijayanta, etc. [79] made detailed research on toluene-MCH, including its utilisation methods, well-to-wheel efficiency, cost analysis, and future development. According to their research, toluene-MCH can be used by direct combustion and fuel cells after dehydrogenation, whose total energy efficiencies are 26% and 45%, respectively. Compared with other hydrogen storage technologies, toluene-MCH has advantages in the production stage, which consumes only 25% of the total energy stored in H₂. During transportation, its loss can be neglected. Nevertheless, much energy will be consumed during dehydrogenation, which is a common problem for other LOHCs. In his forecasting model, the cost of Toluene-MCH can be reduced to JPY 31.5 (USD 0.26) *Nm⁻³-H₂ in 2030 and further drop to JPY 27.3 (USD 0.22) *Nm⁻³-H₂ in 2050.

Table 6. Technical properties of some potential LOHCs [81].

Properties	Toluene-MCH		Naphthalene-Decalin		Benzene-Cyclohexane		DBT-PDBT	
	Toluene	MCH	Naphthalene	Decalin	Benzene	Cyclohexane	DBT	PDBT
	Physical							
Chemical formula	C ₇ H ₈	C ₇ H ₁₄	C ₁₀ H ₈	C ₁₀ H ₁₈	C ₆ H ₆	C ₆ H ₁₂	C ₂₁ H ₂₀	C ₂₁ H ₃₈
density	867	0.769	0.975	0.896	0.874	0.779	1.010	1.057
Melting point	−95	−127	80.3	Cis −43.0 Trans −30.4	5.5	6.5	−30	−34
Boiling point	111	101	218	Cis −94.6 Trans 185.5	80	81	278	395
Phase under ambient cond.	Liquid	Liquid	Solid	Liquid	Liquid	Liquid	Liquid	Liquid
Gravimetric density (wt%)		6.16		7.29		7.2		6.2
Volumetric density(kg/m ³)		47.4		65.4		55.9		57
Heat of reaction (kJ/mol)		204.8		319.5(cis), 332.5(trans)		205.9		588.5
Temperature (°C)		200–300		150–250		150–250		180
Pressure (bar)		10–50		20–50		10–50		10–50
	Dehydrogenation with selected catalyst							
Temperature (°C)		250–350		300–350		330		260–320
Pressure (bar)		1–5		1–4		1–4		1–5
Advantages	Both liquid in wide range temperature		-Relatively high H ₂ content -Different phase		-Relatively high H ₂ content		-Higher intrinsic safety -Good thermal stability	
Challenges	-Irritative -Inflammable -Volatile		(difficulties in storage and transportation) -High energy for dehydrogenation -Volatile		-High melting point (possibility of phase change) -Toxic		-High energy for dehydrogenation	

M. Niermann, etc. [75] also comprehensively compared various LOHCs with non-LOHCs technology. Figure 8 illustrates that methanol is a suitable candidate for hydrogen delivery and import, as its overall system costs only EUR 9.9 (USD 10.8)/kg-H₂. Dibenzotoluene and toluene are also possible options with the assumption that their dehydrogenation process is assisted by wasted heat. Their costs are EUR 11.5 (USD 12.65) and EUR 11.9 (USD 13.09)/kg-H₂, following methanol.

Besides the whole supply chain of LOHCs, their specific application processes, especially dehydrogenation, also receive much attention. Heat supply methods and integration are believed to be key for LOHCs' application [80,82]. According to Table 6, no matter the kind of LOHCs, their reactions need to absorb heat to achieve high temperature. It requires the onboard thermal management system to undertake heavy responsibility. On the other hand, the high heat supply requirement also offers the chance to reuse wasted energy generated from the fuel cell stacks, as their heat efficiency is around 50%. Nearly half of the energy stored in hydrogen dissipates in the form of heat.

In summary, LOHCs are attractive for their high hydrogen storage capacities. Another outstanding characteristic of LOHCs is that they can be seamlessly integrated with current technologies and industries. This results in cost reduction while ensuring large-scale promotion. Barriers to its application appear because of its dehydrogenation process, including complex catalytic conditions, large energy consumption, low hydrogen releasing speed, and toxic by-products generated from side reactions. Much effort, especially of the onboard heat management system, is needed to optimise the H₂ releasing process to

achieve the excellent performance required for LOHC-powered trains. However, LOHCs are a possible choice for H₂ transportation because of their high hydrogen capacities.

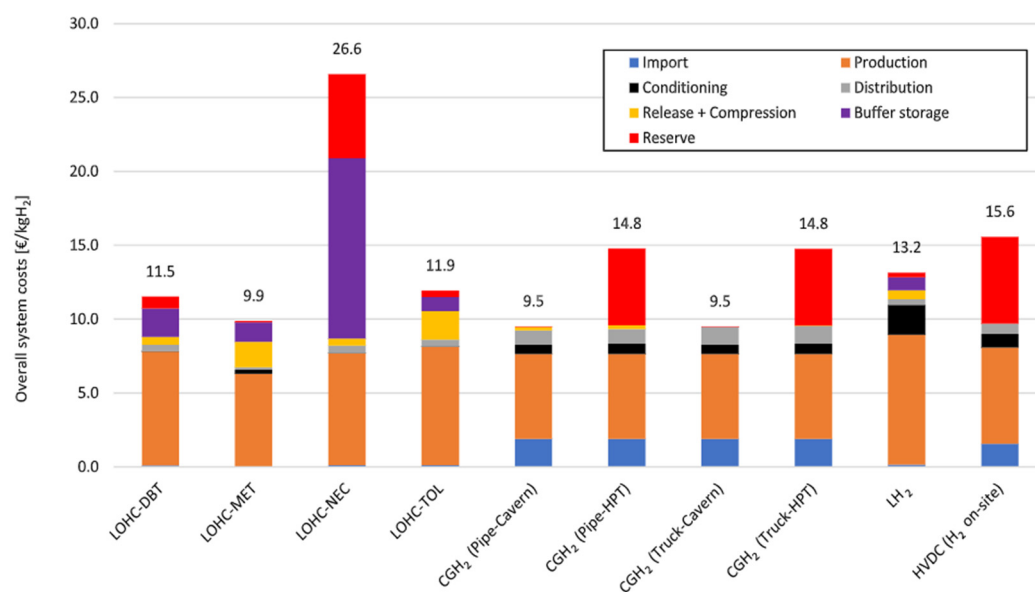


Figure 8. Overall system costs (OSC) of the assessed hydrogen supply chains (DBT: dibenzyltoluene, HPT: high-pressure tank, HVDC: High Voltage Direct Transmission, LH₂: Liquefied Hydrogen, LOHC: Liquid Organic Hydrogen Carrier, MET: methanol, NEC: N-ethylcarbazole, Pipe: Pipeline, TOL: toluene). Reprinted/adapted with permission from Ref. [75], copyright 2021 Elsevier.

