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Authors:

Mauricio Chiliquinga, Patricio J. Espinoza-Montero, Oscar Rodríguez, Alain Picos, Erick R. Bandala, S. Gutiérrez-Granados, Juan M. Peralta-Hernández

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Article

Simultaneous Electrochemical Generation of Ferrate and Oxygen Radicals to Blue BR Dye Degradation

Mauricio Chiliquinga ^{1,2}, Patricio J. Espinoza-Montero ^{3,*}, Oscar Rodríguez ², Alain Picos ², Erick R. Bandala ⁴, S. Gutiérrez-Granados ² and Juan M. Peralta-Hernández ^{2,*}

- ¹ Departamento de Ingeniería Civil y Ambiental, Facultad de Ingeniería Civil y Ambiental, Escuela Politécnica Nacional. P.O. Box, Quito 17-01-2759, Ecuador; mauricioacade14@hotmail.com
- ² Departamento de Química, División de Ciencias Naturales y Exactas, Universidad de Guanajuato, Cerro de la Venada s/n, Pueblito de Rocha, Guanajuato 36040, Mexico;
- om.rodrigueznarvaez@ugto.mx (O.R.); picosbrother@hotmail.com (A.P.); gutigs59@hotmail.com (S.G.-G.) ³ Escuela de Ciencias Químicas, Pontificia Universidad Católica del Ecuador, Avenida 12 de Octubre y Roca,
- Apartado, Quito 17-01-2184, Ecuador
 Divicion of Hydrologic Sciences, Desert Research Institute, 755 F. Elamingo Road
- ⁴ Division of Hydrologic Sciences, Desert Research Institute, 755 E. Flamingo Road, Las Vegas, NV 89119-7363, USA; Erick.Bandala@dri.edu
- * Correspondence: pespinoza646@puce.edu.ec (P.J.E.-M.); juan.peralta@ugto.mx (J.M.P.-H.); Tel.: +593-2299-1700 (ext. 1929) (P.J.E.-M.); +52-4737327555 (ext. 5416) (J.M.P.-H.)

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Abstract: In this study, electro-oxidation (EOx) and in situ generation of ferrate ions [Fe(VI)] were tested to treat water contaminated with Blue BR dye (BBR) using a boron-doped diamond (BDD) anode. Two electrolytic media (0.1 M HClO₄ and 0.05 M Na₂SO₄) were evaluated for the BDD, which simultaneously produced oxygen radicals (•OH) and [Fe(VI)]. The generation of [Fe(VI)] was characterized by cyclic voltammetry (CV) and the effect of different current intensity values (e.g., 7 mA cm⁻², 15 mA cm⁻², and 30 mA cm⁻²) was assessed during BBR degradation tests. The discoloration of BBR was followed by UV-Vis spectrophotometry. When the EOx process was used alone, only 78% BBR discoloration was achieved. The best electrochemical discoloration conditions were found using 0.05 M Na₂SO₄ and 30 mA cm⁻². Using these conditions, overall BBR discoloration values up to 98%, 95%, and 87% with 12 mM, 6 mM, and 1 mM of FeSO₄, respectively, were achieved. In the case of chemical oxygen demand (COD) reduction, the EOx process showed only a 37% COD reduction, whereas combining [Fe(VI)] generation using 12 mM of FeSO₄ achieved an up to 61% COD reduction after 90 min. The evolution of reaction byproducts (oxalic acid) was performed using liquid chromatography analysis.

Keywords: advace oxitadion processes (AOP); electro-oxidation; ferrate ion; BBR dye

1. Introduction

Industrial effluents contain a wide variety of pollutants that are potentially harmful to humans, such as dyes and organic compounds, and most of these pollutants are difficult to remove using conventional water treatment systems (e.g., physicochemical, and/or biological processes) [1]. When released into the environment without the proper treatment, these effluents produce significant fluctuations in water quality parameters such as chemical oxygen demand (COD), biological oxygen demand (BOD), pH, color, and/or salinity [2], which increase public concerns when the proper treatments are not being implemented. Therefore, finding alternative treatment processes that are suitable to remove highly recalcitrant pollutants in industrial wastewater effluents is a pending science and technology need.

