# Effect of Physical and Mechanical Activation on the Physicochemical Structure of Coal-Based Activated Carbons for SO2 Adsorption

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#### Abstract:

The SO2 adsorption efficiency of activated carbons (ACs) is clearly dependent on its physicochemical structure. Related to this, the effect of physical and mechanical activation on the physicochemical structure of coal-based ACs has been investigated in this work. In the stage of CO2 activation, the rapid decrease of the defective structure and the growth of aromatic layers accompanied by the dehydrogenation of aromatic rings result in the ordered conversion of the microstructure and severe carbon losses on the surfaces of Char-PA, while the oxygen content of Char-PA, including C=O (39.6%), C?O (27.3%), O?C=O (18.4%) and chemisorbed O (or H2O) (14.7%), is increased to 4.03%. Char-PA presents a relatively low SBET value (414.78 m2/g) owing to the high value of Non-Vmic (58.33%). In the subsequent mechanical activation from 12 to 48 h under N2 and dry ice, the strong mechanical collision caused by ball-milling can destroy the closely arranged crystalline layers and the collapse of mesopores and macropores, resulting in the disordered conversion of the microstructure and the formation of a defective structure, and a sustained increase in the SBET value from 715.89 to 1259.74 m2/g can be found with the prolonging of the ball-milling time. There is a gradual increase in the oxygen content from 6.79 to 9.48% for Char-PA-CO2-12/48 obtained by ball-milling under CO2. Remarkably, the varieties of physicochemical parameters of Char-PA-CO2-12/48 are more obvious than those of Char-PA-N2-12/48 under the same ball-milling time, which is related to the stronger solid-gas reactions caused by the mechanical collision under dry ice. Finally, the results of the SO2 adsorption test of typical samples indicate that Char-PA-CO2-48 with a desirable physicochemical structure can maintain 100% efficiency within 30 min and that its SO2 adsorption capacity can reach 138.5 mg/g at the end of the experiment. After the 10th cycle of thermal regeneration, Char-PA-CO2-48 still has a strong adsorptive capacity (81.2 mg/g).

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Article

# Effect of Physical and Mechanical Activation on the Physicochemical Structure of Coal-Based Activated Carbons for SO<sub>2</sub> Adsorption

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Abstract: The SO<sub>2</sub> adsorption efficiency of activated carbons (ACs) is clearly dependent on its physicochemical structure. Related to this, the effect of physical and mechanical activation on the physicochemical structure of coal-based ACs has been investigated in this work. In the stage of  $CO_2$ activation, the rapid decrease of the defective structure and the growth of aromatic layers accompanied by the dehydrogenation of aromatic rings result in the ordered conversion of the microstructure and severe carbon losses on the surfaces of Char-PA, while the oxygen content of Char-PA, including C=O (39.6%), C–O (27.3%), O–C=O (18.4%) and chemisorbed O (or H<sub>2</sub>O) (14.7%), is increased to 4.03%. Char-PA presents a relatively low  $S_{BET}$  value (414.78 m<sup>2</sup>/g) owing to the high value of Non- $V_{mic}$ (58.33%). In the subsequent mechanical activation from 12 to 48 h under  $N_2$  and dry ice, the strong mechanical collision caused by ball-milling can destroy the closely arranged crystalline layers and the collapse of mesopores and macropores, resulting in the disordered conversion of the microstructure and the formation of a defective structure, and a sustained increase in the S<sub>BET</sub> value from 715.89 to 1259.74 m<sup>2</sup>/g can be found with the prolonging of the ball-milling time. There is a gradual increase in the oxygen content from 6.79 to 9.48% for Char-PA-CO<sub>2</sub>-12/48 obtained by ball-milling under CO<sub>2</sub>. Remarkably, the varieties of physicochemical parameters of Char-PA-CO<sub>2</sub>-12/48 are more obvious than those of Char-PA-N<sub>2</sub>-12/48 under the same ball-milling time, which is related to the stronger solid-gas reactions caused by the mechanical collision under dry ice. Finally, the results of the  $SO_2$ adsorption test of typical samples indicate that Char-PA-CO<sub>2</sub>-48 with a desirable physicochemical structure can maintain 100% efficiency within 30 min and that its SO<sub>2</sub> adsorption capacity can reach 138.5 mg/g at the end of the experiment. After the 10th cycle of thermal regeneration, Char-PA-CO<sub>2</sub>-48 still has a strong adsorptive capacity (81.2 mg/g).