6. Ammonia

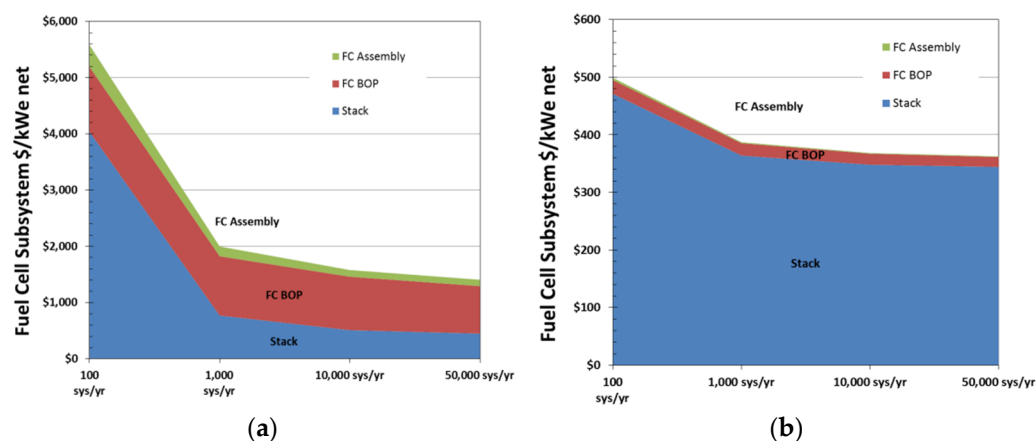
Ammonia (NH₃) has been discussed as the energy carrier for mobility for a long time and has been increasingly recognised as an alternative carbon-free energy source in recent years [83–86]. KHM Al-Hamed, etc. have conducted much effort to introduce ammonia to clean locomotives. They proposed a novel integrated solid-oxide fuel cell powering system with heat recovery. The overall energy and exergy efficiencies improve up to 74.22% and 71.95%, which is a great improvement to existing diesel-based locomotives.

As shown in Table 7, Ammonia has a high gravimetric H₂ density, 17.7 wt%, superior to most hydrogen storage technologies. Its volumetric H₂ density is also attractive, 120.3 kg-H₂/m⁻³. Similar to hydrogen, it can be stored in vessels under cryogenic temperature (240 K at atmospheric pressure) or high pressure (10 bar at room temperature) [87]. However, liquid ammonia is easier to obtain than liquid hydrogen, which means it costs less but achieves a higher energy density. Another obvious strength is its mature industrial production system. NH₃ is one of the most highly produced inorganic chemicals, 175 million tons are produced annually worldwide, widely used as a source of nitrogen in agriculture. Based on the mature large-scale production and easily attainable requirements for density, the process of its production and transportation are cheaper than LH₂. According to Apodaca and Ewing [30], its price is only 0.3 USD/kg (0.058 USD/kWh), which is competitive with the current fossil fuel price. The hidden danger for NH₃ application is its toxicity and potential nitric oxide (NO_x) generation [88]. Careful handling during storage and transportation is demanded to avoid the risk of leakage. The control of NO_x emissions has been investigated in detail from its production to utilisation [89,90]. These problems are being solved now, or optimisation is being realised to some extent.

Table 7. Relevant properties of ammonia [91].

Property	Unit	Value
Molecular weight	g/mol	7.03
Gravimetric H ₂ capacity	wt%	17.7
Volumetric H ₂ capacity	kg-H ₂ /m ⁻³	120.3
Storage condition	bar or K	10 or 240
H ₂ release temperature	K	600–1200
Regeneration temperature	K	650–900
Ignition temperature	K	924
Price	USD/kg (USD/kWh)	0.3 (0.058)

There are three routes for ammonia utilisation as the vehicular energy source. Firstly, ammonia acts as a hydrogen carrier. It is used by fuel cells after decomposition to release H₂. Huge amounts of energy are required during ammonia decomposition, 2.79 kJ/mol-H₂, theoretically. After decomposition, H₂ separation, purification, storage, and compression are needed before it can be used by fuel cells [87]. Numerous catalysts are being developed and tested to optimise its decomposition process, which is the research hotspot for this route now. The comprehensive energy efficiency, including its production, transportation, and utilisation, is about 34%. Direct combustion is another method under the spotlight. NH₃ can be mixed with other fuels, such as hydrogen, in certain proportions to enhance its combustion ability [92]. Ammonia internal combustion engines are successfully used in marine engineering and have proved to be feasible. After taking optimisation measures, its well-to-wheel energy utilisation efficiency of direct combustion can reach about 34%. The major pollutant in the combustion process is NO_x. It can be reduced but cannot be completely avoided with the existing technology. Additionally, ammonia-fed solid-oxide fuel cell (SOFC) is an emerging technology which can directly use NH₃ without decomposition. Two types of ammonia-fed SOFCs are developed, SOFC-H (proton-conducting) and SOFC-O (oxygen-ion conducting) [93]. SOFC-H may be the more suitable one for onboard use because of its higher energy utilisation efficiency considering the fuel economics. Its total energy efficiency is predicted to reach 46%. Among the three routes, direct use by fuel cell seems to have the best energy utilisation efficiency at 46%, approximately. The noteworthy hindrance to this route is the price of SOFCs, as shown in Figure 9. According to the analysis from B.D. James [94], the cost of a SOFC system is still at a high value, but will drop when higher powered systems and more SOFC systems are required. It can be predicted that the price of SOFC systems will continue to decrease with relevant technology improvement.

**Figure 9.** Cost prediction and analysis for SOFC subsystem (a) 1 kW Fuel Cell SOFC Subsystem; (b) 100 kW Fuel Cell SOFC Subsystem [94].

Although ammonia encourages relatively high energy consumption in both synthesis and decomposition (if required), it still has the highest overall well-to-wheel energy efficiency. From the point of view of fuel cost, ammonia shows the lowest price, regardless of direct use or decomposing, JPY 31 (USD 0.246) *Nm⁻³-H₂ and JPY 24.5 (USD 0.201) *Nm⁻³-H₂ in 2030, respectively [79]. Considering its high energy capacity, low cost, and mature supply chain, ammonia is, at least, a potential medium for hydrogen transportation. Moreover, it can be a promising candidate for locomotives with the technology development of its catalyst for decomposition and SOFC-H.

7. Metal Hydride-Based Storage

Metal hydride (MH)-based hydrogen storage technology is a chemical storage method where hydrogen is chemically stored on materials by an absorption process. Researchers from Romania [95] proposed a hybrid propulsion train with hydrogen stored in metal hydrides, which were made up of two locomotives and two wagons. Compared with battery packs, the metallic hydride tank can store five times more energy using the same weight. Additionally, it was declared to contain more energy per cubic meter than liquid hydrogen storage. Meanwhile, there are some researchers discussing the application of MH for light-duty mobile applications, such as forklifts and cars [96,97]. Thus, MH is another onboard hydrogen storage technology receiving attention.

MH storage systems are composed of the MH tubes. DOE uses Type III and IV tank technology for tube manufacturing, with stainless steel tubes also being used by some manufacturers. The fundamental performance of the MH system is determined by the material powder selected. At present, the main alloying materials for metal hydrides are intermetallic compounds (AB₅, AB₂, AB, and A₂B). They are attractive as they are capable of absorbing large quantities of hydrogen. However, the hydrogen gravimetric density of common intermetallic metal hydrides is relatively low, as shown in Table 8, which is a serious impediment to their vehicular application. Moreover, their slow kinetics and complicated activation procedure further limit their practicality for mobile vehicles. Instead, intermetallic hydrides are applied to many other areas, such as nickel metal hydride battery electrodes, hydrogen purification systems, cooling systems, as well as hydrogen sensors [98].

Table 8. Properties of some metal hydrides [99–104].