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An alternative for water treatment known since the 1970s has been ferrate(VI) ion (FeO₄^{2–}), a very strong, chemically green oxidizer, highly stable in aqueous medium, especially at alkaline and neutral pH, where iron shows oxidation state +6 [3–6]. However, we must emphasize that ferrate's highest oxidizing power occurs preferably in an acidic medium, and decreases in alkaline pH (reaction 1 and 2) [4,7].

$$FeO_4^{2-} + 8H^+ + 3e^- \rightleftharpoons Fe^{3+} + 4H_2O$$
 $E^\circ = +2.20 \text{ V vs. SHE}$ (1)

$$FeO_4^{2-} + 2H_2O + 3e^- \rightleftharpoons Fe(OH)_3 + 5OH^- \qquad E^\circ = +0.72 \text{ V vs. SHE}$$
 (2)

Ferrate anions can exist in various oxidation states: $[FeO_4]^{2-}$ with Fe(VI), $[FeO_4]^{3-}$ with Fe(V) or $[FeO_4]^{4-}$ with Fe(IV) [8]. However, Fe(VI) is the most stable form with broad industrial uses. The unique chemical properties of ferrate (VI) include:

- (a) High redox potential, with the ability to oxidize harmful organic and inorganic species such as nitrosamines, phenol, nitrilotriacetic acid, hydrazine, thiourea, sulfides, cyanide, thioacetamide, ammonia, thiocyanate, soluble oils, as well as inactivate viruses and bacteria [5,8–11].
- (b) A bifunctional ability to act as oxidizing and coagulating agent, due to the simultaneous release of ferric ions (Fe(III)), specifically under neutral or alkaline conditions [12–14].
- (c) A higher redox potential than other oxidizers commonly used for water treatment such as chlorine (1.358 V vs. SHE), hydrogen peroxide (1.776 V vs. SHE), and ozone (2.076 V vs. SHE) [15].
- (d) Ferrate use prevents the formation of carcinogenic disinfection byproducts (mainly trihalomethanes).
- (e) It generates non-toxic reduction byproducts such as Fe(III) and Fe(II), which can be used for other purposes.
- (f) Ferrate can also be used for biofouling control and for the removal of other contaminants such as metals, non-metals, and radionuclides [16–18].

Boron-doped diamond (BDD) electrodes have an inert surface, a wide electrochemical window, low adsorption, high corrosion resistance, and electrochemical stability. These electrodes are also considered a suitable surface upon which to carry out electro-oxidation (EOx) processes [19]. They have greater O₂ evolution overpotential than other electrodes (e.g., Pt and PbO₂) and low water oxidation reaction, combined with the capability to generate large amounts of oxygen radicals (e.g., •OH) [20]. Recent studies suggest that ferrate ions can be generated in situ from Fe(II) salts using a BDD anode surface under acidic conditions (0.1 M HClO₄) by applying a potential of 2.2 V vs. NHE [21].

Despite the existing information about the potential of ferrate for water treatment [22–27] and the attractive features of its generation in situ by EOx processes, more research is needed to identify the best reaction conditions to treat complex industrial effluents using this technology. The goal of this work was to investigate the best conditions to generate ferrate ions in situ using a BDD electrode by cyclic voltammetry as well as assess the feasibility of using in situ generated ferrate simultaneously with the EOx process to degrade a textile dye (e.g., Blue BR (BBR) dye), following water discoloration, COD abatement, as well as an assessment of the evolution of reaction byproducts (e.g., carboxylic acids).

As is well known, the interest in studying the electrochemical generation of the ferrate ion on boron-doped diamond (BDD) electrodes, has gained great relevance; this due to its potential applications in the environmental area, specifically in water treatment. This paper presents results on the simultaneous production of the ferrate ion and free radicals on a BDD surface; studies of the generation of both species in two different electrolytes and with the addition of different concentrations of iron sulfate are presented, we also study the effect of the current density on the degradation of an industrial dye; for this, the level of discoloration, reduction in COD and the evolution of a byproduct, namely carboxylic acid, are considered. We consider this research to be relevant because we present important results on how the action of both oxidants generated on the same electrode simultaneously will improve the degradation of the dye, which enhances its application in water treatment.