**Keywords:** activated carbons; physical activation; mechanical activation; physicochemical structure; SO<sub>2</sub> adsorption

# 1. Introduction

For a long time, SO<sub>2</sub> emission from large coal-fired power plants has seriously polluted the environment and threatened human health [1]. The traditional wet desulfurization technology using calcium-based absorbent is unable to satisfy sustainable development, owing to its ecological destruction and the production of massive low-value by-products [2]. Dry desulfurization technology using porous carbon materials (such as activated carbons, ACs) as adsorbents has a better application



prospect owing to its low price and ability to produce valuable by-products (such as sulfuric acid) [3]. ACs are usually prepared via a physical activation method and chemical activation method. In the process of chemical activation, the substantial water/acid is consumed to remove a large number of residual reagents (such as KOH [4,5], K<sub>2</sub>CO<sub>3</sub> [6,7], ZnCl<sub>2</sub> [8], and H<sub>3</sub>PO<sub>4</sub> [9]), which not only increases the preparation costs but also causes environmental pollution. Thus, it is highly desirable to apply physical activation as a green and low-cost method for the preparation of ACs. In the process of physical activation, activation agents including steam,  $CO_2$  and their mixtures can partially etch the carbon network to produce some porosity and functional groups, and some researchers [10–14] have found that CO<sub>2</sub> activation can make it easier to generate pores inside the particles than steam activation can. In addition, the preparation of ACs using coal as raw material can also meet desulfurization requirements in coal-fired power plants. Furthermore, the desulfurization performance of ACs is closely related to its physicochemical structure, such as a lot of active sites and a high specific surface area ( $S_{BET}$ ) in the presence of the hierarchical pore [15,16]. In the process of physical activation, the pore development follows a branched model. First, the micropore is formed on the surface of particles at the initial stage, after which the successive diffusion of activated agents from surface to core helps the formation of a new micropore; meanwhile, the formation of mesopores and macropores originates from the enlargement of the original micropores [17,18]; this branched model inevitably leads to a low specific surface area (S<sub>BET</sub>) and a high carbon loss on the surface of the particles, even under various activation conditions (such as the activation temperature, activation time and activated gas species, etc.) [13,14,19,20]. In addition, the active sites of porous carbon materials usually include oxygen/nitrogen-containing functional groups and defects at the edge of the aromatic layers. Zhu et al. [13,14] have found that the surface chemical properties of ACs are also significantly changed to form some oxygen-containing functional groups with the carbon loss at the stage of  $CO_2$  activation. Some researchers and our previous work [21–23] have found that the dehydrogenation of aromatic rings accompanied by the rapid decrease of the defect structure helps the vertical condensation and the transverse growth of aromatic layers during the physical activation, thus resulting in the removal of a large number of active sites. In summary, it is difficult to obtain the ideal ACs with a desirable porosity and more active sites in the stage of physical activation.

A ball-milling technique is a novel method to synthesize materials by mechanical activation without producing hazardous products (which can destroy the chemical bonds of the macromolecular structure), finally resulting in the molecular rearrangement, amorphization and recrystallization of the crystal structure [24,25]. Ong et al. [26] have found that the specific surface area (S<sub>BET</sub>) and the oxygen content of the sample increase rapidly from 6 m<sup>2</sup>/g to 450 m<sup>2</sup>/g and from 3.6% to 5.0% within 12 h of milling in the oxidizing atmosphere. Zhang et al. [27] also found that the size distribution of the sample ends up being narrower and its average particle size decreases with the increase of the milling time from 0.25 to 8 h because of the high collision strength between the agate balls during the ball-milling process. Salver-Disma et al. [28] have demonstrated that the mechanical milling of natural graphite is one possibility for producing disordered carbons with large intercalation capacities. The milled graphite contains large amounts of defects and present anisotropies [29]. Nevertheless, information regarding the changes in the physicochemical structure of coal-based ACs during physical and mechanical activation is still limited.