Type	Component	Hydrogen Storage Capacity (wt%)	Temperature (K)	Pressure (MPa)
Intermetallic hydrides	LaNi ₅ H ₆	1.37	295	0.1
	FeTiH ₂	1.89	185	0.1
	Mg ₂ NiH ₄	3.59	255	0.1
	ZrMn ₂ H ₂	1.77	440	0.1
Complex hydrides	LiBH ₄ nanocomposite	6.5	573	-
	LiBH ₄ + SiO ₂	13.5	373	5.0
	NaAlH ₄ + 1.0 mol% TiCl ₃	5.6	323–383	-
	NaAlH ₄ + 4.0 mol% Ti	4.8	373	-
	NaAlH ₄ + 1.0 mol% Ti	5.6	443/423	15.4
	Na ₃ AlH ₆ + 2.0 mol% TiCl ₃	2.1	473/543	6.0
	NaAlH ₄ + porous carbon	7.0	673	10.0
	NaAlH ₄ + none-porous carbon	6.3	673	10.0

To enlarge hydrogen gravimetric capacity, complex hydrides composed of light elements gained significance. Challenges for its onboard utilisation mainly focus on the cost, operation conditions, and refuelling time. High thermodynamic stability and slow kinetics during hydrogen cycling affect its practicality in onboard use, causing high temperature and pressure to be essential during operation. Taking NaAlH₄ (Sodium Alanate) as an

example, its hydrogen storage capacity ranges from 2 wt% to 7 wt%, but its operation conditions are really harsh. High pressure and temperature are a must no matter what elements are added. It is demonstrated by DOE as shown in Figure 10 that the projected SAH system is inferior in terms of the system cost, fill time, and hydrogen storage density. Hopefully, these issues are being studied and tackled by the addition of new elements into the system, or the addition of reactive hydride composites. Overall, complex hydrides have higher H₂ capacity than intermetallic hydrides. Further research on the novel material and optimisation for onboard thermal management systems is needed to improve its dehydrogenation and hydrogenation process before its practical application for locomotives.

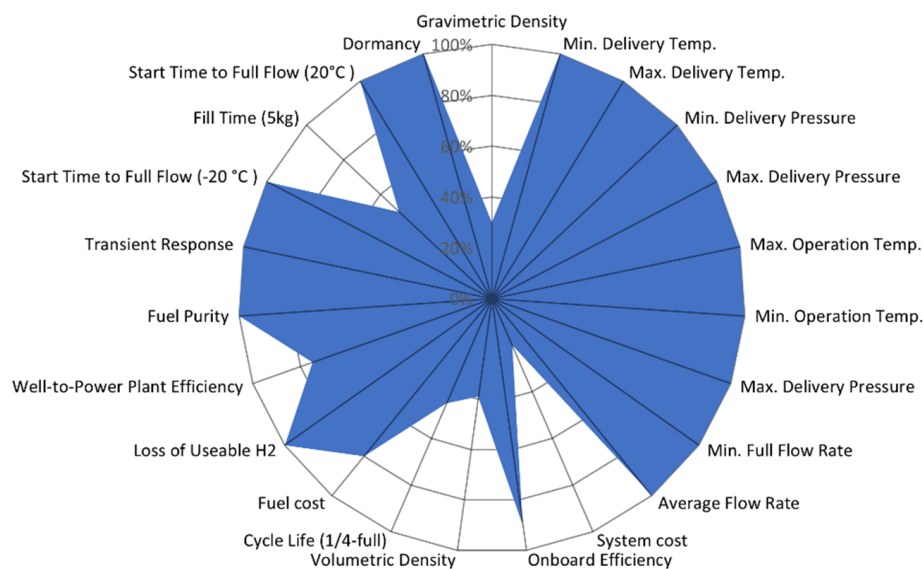


Figure 10. Projected sodium alanate (SAH) system compared against 2020 targets, dual tank, from DOE [105].

Similarly, magnesium-based alloys have advantages in their hydrogen gravimetric capacity, up to 7.6 wt% [106]. Its hydrogenation and dehydrogenation process would be difficult due to the strong bonding between magnesium and hydrogen. Recent research shows that its hydrogen absorption/desorption properties can be enhanced at 573 K by the synthesis of ultra-fine microstructures and the addition of catalysts such as transition metals, rare earth metals, and transition metal oxides [26]. However, the kinetics of Mg-based hydrides are still unsatisfactory at low temperatures. Harsh operating/refuelling conditions and slow hydrogen supply rate are obstacles to their further onboard application.

Chemical hydrides, such as ammonia borane (NH₃BH₃), raised considerable attention for their high gravimetric hydrogen storage capacities [107]. The published assessment on the ammonia borane system from DOE is presented in the form of a spider diagram, as shown in Figure 11. It can be easily seen that the system cost, well-to-power plant efficiency, and fuel cost are far from satisfactory. The barrier of most chemical hydrides for onboard application is their irreversibility, which makes them one-way single-use fuels. Moreover, leftover by-products must be removed from the vehicle for off-board regeneration. Therefore, chemical hydrides are not suitable for vehicle-mounted employment now, but they have great potential for hydrogen transportation as the H₂ carrier.

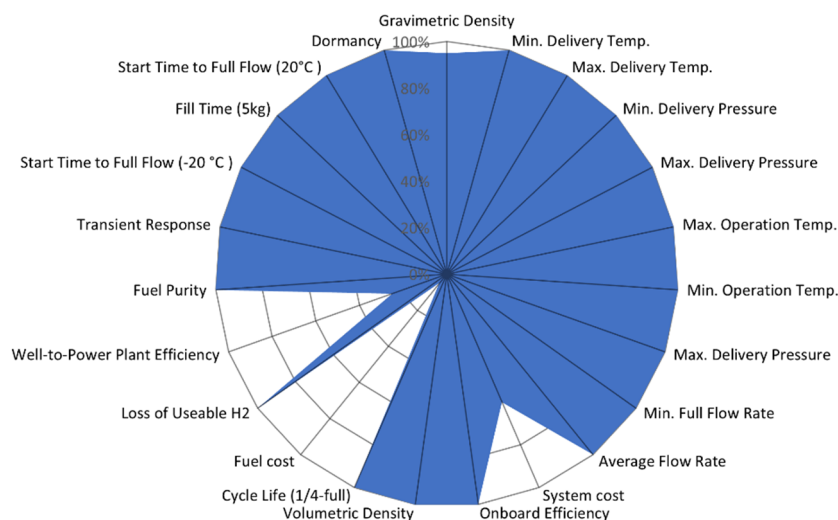


Figure 11. Projected ammonia borane system compared against 2020 Targets, 50% mass loaded slurry, from DOE [105].

8. Overall Comparison

Since most hydrogen storage technologies are not commercially mature, there are not enough reliable industrial data to reflect their performance in practice. We used the data from DOE, ANL, LLNL, etc., which was published from 2013 to 2017 [108–111], to compare their storage capacity and cost, as shown in Figure 12. The selection of the hydrogen storage mode for trains requires a comprehensive consideration of their technical credibility and economic credibility according to the specific requirements.

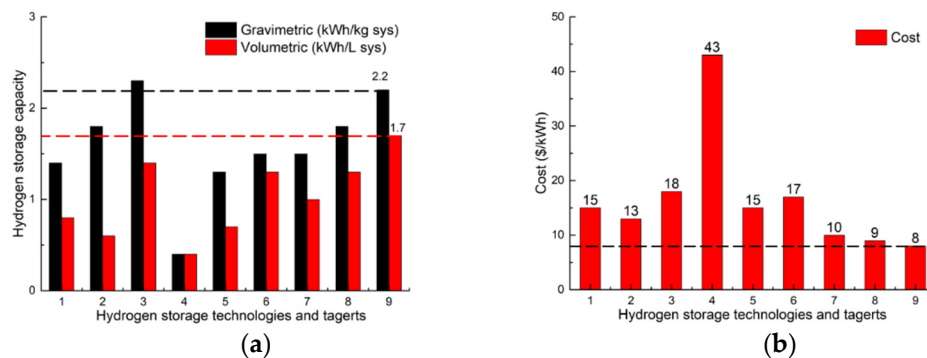


Figure 12. Projected performance of hydrogen storage systems (a) comparison of hydrogen storage capacity; (b) comparison of cost, projected to 500 k units/yr. (1: 700 bar compressed Type IV; 2: 300 bar compressed Type IV; 3: 500 bar cryo-compressed; 4: metal hydride NaAlH₄/Ti; 5: Sorbent MOF-5100 bar; 6: Chemical storage, AB liquid; 7: 2020 target values; 8: 2025 target values; 9: ultimate target values).