2. Materials and Methods

2.1. Materials

All reagents used in this investigation—perchloric acid (HClO₄), ferrous sulfate (FeSO₄·7H₂O), sodium sulfate (Na₂SO₄), and sulfuric acid (H₂SO₄)—were obtained from Aldrich and J.T. Baker and used without any purification. The industrial grade BBR dye ($C_{32}H_{28}N_2Na_2O_8S_2$), widely used in the tanning industry in Mexico, was supplied by PCL (Guanajuato, Mexico). The BDD electrode was obtained from MetakemTM (Germany).

2.2. Electrochemical Characterization

The redox behavior of FeSO₄ on BDD was evaluated by CV, employing a three-electrode cell: BDD as an anode (0.5 cm²), Pt wire as a counter electrode, and Ag/AgCl as the reference electrode, using the BASi potentiostat/galvanostat and Epsilon-EC software at a scan rate ranging from 100 mV s⁻¹ to 500 mV s⁻¹. As an electrolyte (blank), we used 0.1 M HClO₄ with 6 mM of FeSO₄ as analyte.

Additionally, the electrochemical response by cyclic voltammetry (CV) of three FeSO₄ concentrations (1 mM, 6 mM, and 12 mM), in two different electrolytes 0.1 M HClO₄ and 0.05 M Na₂SO₄ (adjusted to pH 3 with H₂SO₄) was evaluated. The experiments were performed in a three-electrode electrochemical cell (25 mL), using a BDD (0.5 cm^2) plate as a working electrode, platinum (Pt) wire as a counter electrode, and Ag/AgCl as a reference electrode. The CV tests were performed using a BASi Epsilon potentiostat/galvanostat. Specific concentrations of FeSO₄ were prepared from a stock solution in 100 mL of distilled water and added to the media in all the [Fe(VI)] production experiments.

2.3. Electrochemical Set Up

The discoloration assays were carried out in galvanostatic mode using three different current density values (e.g., 7 mA cm², 15 mA cm², and 30 mA cm²) in a 100 mL tank reactor with constant magnetic stirring (200 rpm). One initial BBR dye concentration (50 mg/L) was used for all the experimental trials. The BBR dye (chemical formula = $C_{32}H_{28}N_2Na_2O_8S_2$, molecular weight = 678.68 g/mol, and λ_{max} = 695 nm) was used in this study. An accurately weighed quantity of the dye was dissolved in distilled water to prepare the stock solution (100 mg L⁻¹). Experimental solutions of desired concentration (50 mg/L) were obtained by successive dilution. The surface area of the BDD anode was 2.5 cm² and a Pt wire was used as the cathode. The study solution was monitored for color reduction using a UV-Vis spectrophotometer (Cintra 1010 device) at λ = 695 nm [27].

Water discoloration was carried out by testing two electrolytic media: 0.1 M HClO_4 and 0.05 MNa₂SO₄ adjusted to pH 3 with H₂SO₄. In both cases, three different FeSO₄ concentrations (1 mM, 6 mM, and 12 mM) were tested. To evaluate the amount of remaining oxidable material in solution, the chemical oxygen demand (COD) was quantified according to the Standard Methods (method 5220D); total nitrogen concentration was also estimated by the Standard Methods [28].

For the different parameters tested, the kinetics approach of the combined electrochemical degradation of BBR dye was determined by a pseudo-first order model, $Ln(A_0/A_t) = kt$, where A_0 is the initial absorbance, A_t is the absorbance after degradation time t, and k is the apparent rate constant.