According to the published research reports from DOE, the barriers for the onboard potential hydrogen storage system are concluded and presented in Table 9. These problems need to be solved to improve their commercial maturity before it can be adopted and mounted on hydrogen-powered hybrid trains.

Integrating all the data and discussions from chapter 2 to chapter 8, the comprehensive summary of the potential storage methods is presented in Table 10. Meanwhile, their technology readiness level (TRL) is predicted based on the reports and research papers above.

Table 9. Existing barriers for potential hydrogen storage systems [108,112].

Barriers	Physical Storage Systems		Material-Based Storage System		
	Compressed	Cold/Cryo-Compressed	Metal Hydride	Sorbent-Based	Chemical Storage
Materials of Construction	•	•	•	•	•
Balance-of-Plant Cost	•	•	•	•	•
Thermal Management	•	•	•	•	•
Tank Cost	•	•	•	•	•
Tank Mass	•	•	•	•	•
Off-board Energy Efficiency	•	•		•	•
Heat Transfer Systems			•	•	•
Material Gravimetric Capacity			•	•	•
Material Volumetric Capacity			•	•	•
Reaction Thermodynamics			•	•	•
Cryogenic Tank Operation		•		•	•
High Temperature Tank Operation			•		•
Carbon Fibre Cost	•	•			
Material Thermal Conductivity			•	•	
Fuel Purity			•		•
Kinetics			•		•
Reactor Design					•
Material Handling					•

Table 10. Summary of different hydrogen storage technologies for onboard use.

Hydrogen Storage Technology	Advantages	Disadvantages	Current State	TRL	
Physical Storage Methods	Compressed hydrogen	-Relatively mature -Many types of storage tanks for different areas -Purity	-Storage density needs to be improved -Cost needs to be reduced	-Successfully used for trains -Mass production	8/9
	Liquid hydrogen	-High volumetric capacity -Purity -Relatively low utilisation cost	-High liquification cost -Short dormancy time (boil-off)	-Mostly used for military and aerospace -Prototype trucks -Being tested for trains in KR and JP	6/7
	Cryo-compressed hydrogen	-High hydrogen capacity -Long dormancy time -Relatively low cost	-Low maturity	-Prototype cars -Onboard simulation for trains by DOE	4/5
Material-based (chemical) storage methods	Metal hydrides	-Some types have high storage capacity -Able to absorb large quantities of hydrogen -Multi-role	-Harsh operation conditions -Refuelling time -High cost for onboard use	-Prototype vehicles -Mostly discussed for hydrogen transportation	4/5
	Liquid organic hydrogen carriers (LOHC)	-High hydrogen capacity -Relatively low cost	-Complex catalytic conditions -Low hydrogen releasing speed -Toxic by-product -Unavoidable purification	-Being tested for trains by Siemens -Mostly discussed for hydrogen transportation	6/7
	Ammonia	-Mature production chain -Low cost -Multiple use routes	-By-product NO _x -Toxic -Expensive DA-SOFC -Dehydrogenation cost	-Successfully used for marine applications (direct combustion) -Lab stage (SOFC route)	6/7 (direct combustion) 4/5 (SOFC route)

Compressed gas hydrogen storage technology is widely used now. Most of the recently released hydrogen-powered locomotives are equipped with 35 MPa CH_2 vessels. However, the hydrogen density still needs to be improved, so it has to be implemented in multi-groups to enlarge the operation range of the locomotives. Such a solution increases the complexity of the pipelines and requires much space occupation and costs. Therefore, CH_2 storage technology may not be suitable for all types of railway systems, especially for long-haul freight trains. Liquid hydrogen storage technology overcomes the problems of H_2 storage capacity to some extent. However, regional LH_2 supply stations, filling supporting facilities, the safety system, etc., need to be further studied and implemented. Cryo-compressed hydrogen technology combines the high H_2 storage capacity from LH_2 and the long dormancy time from CH_2 . If only considering technical advantages, cryo-compressed hydrogen has the potential to be the next-generation onboard energy source for locomotives. Nonetheless, it is still in the prototype stage and there is a long way to go before large-scale commercial use.

Liquid organic hydrogen carrier technology is very attractive because of the high hydrogen storage capacity and low cost. Once the problems of its complex and slow dehydrogenation process are solved, it can be another candidate for the locomotive energy source. Additionally, metal hydrides technology is restricted by relatively harsh operating and refuelling conditions. The high cost for MH materials is another barrier for its commercialisation. Solving the issues above is the precondition of implementing hydride technology for railway transit. Ammonia is another promising hydrogen carrier for trains, since it has a high hydrogen capacity and low cost. With the storage safety and direct ammonia-fed SOFC technology being further evolved in the future, it is possible that ammonia will have a more important status in railway engineering.

To summarise, different hydrogen storage technologies have different benefits, which means they can adapt to varied requirements from different application scenarios. Several conclusions and suggestions can be drawn for railway transit:

- For physical hydrogen storage technologies, it can be forecasted that they will be the most popular onboard storage technology for trains in the next few years, since CH_2 storage can mostly meet the demands for train operation and is the most mature now. If higher requirements in terms of operation range and train power are raised, especially for long-haul freight trains, more attention should be paid to LH_2 and CCH_2 because of their high hydrogen storage capacities and relatively simple procedures before H_2 enters fuel cell stacks. Their supporting technologies are being studied and becoming mature.
- For material-based storage technologies, they are attractive for being able to absorb or adsorb quantities of hydrogen. They are capable for hydrogen transport as hydrogen carriers. Impediments of their train-mounted application are the dehydrogenation and hydrogenation process because controlled energy flow and refuelling speed are important evaluative criteria for mobility. Onboard thermal management design would be an emphasis for a material-based storage system.
- Notably, ammonia has an extremely high energy capacity, along with low cost and a mature production chain. It has various application approaches according to different scenarios, which gives flexible choice for NH_3 -based vehicles. It has the viability to become the energy source for locomotives with relevant technological advances, especially the catalyst for decomposition and SOFC technology.

9. Conclusions

Several hydrogen storage systems with different principles have been developed, tested, and compared. They present different characteristics while being applied to industry applications. As locomotives are expected to work in heavy-duty conditions for a long period, the energy source should achieve high energy density, long term storage, and low cost.

In this paper, we collect the relevant data to compare the potential onboard hydrogen storage methods in terms of their hydrogen storage capacity, operational conditions, economic costs, etc. An overall comparison is conducted to show the advantages and disadvantages of the promising storage methods. Moreover, existing barriers for these storage systems are also presented. Based on the analysis, the conclusions and predictions are made to help readers figure out the technology readiness levels and future trends. It might be a reference for railway manufacturers to choose onboard hydrogen storage technology for their hydrogen-powered hybrid locomotives.

In our future study, we will continue to track the technical progress of onboard hydrogen storage technologies, especially their specific application for railway engineering. Moreover, more attention will be paid to the development of the supporting infrastructures, since they are the basis for the large-scale application of hydrogen energy. Suitability between the infrastructures and onboard storage system will be an essential evaluation criterion for the selection of an onboard hydrogen storage method. Furthermore, the Well-to-Tank efficiency and carbon emissions of the whole supply chain will be another focus to help evaluate their environmental friendliness. It is planned to conduct a comprehensive evaluation for train-used hydrogen storage technology considering economics, technical performance, and environmental requirements.

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References

1. Geels, F.W.; Sovacool, B.K.; Schwanen, T.; Sorrell, S. Sociotechnical transitions for deep decarbonization. *Science* **2017**, *357*, 1242–1244. [[CrossRef](#)] [[PubMed](#)]
2. Pan, X.; Wang, H.; Wang, L.; Chen, W. Decarbonization of China's transportation sector: In light of national mitigation toward the Paris Agreement goals. *Energy* **2018**, *155*, 853–864. [[CrossRef](#)]
3. Cullen, D.A.; Neyerlin, K.C.; Ahluwalia, R.K.; Mukundan, R.; More, K.L.; Borup, R.L.; Weber, A.Z.; Myers, D.J.; Kusoglu, A. New roads and challenges for fuel cells in heavy-duty transportation. *Nat. Energy* **2021**, *6*, 462–474. [[CrossRef](#)]
4. Khosravi, A.; Koury, R.N.N.; Machado, L.; Pabon, J.J.G. Energy, exergy and economic analysis of a hybrid renewable energy with hydrogen storage system. *Energy* **2018**, *148*, 1087–1102. [[CrossRef](#)]
5. Atteridge, W.J.; Lloyd, S.A. Thoughts on use of hydrogen to power railway trains. *Proc. Inst. Mech. Eng. Part A J. Power Energy* **2021**, *235*, 306–316. [[CrossRef](#)]
6. Hoffrichter, A.; Hillmans, S.; Roberts, C. Conceptual propulsion system design for a hydrogen-powered regional train. *IET Electr. Syst. Transp.* **2016**, *6*, 56–66. [[CrossRef](#)]
7. Jones, W.D. Hydrogen On Track. *IEEE Spectr.* **2006**, *43*, 10–13. [[CrossRef](#)]
8. Washing, E.; Pulugurtha, S. Well-to-Wheel Analysis of Electric and Hydrogen Light Rail. *J. Public Transp.* **2015**, *18*, 74–88. [[CrossRef](#)]
9. Gallas, D.; Stobnicki, P. Adoption of Modern Hydrogen Technologies in Rail Transport. *J. Ecol. Eng.* **2022**, *23*, 84–91. [[CrossRef](#)]
10. Sun, Y.; Anwar, M.; Hassan, N.M.S.; Spiriyagin, M.; Cole, C. A review of hydrogen technologies and engineering solutions for railway vehicle design and operations. *Railw. Eng. Sci.* **2021**, *29*, 212–232. [[CrossRef](#)]
11. Miller, A.R.; Peters, J.; Smith, B.E.; Velev, O.A. Analysis of fuel cell hybrid locomotives. *J. Power Sources* **2006**, *157*, 855–861. [[CrossRef](#)]
12. Hoffrichter, A.; Hillmans, S.; Roberts, C. Review and assessment of hydrogen propelled railway vehicles. In Proceedings of the IET Conference on Railway Traction Systems, Birmingham, UK, 13–15 April 2010.

13. Hoffrichter, A. *Hydrogen-Rail (Hydrail) Development*; H2@ Rail Workshop: Lansing, MI, USA, 2019; pp. 1–4.
14. Yan, Y.; Li, Q.; Chen, W.; Su, B.; Liu, J.; Ma, L. Optimal energy management and control in multimode equivalent energy consumption of fuel cell/supercapacitor of hybrid electric tram. *IEEE Trans. Ind. Electron.* **2018**, *66*, 6065–6076. [[CrossRef](#)]
15. Siwec, J. Use of Hydrogen Fuel Cells in Rail Transport. *Probl. Kolejnictwa* **2021**, *190*, 113–117. [[CrossRef](#)]
16. Calvert, C.; Allan, J.; Amor, P.; Hillmans, S.; Roberts, C.; Weston, P. Concept development and testing of the UK's first hydrogen-hybrid train (HydroFLEX). *Railw. Eng. Sci.* **2021**, *29*, 248–257. [[CrossRef](#)]
17. Ogawa, K.; Yoneyama, T.; Sudo, T.; Kashiwagi, T.; Yamamoto, T. Performance improvement of fuel cell hybrid powered test railway vehicle. *Q. Rep. RTRI* **2021**, *62*, 16–21. [[CrossRef](#)]
18. Durbin, D.J.; Malardier-Jugroot, C. Review of hydrogen storage techniques for on board vehicle applications. *Int. J. Hydrogen Energy* **2013**, *38*, 14595–14617. [[CrossRef](#)]
19. Hassan, I.A.; Ramadan, H.S.; Saleh, M.A.; Hissel, D. Hydrogen storage technologies for stationary and mobile applications: Review, analysis and perspectives. *Renew. Sustain. Energy Rev.* **2021**, *149*, 111311. [[CrossRef](#)]
20. Lahnaoui, A.; Wulf, C.; Heinrichs, H.; Dalmazzone, D. Optimizing hydrogen transportation system for mobility via compressed hydrogen trucks. *Int. J. Hydrogen Energy* **2019**, *44*, 19302–19312. [[CrossRef](#)]
21. Abe, J.O.; Popoola, A.P.I.; Ajenifuja, E.; Popoola, O.M. Hydrogen energy, economy and storage: Review and recommendation. *Int. J. Hydrogen Energy* **2019**, *44*, 15072–15086. [[CrossRef](#)]
22. Kayfeci, M.; Keçebaş, A. Hydrogen storage. In *Solar Hydrogen Production*; Elsevier: Amsterdam, The Netherlands, 2019; pp. 85–110.
23. Xu, X.; Xu, H.; Zheng, J.; Chen, L.; Wang, J. A high-efficiency liquid hydrogen storage system cooled by a fuel-cell-driven refrigerator for hydrogen combustion heat recovery. *Energy Convers. Manag.* **2020**, *226*, 113496. [[CrossRef](#)]
24. Ahluwalia, R.K.; Peng, J.K.; Roh, H.S.; Hua, T.Q.; Houchins, C.; James, B.D. Supercritical cryo-compressed hydrogen storage for fuel cell electric buses. *Int. J. Hydrogen Energy* **2018**, *43*, 10215–10231. [[CrossRef](#)]
25. James, B.D.; Houchins, C.; Huya-Kouadio, J.M.; DeSantis, D.A. *Hydrogen Storage System Cost Analysis*; Strategic Analysis Inc.: Arlington, VA, USA, 2016.
26. Rusman, N.A.A.; Dahari, M. A review on the current progress of metal hydrides material for solid-state hydrogen storage applications. *Int. J. Hydrogen Energy* **2016**, *41*, 12108–12126. [[CrossRef](#)]
27. Ley, M.B.; Jepsen, L.H.; Lee, Y.-S.; Cho, Y.W.; Von Colbe, J.M.B.; Dornheim, M.; Rokni, M.; Jensen, J.O.; Sloth, M.; Filinchuk, Y. Complex hydrides for hydrogen storage—new perspectives. *Mater. Today* **2014**, *17*, 122–128. [[CrossRef](#)]
28. Ponthieu, M.; Fernández, J.; Cuevas, F.; Bodega, J.; Ares, J.R.; Adeva, P.; Sánchez, C. Thermodynamics and reaction pathways of hydrogen sorption in Mg₆ (Pd, TM)(TM = Ag, Cu and Ni) pseudo-binary compounds. *Int. J. Hydrogen Energy* **2014**, *39*, 18291–18301. [[CrossRef](#)]
29. Liu, T.; Wang, C.; Wu, Y. Mg-based nanocomposites with improved hydrogen storage performances. *Int. J. Hydrogen Energy* **2014**, *39*, 14262–14274. [[CrossRef](#)]
30. Smythe, N.C.; Gordon, J.C. Ammonia borane as a hydrogen carrier: Dehydrogenation and regeneration. *Eur. J. Inorg. Chem.* **2010**, *2010*, 509–521. [[CrossRef](#)]
31. Macfarlane, D.R.; Cherepanov, P.V.; Choi, J.; Suryanto, B.H.R.; Hodgetts, R.Y.; Bakker, J.M.; Ferrero Vallana, F.M.; Simonov, A.N. A Roadmap to the Ammonia Economy. *Joule* **2020**, *4*, 1186–1205. [[CrossRef](#)]
32. Alagharu, V.; Palanki, S.; West, K.N. Analysis of ammonia decomposition reactor to generate hydrogen for fuel cell applications. *J. Power Sources* **2010**, *195*, 829–833. [[CrossRef](#)]
33. Davoodabadi, A.; Mahmoudi, A.; Ghasemi, H. The potential of hydrogen hydrate as a future hydrogen storage medium. *Iscience* **2021**, *24*, 101907. [[CrossRef](#)]
34. USDoE. Hydrogen Sorption Center of Excellence (HSCoE) Final Report. Available online: <https://www.energy.gov/eere/fuelcells/downloads/hydrogen-sorption-center-excellence-hscoe-final-report> (accessed on 7 March 2014).
35. Xia, Y.; Yang, Z.; Zhu, Y. Porous carbon-based materials for hydrogen storage: Advancement and challenges. *J. Mater. Chem. A* **2013**, *1*, 9365. [[CrossRef](#)]
36. Ramirez-Vidal, P.; Sdanghi, G.; Celzard, A.; Fierro, V. High hydrogen release by cryo-adsorption and compression on porous materials. *Int. J. Hydrogen Energy* **2022**, *47*, 8892–8915. [[CrossRef](#)]
37. Ahluwalia, R.; Peng, J. Automotive hydrogen storage system using cryo-adsorption on activated carbon. *Int. J. Hydrogen Energy* **2009**, *34*, 5476–5487. [[CrossRef](#)]
38. Stamatakis, E.; Zoulias, E.; Tzamalis, G.; Massina, Z.; Analytis, V.; Christodoulou, C.; Stubos, A. Metal hydride hydrogen compressors: Current developments & early markets. *Renew. Energy* **2018**, *127*, 850–862.
39. Tarasov, B.P.; Fursikov, P.V.; Volodin, A.A.; Bocharnikov, M.S.; Shimkus, Y.Y.; Kashin, A.M.; Yartys, V.A.; Chidziva, S.; Pasupathi, S.; Lototskiy, M.V. Metal hydride hydrogen storage and compression systems for energy storage technologies. *Int. J. Hydrogen Energy* **2021**, *46*, 13647–13657. [[CrossRef](#)]
40. Rivard, E.; Trudeau, M.; Zaghbi, K. Hydrogen Storage for Mobility: A Review. *Materials* **2019**, *12*, 1973. [[CrossRef](#)]
41. Li, M.; Bai, Y.; Zhang, C.; Song, Y.; Jiang, S.; Grouset, D.; Zhang, M. Review on the research of hydrogen storage system fast refueling in fuel cell vehicle. *Int. J. Hydrogen Energy* **2019**, *44*, 10677–10693. [[CrossRef](#)]
42. Hua, T.Q.; Ahluwalia, R.K.; Peng, J.K.; Kromer, M.; Lasher, S.; McKenney, K.; Law, K.; Sinha, J. Technical assessment of compressed hydrogen storage tank systems for automotive applications. *Int. J. Hydrogen Energy* **2011**, *36*, 3037–3049. [[CrossRef](#)]