Carboxylic acids were identified and quantified by ion-exclusion HPLC using an Agilent Technologies 1260 Infinity Series with a Bio-Rad Aminex HPX 87H (300 mm × 7.8 mm) column at 35 °C and by setting the photodiode detector at $\lambda = 210$ nm. For these determinations, 20 µL of the sample was injected into the HPLC, using 4 mM of H₂SO₄ as the mobile phase and flow rate 0.8 mL/min [29–32]. The quantification of the COD was carried out only for the best BBR degradation conditions (e.g., electrolytic solution of 0.05 M of Na₂SO₄ at a pH of 3, current density of 30 mA cm⁻², and 12 mM of FeSO₄) following the Standard Methods [29].

3. Results and Discussion

3.1. Cyclic Voltammetric (CV) Study

Figure 1 shows the redox behavior of 6 mM of FeSO₄ on BDD at different scan rates (100 mV s⁻¹ to 500 mV s⁻¹) using 0.1 M HClO₄ as electrolyte. It is worth emphasizing that the linear behavior of the second peaks agree with the Randles–Sevcik equation (I_p vs. (scan rate)^{1/2}) (data not shown), indicating a diffusion-controlled process where the redox species are not adsorbed on the surface of the electrode [33]. In this study, oxidation peaks from Fe(II) to Fe(III) were observed at 0.54 V vs. Ag/AgCl, the overoxidation of Fe(III) to [Fe(VI)] was found at 0.90 V vs. Ag/AgCl, and reduction to Fe(II) was identified at 0.25 V vs. Ag/AgCl. These results support the theory of in situ formation of [Fe(VI)] on the BDD surface, as shown in Figure 1 [34]. In Figure 2 the electrogeneration of the ferrate ion can be confirmed as the concentration of FeSO₄ increases both the oxidation signal from Fe(II) to Fe(III) and the oxidation signal from Fe(III) to [Fe(VI)] increases proportionally. The number of oxidation and reduction signals matches with those described for Figure 1, even though a slight displacement in the potential axis was observed, probably related to the amount of $FeSO_4$ used for the media. However, ferrate ion production was found to increase as the concentration of FeSO₄ increased [35]. In a previous work, our research group suggested ferrate ion formation at potential values close to 2.5 V Ag/AgCl, using 0.1 M HClO₄ [21,35]. The difference in the oxidation and over-oxidation reaction behavior of Fe(II) to Fe(III) and Fe(VI), respectively, observed in this study could be related to the composition of the electrode surface ($C-sp^2/C-sp^3$ ratio), usage time, and the composition of BDD during its syntheses (e.g., doping level, or precursor used) [36].



Figure 1. Behavior of 6 mM FeSO₄ at different voltammetric scan rate, in 0.1 M HClO₄, on 0.5 borondoped diamond (BDD) cm² as working electrode; counter electrode—platinum wire.



Figure 2. Voltammetric response of $FeSO_4$ at different concentrations in 0.1 M HClO₄, with BDD 0.5 cm² as working electrode, scanning speed 50 mV s⁻¹; counter electrode—platinum wire.

Figure 3 shows the redox behavior of 6 mM FeSO₄ on BDD, at different scan rates (50 mV s⁻¹ to 100 mV s⁻¹) using 0.05 M Na₂SO₄ as electrolyte after adjusting pH to 3 with concentrated H₂SO₄. Two signals for oxidation from Fe(II) to Fe(III) at -0.30 V vs. Ag/AgCl were identified, plus another for overoxidation of Fe(II) to Fe(VI) at 0.78 V vs. Ag/AgCl. Figure 4 shows the effect of FeSO₄ concentration when a constant scan rate (50 mV s⁻¹) was used. It is worth noting that at increased concentrations of FeSO₄, the oxidation and reduction signals increase slightly and move significantly towards higher values of both oxidation and reduction potential. In addition, the second oxidation signal appeared at a lower potential value when Na₂SO₄ was used as the electrolyte (0.78 V, Figure 4), compared with the signal obtained when HClO₄ was used as the electrolyte (0.90 V, Figure 2). Therefore, better degradation of BBR would be expected when Na₂SO₄ is used as the electrolyte, as this reaction media would favor the formation of ferrate ion at lower potential values [37].



Figure 3. Behavior of 6 mM FeSO₄ at different voltammetric scan rate, $0.05 \text{ M Na}_2\text{SO}_4$, on BDD 0.5 cm^2 as working electrode; counter electrode—platinum wire.