43. USDoE. DOE Technical Targets for Onboard Hydrogen Storage for Light-Duty Vehicles. Available online: <https://www.energy.gov/eere/fuelcells/doe-technical-targets-onboard-hydrogen-storage-light-duty-vehicles> (accessed on 1 November 2021).
44. James, B.D.; Houchins, C. 700 Bar Type IV H2 Pressure Vessel Cost Projections. Available online: https://www.energy.gov/sites/prod/files/2016/09/f33/fcto_h2_storage_700bar_workshop_2_james.pdf (accessed on 24 August 2016).
45. Din, T.; Hillmansen, S. Energy consumption and carbon dioxide emissions analysis for a concept design of a hydrogen hybrid railway vehicle. *IET Electr. Syst. Transp.* **2018**, *8*, 112–121. [[CrossRef](#)]
46. Gallucci, M. Hydrogen trains roll into service: A new hybrid locomotive signals a growing push for zero-emission rail technologies—[News]. *IEEE Spectr.* **2019**, *56*, 6–7. [[CrossRef](#)]
47. Ku, B.-Y. September 2021 Land Transportation News [Transportation Systems]. *IEEE Veh. Technol. Mag.* **2021**, *16*, 14–17. [[CrossRef](#)]
48. Fedele, E.; Iannuzzi, D.; Del Pizzo, A. Onboard energy storage in rail transport: Review of real applications and techno-economic assessments. *IET Electr. Syst. Transp.* **2021**, *11*, 279–309. [[CrossRef](#)]
49. Alstom. Successful Year and a Half of Trial Operation of the World’s First Two Hydrogen Trains, Next Project Phase Begins. Available online: <https://www.alstom.com/press-releases-news/2020/5/successful-year-and-half-trial-operation-worlds-first-two-hydrogen> (accessed on 19 May 2020).
50. Stetson, N.T.; McWhorter, S.; Ahn, C.C. *Compendium of Hydrogen Energy: Hydrogen Storage, Distribution and Infrastructure*; Woodhead Publishing: Sawston, UK, 2015; Volume 2, pp. 3–25.
51. Yanxing, Z.; Maoqiong, G.; Yuan, Z.; Xueqiang, D.; Jun, S. Thermodynamics analysis of hydrogen storage based on compressed gaseous hydrogen, liquid hydrogen and cryo-compressed hydrogen. *Int. J. Hydrogen Energy* **2019**, *44*, 16833–16840. [[CrossRef](#)]
52. Ahluwalia, R.; Hua, T.; Peng, J.; Kumar, R. System level analysis of hydrogen storage options. In *DOE Hydrogen Program Annual Review*; DOE: Washington, DC, USA, 2010.
53. Ahluwalia, R.; Hua, T.; Peng, J.; Kumar, R. System level analysis of hydrogen storage options. In *DOE Hydrogen Program Annual Review*; DOE: Washington, DC, USA, 2020.
54. Aziz, M.; Oda, T.; Kashiwagi, T. Comparison of liquid hydrogen, methylcyclohexane and ammonia on energy efficiency and economy. *Energy Procedia* **2019**, *158*, 4086–4091. [[CrossRef](#)]
55. Peng, J.K.; Ahluwalia, R.K. Enhanced dormancy due to para-to-ortho hydrogen conversion in insulated cryogenic pressure vessels for automotive applications. *Int. J. Hydrogen Energy* **2013**, *38*, 13664–13672.
56. Agarwal, R.; Dondapati, R.S. Numerical investigation on hydrodynamic characteristics of two-phase flow with liquid hydrogen through cryogenic feed lines at terrestrial and microgravity. *Appl. Therm. Eng.* **2020**, *173*, 115240. [[CrossRef](#)]
57. Thomas, J.M.; Edwards, P.P.; Dobson, P.J.; Owen, G.P. Decarbonising energy: The developing international activity in hydrogen technologies and fuel cells. *J. Energy Chem.* **2020**, *51*, 405–415. [[CrossRef](#)]
58. Kang, D.; Yun, S.; Kim, B.-K. Review of the Liquid Hydrogen Storage Tank and Insulation System for the High-Power Locomotive. *Energies* **2022**, *15*, 4357. [[CrossRef](#)]
59. Siebel, T. Pressure in the Hydrogen Tank. *ATZ Worldw.* **2021**, *123*, 8–13.
60. Rao, A.G.; Yin, F.; Werij, H. Energy Transition in Aviation: The Role of Cryogenic Fuels. *Aerospace* **2020**, *7*, 181. [[CrossRef](#)]
61. Gupta, R.K.; Basile, A.; Veziroglu, T.N. *Compendium of Hydrogen Energy*; Woodhead Publishing: Cambridge, UK, 2016; Volume 2.
62. Barthélémy, H.; Weber, M.; Barbier, F. Hydrogen storage: Recent improvements and industrial perspectives. *Int. J. Hydrogen Energy* **2017**, *42*, 7254–7262. [[CrossRef](#)]
63. Moreno-Blanco, J.; Petitpas, G.; Espinosa-Loza, F.; Elizalde-Blancas, F.; Martinez-Frias, J.; Aceves, S.M. The storage performance of automotive cryo-compressed hydrogen vessels. *Int. J. Hydrogen Energy* **2019**, *44*, 16841–16851. [[CrossRef](#)]
64. Ahluwalia, R.K.; Hua, T.Q.; Peng, J.K.; Lasher, S.; McKenney, K.; Sinha, J.; Gardiner, M. Technical assessment of cryo-compressed hydrogen storage tank systems for automotive applications. *Int. J. Hydrogen Energy* **2010**, *35*, 4171–4184. [[CrossRef](#)]
65. Shafiei, E.; Davidsdottir, B.; Leaver, J.; Stefansson, H.; Asgeirsson, E.I. Comparative analysis of hydrogen, biofuels and electricity transitional pathways to sustainable transport in a renewable-based energy system. *Energy* **2015**, *83*, 614–627. [[CrossRef](#)]
66. Zhan, X.; Yan, Y.; Wei, W.; Dongke, S.; Zhonghua, N. Supply system of cryo-compressed hydrogen for fuel cell stacks on heavy duty trucks. *Int. J. Hydrogen Energy* **2020**, *45*, 12921–12931.
67. Yan, Y.; Xu, Z.; Han, F.; Wang, Z.; Ni, Z. Energy control of providing cryo-compressed hydrogen for the heavy-duty trucks driving. *Energy* **2021**, *242*, 122817. [[CrossRef](#)]
68. Chen, L.; Xiao, R.; Cheng, C.; Tian, G.; Chen, S.; Hou, Y. Thermodynamic analysis of the para-to-ortho hydrogen conversion in cryo-compressed hydrogen vessels for automotive applications. *Int. J. Hydrogen Energy* **2020**, *45*, 24928–24937. [[CrossRef](#)]
69. Ahluwalia, R.K.; Papadias, D.; Peng, J.-K.; Krause, T. Total Cost of Ownership for Line Haul, Yard Switchers and Regional Passenger Locomotives –Preliminary Results. In Proceedings of the 2019 US DOE Hydrogen Program Annual Merit Review, Crystal City, VA, USA, 29 April–1 May 2019.
70. Aceves, S.; Brunner, T. *Hydrogen Storage Tests for Cryo-Compressed Vessels, CRADA No. TC02119.0*; Lawrence Livermore National Lab.(LLNL): Livermore, CA, USA, 2021.
71. Petitpas, G. *1,000+ Cycles of a 350 Bar Prototype Cryo-Compressed Pressure Vessel*; Lawrence Livermore National Lab.(LLNL): Livermore, CA, USA, 2018.
72. James, B.D.; Houchins, C.; Huya-Kouadio, J.; DeSantis, D. Hydrogen Storage Cost Analysis. In Proceedings of the US DOE Hydrogen and Fuel Cells Program Annual Merit Review, Washington, DC, USA, 13–15 June 2018.

73. Geiling, J.; Steinberger, M.; Ortner, F.; Seyfried, R.; Nuß, A.; Uhrig, F.; Lange, C.; Öchsner, R.; Wasserscheid, P.; März, M.; et al. Combined dynamic operation of PEM fuel cell and continuous dehydrogenation of perhydro-dibenzyltoluene. *Int. J. Hydrogen Energy* **2021**, *46*, 35662–35677. [[CrossRef](#)]
74. Rao, P.C.; Yoon, M. Potential liquid-organic hydrogen carrier (LOHC) systems: A review on recent progress. *Energies* **2020**, *13*, 6040. [[CrossRef](#)]
75. Niermann, M.; Timmerberg, S.; Drünert, S.; Kaltschmitt, M. Liquid Organic Hydrogen Carriers and alternatives for international transport of renewable hydrogen. *Renew. Sustain. Energy Rev.* **2021**, *135*, 110171. [[CrossRef](#)]
76. Preuster, P.; Papp, C.; Wasserscheid, P. Liquid organic hydrogen carriers (LOHCs): Toward a hydrogen-free hydrogen economy. *Acc. Chem. Res.* **2017**, *50*, 74–85. [[CrossRef](#)]
77. Gonda, M.; Ohshima, M.A.; Kurokawa, H.; Miura, H. Toluene hydrogenation over Pd and Pt catalysts as a model hydrogen storage process using low grade hydrogen containing catalyst inhibitors. *Int. J. Hydrogen Energy* **2014**, *39*, 16339–16346. [[CrossRef](#)]
78. Mizuno, Y.; Ishimoto, Y.; Sakai, S.; Sakata, K. Economic analysis on international hydrogen energy carrier supply chains. *J. Jpn. Soc. Energy Resour.* **2016**, *38*, 11–17.
79. Wijayanta, A.T.; Oda, T.; Purnomo, C.W.; Kashiwagi, T.; Aziz, M. Liquid hydrogen, methylcyclohexane, and ammonia as potential hydrogen storage: Comparison review. *Int. J. Hydrogen Energy* **2019**, *44*, 15026–15044. [[CrossRef](#)]
80. Hurskainen, M.; Ihonen, J. Techno-economic feasibility of road transport of hydrogen using liquid organic hydrogen carriers. *Int. J. Hydrogen Energy* **2020**, *45*, 32098–32112. [[CrossRef](#)]
81. Aakko-Saksa, P.T.; Cook, C.; Kiviahio, J.; Repo, T. Liquid organic hydrogen carriers for transportation and storing of renewable energy—Review and discussion. *J. Power Sources* **2018**, *396*, 803–823. [[CrossRef](#)]
82. Fikrt, A.; Brehmer, R.; Milella, V.-O.; Müller, K.; Bösmann, A.; Preuster, P.; Alt, N.; Schlücker, E.; Wasserscheid, P.; Arlt, W. Dynamic power supply by hydrogen bound to a liquid organic hydrogen carrier. *Appl. Energy* **2017**, *194*, 1–8. [[CrossRef](#)]
83. Ezzat, M.; Dincer, I. Comparative assessments of two integrated systems with/without fuel cells utilizing liquefied ammonia as a fuel for vehicular applications. *Int. J. Hydrogen Energy* **2018**, *43*, 4597–4608. [[CrossRef](#)]
84. Ezzat, M.; Dincer, I. Development and assessment of a new hybrid vehicle with ammonia and hydrogen. *Appl. Energy* **2018**, *219*, 226–239. [[CrossRef](#)]
85. Al-Hamed, K.H.; Dincer, I. A novel ammonia solid oxide fuel cell-based powering system with on-board hydrogen production for clean locomotives. *Energy* **2021**, *220*, 119771. [[CrossRef](#)]
86. Al-Hamed, K.H.; Dincer, I. Investigation of an integrated powering system for clean locomotives with solid-oxide fuel cell with heat recovery organic Rankine cycle. *Energy Convers. Manag.* **2020**, *219*, 112857. [[CrossRef](#)]
87. Lamb, K.E.; Dolan, M.D.; Kennedy, D.F. Ammonia for hydrogen storage; A review of catalytic ammonia decomposition and hydrogen separation and purification. *Int. J. Hydrogen Energy* **2019**, *44*, 3580–3593. [[CrossRef](#)]
88. Lan, R.; Irvine, J.T.; Tao, S. Ammonia and related chemicals as potential indirect hydrogen storage materials. *Int. J. Hydrogen Energy* **2012**, *37*, 1482–1494. [[CrossRef](#)]
89. Ezzat, M.F.; Dincer, I. Energy and exergy analyses of a novel ammonia combined power plant operating with gas turbine and solid oxide fuel cell systems. *Energy* **2020**, *194*, 116750. [[CrossRef](#)]
90. Barelli, L.; Bidini, G.; Cinti, G. Operation of a Solid Oxide Fuel Cell Based Power System with Ammonia as a Fuel: Experimental Test and System Design. *Energies* **2020**, *13*, 6173. [[CrossRef](#)]
91. Valera-Medina, A.; Xiao, H.; Owen-Jones, M.; David, W.I.; Bowen, P. Ammonia for power. *Prog. Energy Combust. Sci.* **2018**, *69*, 63–102. [[CrossRef](#)]
92. Chai, W.S.; Bao, Y.; Jin, P.; Tang, G.; Zhou, L. A review on ammonia, ammonia-hydrogen and ammonia-methane fuels. *Renew. Sustain. Energy Rev.* **2021**, *147*, 111254. [[CrossRef](#)]
93. Afif, A.; Radenahmad, N.; Cheok, Q.; Shams, S.; Kim, J.H.; Azad, A.K. Ammonia-fed fuel cells: A comprehensive review. *Renew. Sustain. Energy Rev.* **2016**, *60*, 822–835. [[CrossRef](#)]
94. James, B.D.; DeSantis, D.A. *Manufacturing Cost and Installed Price Analysis of Stationary Fuel Cell Systems*; Strategic Analysis Inc.: Arlington, VA, USA, 2015.
95. Stanescu, A.; Mocioi, N.; Dimitrescu, A. Hybrid Propulsion Train with Energy Storage in Metal Hydrides. In Proceedings of the Electric Vehicles International Conference (EV), Bucharest, Romania, 3–4 October 2019; IEEE: Bucharest, Romania, 2019; pp. 1–4.
96. Davids, M.; Lototsky, M.; Malinowski, M.; Van Schalkwyk, D.; Parsons, A.; Pasupathi, S.; Swanepoel, D.; van Niekerk, T. Metal hydride hydrogen storage tank for light fuel cell vehicle. *Int. J. Hydrogen Energy* **2019**, *44*, 29263–29272. [[CrossRef](#)]
97. Lototsky, M.; Tolj, I.; Klochko, Y.; Davids, M.W.; Swanepoel, D.; Linkov, V. Metal hydride hydrogen storage tank for fuel cell utility vehicles. *Int. J. Hydrogen Energy* **2020**, *45*, 7958–7967. [[CrossRef](#)]
98. Falahati, H.; Barz, D.P.J. Evaluation of hydrogen sorption models for AB5-type metal alloys by employing a gravimetric technique. *Int. J. Hydrogen Energy* **2013**, *38*, 8838–8851. [[CrossRef](#)]
99. Szajek, A.; Jurczyk, M.; Okońska, I.; Smardz, K.; Jankowska, E.; Smardz, L. Electrochemical and electronic properties of nanocrystalline Mg-based hydrogen storage materials. *J. Alloys Compd.* **2007**, *436*, 345–350. [[CrossRef](#)]
100. Wang, P.; Kang, X.-d. Hydrogen-rich boron-containing materials for hydrogen storage. *Dalton Trans.* **2008**, 5400–5413. [[CrossRef](#)] [[PubMed](#)]
101. Züttel, A.; Wenger, P.; Rentsch, S.; Sudan, P.; Mauron, P.; Emmenegger, C. LiBH₄ a new hydrogen storage material. *J. Power Sources* **2003**, *118*, 1–7. [[CrossRef](#)]