Figure 4. Voltammetric response of FeSO₄ at different concentrations, $0.05 \text{ M} \text{ Na}_2 \text{SO}_4$, on BDD 0.5 cm^2 as working electrode, scan rate 50 mV s⁻¹; counter electrode—platinum wire.

3.2. BBR Dye Degradation

3.2.1. Effect of the Electrolyte on the EOx Discoloration Process

The effect of the electrolyte type on the EOx discoloration was explored first. Figure 5 shows the discoloration curves as a function of reaction time for $HClO_4$ (Figure 5a) and Na_2SO_4 (Figure 5b) at the different current density values tested (e.g., 7 mA cm⁻², 15 mA cm⁻², and 30 mA cm⁻²). As shown, no significant difference was found when the lower current density (7 mA cm⁻²) was tested

independently of the electrolyte type used. Nevertheless, a significant difference was found when higher current density values were tested. For example, an overall discoloration of 23% was achieved using 15 mA cm^{-2} and 0.1 M HClO_4 , whereas up to 62% of overall discoloration (over twice the amount achieved reached for HClO₄) was achieved when $0.05 \text{ M Na}_2\text{SO}_4$ was used as the electrolyte.



Figure 5. Removal of an aqueous solution of Blue BR (BBR) azo dye, $C_0 = 50 \text{ mg/L}$, during the oxidation process in (**a**) 0.1 M of HClO₄ and (**b**) 0.05 M Na₂SO₄ with a solution volume of 0.1 L.

When the highest current density (30 mA cm⁻²) was tested, the overall water discoloration achieved after 60 min was 49% for 0.1 M HClO₄, whereas the trials using 0.05 M Na₂SO₄ showed an overall water discoloration as high as 82%. It is worth noting that HClO₄ consistently produced lower overall discoloration than Na₂SO₄ under the same experimental conditions. These results could be due to halide electrolytes generating active halide species, which has been suggested in other studies [38]. In their report, Ambauen et al. [38] found that once hydroxyl radicals are formed, secondary reactions may occur when electrochemically active electrolytes are present, including the scavenging of the reactive oxygen species and the secondary production of other less reactive species that are capable of reacting with the organic pollutants under some conditions, resulting in partial chemical oxidation. However, based on the mechanisms for active chloride-mediated electrochemical oxidation, this type of side reaction is not favored because, in most cases, chlorinated byproducts possess a higher toxicity.

On the other hand, using Na₂SO₄ in the EOx-based discoloration of dye water has interesting potential. Previously, we used a BDD anode to remove different industrial sulfonated dye products from water [39]. In that study, we found BBR discoloration ranging from 25% to 95%, which was possibly related to the production of a low and steady concentration of oxygen radical on the BDD surface attacking the dye molecules. The best results were achieved using the highest current density value tested (e.g., 18 mA cm⁻²), a pH of 3, a 0.5 L laboratory stirred tank reactor, and a 25 cm² BDD electrode. In this study, we achieved up to 82% of BBR discoloration for the same reaction time reported previously, but using a BDD electrode area one order of magnitude lower (e.g., 2.5 cm²).

From this study, pseudo-first-order kinetics were calculated as described above. In the case of HClO₄ medium, the following results were obtained: (\blacktriangle) 0.0038, (\bigstar) 0.0045, (\bigstar) 0.0086 min⁻¹, respectively. For the Na₂SO₄ supporting electrolyte, the following values were obtained: (\blacklozenge) 0.0043, (\bigstar) 0.0161, (\blacklozenge) 0.0293 min⁻¹, respectively. For all the experimental fittings using the pseudo-first order kinetics model, the minimum R² value obtained was 0.99, suggesting that this kinetics model describes the chemical process fairly good. As shown, the *k*-values found for Na₂SO₄ were about 3.5 times higher than those observed when HClO₄ was used as the supporting electrolyte.