102. Gross, K.; Sandrock, G.; Thomas, G. Dynamic in situ X-ray diffraction of catalyzed alanates. *J. Alloys Compd.* **2002**, *330*, 691–695. [[CrossRef](#)]
103. Jensen, C.; Gross, K. Development of catalytically enhanced sodium aluminum hydride as a hydrogen-storage material. *Appl. Phys. A* **2001**, *72*, 213–219. [[CrossRef](#)]
104. Urbanczyk, R.; Peinecke, K.; Felderhoff, M.; Hauschild, K.; Kersten, W.; Peil, S.; Bathen, D. Aluminium alloy based hydrogen storage tank operated with sodium aluminium hexahydride Na₃AlH₆. *Int. J. Hydrogen Energy* **2014**, *39*, 17118–17128. [[CrossRef](#)]
105. USDoE. System Projection Graphs. Available online: <https://www.energy.gov/eere/fuelcells/hydrogen-storage-engineering-center-excellence#graphs> (accessed on 8 March 2022).
106. De Castro, J.F.R.; Santos, S.F.; Costa, A.L.M.; Yavari, A.R.; Botta F, W.J.; Ishikawa, T.T. Structural characterization and dehydrogenation behavior of Mg–5 at.%Nb nano-composite processed by reactive milling. *J. Alloys Compd.* **2004**, *376*, 251–256. [[CrossRef](#)]
107. Kang, X.-D.; Luo, J.-H.; Wang, P. Efficient and highly rapid hydrogen release from ball-milled 3NH₃BH₃/MMgH₃ (M = Na, K, Rb) mixtures at low temperatures. *Int. J. Hydrogen Energy* **2012**, *37*, 4259–4266. [[CrossRef](#)]
108. USDoE. Hydrogen Storage Tech Team Roadmap. Available online: https://www.energy.gov/sites/prod/files/2017/08/f36/hst_t_roadmap_July2017.pdf (accessed on 30 July 2017).
109. USDoE. DOE Hydrogen and Fuel Cells Program Record#15013. Available online: https://www.hydrogen.energy.gov/pdfs/15013_onboard_storage_performance_cost.pdf (accessed on 30 September 2015).
110. USDoE. System Level Analysis of Hydrogen Storage Options. Available online: https://www.hydrogen.energy.gov/pdfs/review17/st001_ahluwalia_2017_o.pdf (accessed on 5 June 2017).
111. USDoE. Hydrogen Storage Engineering Center of Excellence-Savannah River National Laboratory (Anton). Available online: https://www.hydrogen.energy.gov/pdfs/review16/st004_anton_2016_o.pdf (accessed on 9 June 2016).
112. USDoE. Department of Energy Hydrogen Program Plan. Available online: https://www.hydrogen.energy.gov/roadmaps_vision.html (accessed on 30 November 2020).