3.2.2. BBR Dye Degradation at Different Current Densities in 0.1 M HClO₄ and FeSO₄

Figure 6a shows water discoloration as a function of FeSO₄ concentration using a current density of 7 mA cm⁻². Slow discoloration was observed for the EOx process alone (\blacklozenge), and 31% BBR degradation and *k*-value 0.0030 min⁻¹ were achieved. By adding 1 mM of FeSO₄ to the system (\blacktriangle), a 38% discoloration and *k*-value 0.0035 min⁻¹ were achieved. Further increasing the FeSO₄ concentration (e.g., 6 mM (\blacksquare), and 12 mM (\bullet)) led to water discoloration values of 41% and 46%, respectively, and reaction rate constant values of 0.0038 min⁻¹ and 0.0042 min⁻¹, respectively, were obtained after two hours of treatment [40,41].



Figure 6. Removal of an aqueous solution of BBR azo dye, $C_0 = 50 \text{ mg/L}$, during the oxidation process in 0.1 M of HClO₄ with a solution volume of 0.1 L, (a) $j = 7 \text{ mA cm}^{-2}$, (b) $j = 15 \text{ mA cm}^{-2}$, (c) $j = 30 \text{ mA cm}^{-2}$, and fit to first order reaction kinetics (d), (e) y (f), respectively; (\blacklozenge) BDD without FeSO₄, (\blacktriangle) 1 mM of FeSO₄, (\blacksquare) 6 mM of FeSO₄, and (\bullet) 12 mM of FeSO₄.

When current density was increased to 15 mA cm⁻² (Figure 6b), an improvement in discoloration tendency was observed, and the increase in FeSO₄ concentration produced a higher removal speed and discoloration percentage. For the EOx process alone (\blacklozenge), a 46% discoloration and k_1 -value of 0.0046 min⁻¹ were observed. When 1 mM of FeSO₄ (\blacktriangle) was used, a 50% discoloration and k_1 -value of 0.0053 min⁻¹ were achieved. Using 6 mM of FeSO₄ (\blacksquare) produced a 54% discoloration and k_1 -value of 0.0060 min⁻¹. Finally, the process with the greatest discoloration used 12 mM of FeSO₄ (\bullet), generating a 63% discoloration after two hours of treatment and a k_1 -value of 0.0076 min⁻¹.

Further increasing the current density to 30 mA cm⁻² showed the best results, as shown in Figure 6c. Compared with the other conditions tested, the highest discoloration was achieved by

adding 12 mM of FeSO₄ (•) into the solution, followed by adding 6 mM of FeSO₄ (**■**), 1 mM of FeSO₄ (**▲**), and finally using the EOx process alone (•), which produced water discoloration values as high as 93%, 85%, 77%, and 67%, respectively, and k_1 -values of 0.0191 min⁻¹, 0.0141 min⁻¹, 0.0112 min⁻¹, and 0.0087 min⁻¹, respectively.

3.2.3. BBR Dye Degradation at Different Current Densities in 0.05 M of Na₂SO₄ and FeSO₄

Figure 7a shows the degradation of BBR dye (50 mg L⁻¹) using 0.05 M Na₂SO₄ at pH 3 as the support electrolyte after 60 min. It is worth noting that continuous dye degradation was observed for the four different conditions tested: EOx alone and adding 1 mM, 6 mM, and 12 mM of FeSO₄ while operating at a constant current density (7 mA cm⁻²). The EOx process alone (\blacklozenge) showed 36% discoloration ($k_1 = 0.0036 \text{ min}^{-1}$). When 1 mM of FeSO₄ (\blacktriangle) was added, 91% discoloration was achieved ($k_1 = 0.0052 \text{ min}^{-1}$).



Figure 7. Removal of an aqueous solution of BBR azo dye, $C_0 = 50 \text{ mg/L}$, during the oxidation process in 0.05 M of Na₂SO₄ and at a pH of 3 with a solution volume of 0.1 L, (**a**) $j = 7 \text{ mA cm}^{-2}$, (**b**) $j = 15 \text{ mA cm}^{-2}$, (**c**) $j = 30 \text{ mA cm}^{-2}$, and fit to first order reaction kinetics (**d**), (**e**) y (**f**), respectively; (**♦**) BDD without FeSO₄, (**a**) 1 mM of FeSO₄, (**b**) 6 mM of FeSO₄, and (**•**) 12 mM of FeSO₄.

Water discoloration as high as 94% was observed when 6 mM of FeSO₄ was added (**■**) ($k_1 = 0.0120 \text{ min}^{-1}$), and finally the faster discoloration (e.g., 96%, $k_1 = 0.0258 \text{ min}^{-1}$) was achieved after 60 min of treatment using 12 mM of FeSO₄ (•).

Increasing the current density to 15 mA cm⁻² (Figure 7b) generated better results for BBR dye discoloration for shorter process times. When EOx was used alone (\blacklozenge), 63% ($k_1 = 0.0166 \text{ min}^{-1}$) was

observed. When 1 mM of FeSO₄ (\blacktriangle) was added, 80% dye removal ($k_1 = 0.0297 \text{ min}^{-1}$) was achieved after 60 min. By increasing FeSO₄ to 6 mM (\blacksquare), 89% ($k_1 = 0.0404 \text{ min}^{-1}$) was reached and, when using 12 mM of FeSO₄ (\bullet), 96% ($k_1 = 0.0645 \text{ min}^{-1}$) was reached after 60 min.

The same tendency was observed when the highest current density (30 mA cm⁻²) was applied, as shown in Figure 7c. In this case, using 12 mM of FeSO₄ (•) generated 98% discoloration ($k_1 = 0.0703 \text{ min}^{-1}$), and using 6 mM of FeSO₄ (•) generated 95% discoloration ($k_1 = 0.0528 \text{ min}^{-1}$). Using 1 mM of FeSO₄ (•), 87% discoloration ($k_1 = 0.0347 \text{ min}^{-1}$) was achieved, and finally EOx alone (•) only reached 78% discoloration ($k_1 = 0.0257 \text{ min}^{-1}$) after 60 min.

Based on these results, a combined BBR oxidation process is proposed. For the first case where we used FeSO₄ and HClO₄ as an electrolyte, the oxidation process would occur directly on the BDD electrode (EOx) and indirectly (chemically) through the hydroxyl radicals (resulting from water oxidation) and ferrate ions (resulting from FeSO₄ oxidation), as in Scheme 1, reactions 4, 5 and 8. For the second case, where FeSO₄ and Na₂SO₄ were used as electrolyte, the BBR oxidation process occurs directly on the BDD electrode (EOx, reaction 5) and indirectly (chemically) through the hydroxyl radicals (resulting from water oxidation, reactions 3 and 4), ferrate (VI) ions (resulting from FeSO₄ oxidation, reactions 7 and 8) and perosodisulfates (resulting from the oxidation of Na₂SO₄, reactions 9 and 10), as in the Scheme 2 [42]. The formation of peroxodisulfate causes the latter case to be more effective in the oxidation of the BBR.

Based on the above, the simultaneous processes of EOx and the generation of ferrate ions in situ can be summarized with the following reactions [21]:

1. Discharge of water into the system and generation of oxygen radicals (•OH).

$$BDD + H_2O \rightarrow BDD(^{\bullet}OH) + H^+ + e^-$$
(3)

2. Oxidation of contaminants by oxygen radicals (•OH).

$$BDD(^{\bullet}OH) + R \rightarrow BDD + nCO_2 + mH_2O$$
(4)

3. Oxidation of contaminants on BDD.

$$BDDpolarized(+) + R \rightarrow BDD(nCO_2) + mH_2O$$
(5)

4. Generation of [Fe(VI)] from FeSO₄ on BDD.

oxidation :
$$Fe^{2+} + OH \rightleftharpoons Fe^{3+} + OH^{-}$$
 (6)

over – oxidation :
$$\operatorname{Fe}^{3+} + 4\operatorname{H}_2\operatorname{O} \rightleftharpoons \operatorname{FeO}_4^{2-} + 8\operatorname{H}^+ + 3e^-$$
 (7)

5. Oxidation of organic compounds by [Fe(VI)] and $S_2O_8^{2-}$:

$$[Fe(VI)] + R \rightarrow Fe(III) + IS + nCO_2 + mH_2O$$
(8)

$$2SO_4^{2-} \to S_2O_8^{2-} + 2e^- \tag{9}$$

$$S_2O_8^{2-} + R \rightarrow 2SO_4^{2-} + IS + nCO_2 + mH_2O$$
 (10)

For this study, stages (e) and (f) were avoided by working at low $FeSO_4$ concentrations, which promoted a synergistic effect in stages (b) and (d).



Scheme 1. Representation of the reactions involved on BDD substrate electrode held in FeSO₄ and 0.1 M of HClO₄.



Scheme 2. Representation of the reactions involved on BDD substrate electrode held in FeSO₄ and 0.05 M Na₂SO₄.

3.2.4. COD Determinations and Byproduct Evolution

In Figure 8, COD reduction is shown by comparing EOx alone (\blacklozenge) with the in situ generation of [Fe(VI)] (\bullet). Electro-oxidation alone was able to achieve 37% COD removal after 90 min of treatment. In the case of ferrate generation, 61% COD removal was obtained, suggesting electrogenerated [Fe(VI)] ions directly influence a decrease in COD by carrying out pollutant degradation more efficiently and reducing the amount of oxidable matter in the solution [43,44].

Figure 8a shows the accumulation of a low amount of carboxylic acids generated during the EOx process alone (\blacklozenge) and while testing the simultaneous EOx/[Fe(VI)] processes using 12 mM of Fe₂O₄ (\bullet) at 30 mA cm⁻². The carboxylic acid quantified from BBR degradation was oxalic acid. Figure 8b shows that oxalic acid generation contributed only almost 20 mg/L using the EOx process alone, whereas adding 12 mM of FeSO₄ produced only 2 mg L⁻¹ under the simultaneous EOx/[Fe(VI)] process. These results suggest that the degradative pathway of BBR produces carboxylic acid because of the combined action of 'OH and ferrate ions generated in the solution [45–49].



Figure 8. (a) Variation of COD abatement for 50 mg/L of BBR azo dye using BDD electrolysis without FeSO₄ (\blacklozenge) and the simultaneous EOx/[Fe(VI)] process using 12 mM of FeSO₄ (\blacklozenge) in 0.05 M of Na₂SO₄ at a pH of 3 at 30 mA cm⁻². (b) Evolution of the concentration of oxalic acid produced during the degradation of 0.4 L of 50 mg/L BBR solution in 0.05 M of Na₂SO₄ at a pH of 3 and 35 °C using BDD without FeSO₄ (\blacklozenge) and the simultaneous EOx/[Fe(VI)] process using 12 mM of FeSO₄ (\blacklozenge) at 30 mA cm⁻².

4. Conclusions

Electrochemical characterization using cyclic voltammetry confirms the in situ electrogeneration of ferrate ions on the BDD surface by adding FeSO₄ in both the sulfate and perchloric acid media. The use of HClO₄ produced discoloration efficiency close to 93% after 120 min of treatment when 12 mM of FeSO₄ was added. However, faster degradation rates were observed using the sulfate medium, which achieved up to 98% of color reduction in 60 min of treatment when 12 mM of FeSO₄ was added and a current density of 30 mA cm⁻² was applied. A COD abatement as high as 63% was observed when the highest FeSO₄ concentration was added to the reaction mixture using the highest current density value. The byproduct analysis detected the presence of only one carboxylic acid (oxalic acid), which was rapidly oxidized by the simultaneous EOx/[Fe(VI)] process. These were identified as the best treatment conditions because they allowed some smaller amount reaction byproducts to accumulate.

Based on the obtained results, it was possible to demonstrate the viability of the simultaneous generation of both oxidant species, the free radical and the ferrate ion, which opens up an important opportunity to carry out not only the degradation of dyes, but also other organic compounds that are difficult to remove. This work provides an advance in the study of the simultaneous generation of oxidant species to the scientific community interested in this subject. In the future, the challenge will be understanding the reaction mechanisms.

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