In this work, a precursor with a stable carbon-based framework obtained by pyrolysis could be treated first by  $CO_2$  activation, which ensures the formation of the original pores (such as some micropores and the hierarchical pores) and some oxygen-containing functional groups. In order to further increase the specific surface area and quantities of the active sites, the samples mentioned above continued to be activated via the ball-milling method under different times (12 h and 48 h, respectively) and different atmospheres (dry ice or  $N_2$ ) to further increase the specific surface area and quantities of the active sites. In addition, the physicochemical structure of all the samples were measured by a D/max-rb X-ray diffractometer (XRD), Raman spectroscopy, Nitrogen adsorption, X-ray photoelectron spectroscopy (XPS), transmission electron microscope (TEM) and high-resolution scanning electron microscope (SEM). Finally, to verify the application potentials of the ACs with the ideal physicochemical structure, an SO<sub>2</sub> removal test was performed to further explore the relationship between the physicochemical structure and SO<sub>2</sub> adsorption of ACs.

#### 2. Materials and Methods

# 2.1. Materials

In this work, Jixi bituminous coal with particle sizes of 200–350  $\mu$ m was obtained from the northeast of China. In order to eliminate the interference of minerals in the raw material, Jixi bituminous coal was treated sequentially using 30 wt % hydrofluoric acid (HF) and 5 mol·L<sup>-1</sup> hydrochloric acid (HCl) following the steps in the literature [30]. Then, the acid-treated samples were washed using deionized water and dried in an oven at 90 °C for 12 h. The proximate analysis and elemental analysis of the acid-treated samples (JX) were given in Table 1.

Table 1. The proximate analyses and elemental analyses of JX (wt %).

Vad	FC <sub>ad</sub>	$A_{\rm ad}$	$M_{\rm ad}$	C <sub>daf</sub>	$H_{daf}$	O <sub>daf</sub> *	N <sub>daf</sub>	S <sub>daf</sub>
39.66	56.60	0.12	3.62	74.81	19.49	4.01	1.31	0.38

\* By difference; ad (air-dried basis): the coal in dry air was used as a benchmark; daf (dry ash free basis): the remaining component after the removal of water and ash in coal was used as a benchmark; *V*: volatile; *FC*: fixed carbon; *A*: ash; *M*: moisture; *C*: carbon element; *H*: hydrogen element; *O*: oxygen element; *N*: nitrogen element; *S*: sulfur element.

#### 2.2. Experimental Process

#### 2.2.1. CO<sub>2</sub> activation

10 g of JX were heated to 900 °C at a constant rate of 5 °C/min in an argon atmosphere flow of 600 mL/min and held for 60 min, and this sample was marked as Char. Then, argon atmosphere was converted to  $CO_2$  (99.999%) at 600 mL/min and held for 60 min, before being finally cooled down to room temperature under an argon atmosphere and being marked as Char-PA.

#### 2.2.2. Mechanical activation

Char-PA was prepared by a planetary ball mill (Pulverisette 6, FRITSCH, Idar-Oberstein, Germany,) by applying a rotation speed of 400 rpm in dry ice or N<sub>2</sub> atmosphere for 12 h and 48 h, respectively. Additionally, a ball-to-powder weight ratio of 15:1 and 12 stainless steel balls with a diameter of 10 mm were used in the process of ball-milling, and these treated samples were marked as Char-PA-N<sub>2</sub>/CO<sub>2</sub>-different activation times. In addition, thermal annealing of a typical sample was processed at 800 °C for 60 min in 5% H<sub>2</sub>/Ar atmosphere; this treated sample was marked as Char-PA-N<sub>2</sub>/CO<sub>2</sub>-different activation times-H<sub>2</sub>.

# 2.3. Measurement Analysis

The surface topography of the samples was obtained via a scanning electron microscope (SEM, Quanta 200, FEI, Oregon, OR, USA) at 200 kV. The microstructure of the samples was tested by high-resolution transmission electron microscope (HRTEM, Tecnai G2 F30, FEI, Oregon, OR, USA) at 300 kV. The crystal information of the samples was received by a D/max-rb X-ray diffractometer (XRD, D8 ADVANCE, Brooke, Karlsruhe, Germany) at a fixed scanning speed of 3°/min from 5° to 85°. The hybrid carbon information of the samples was received by Raman spectroscopy at a stable scanning scope from 1000–1800 cm<sup>-1</sup> using a 532 nm wavelength laser. The elemental composition, chemical state and relative concentration on the surface of the samples were obtained by X-ray photoelectron spectroscopy (XPS, K-Alpha, Thermo Fisher Scientific, Waltham, MA, USA) with an Al K $\alpha$  X-ray at 14 kV and 6 mA [31]. The pore parameters of the samples were received by a micromeritics adsorption

apparatus (ASAP2020, Micromeritics, Norcross, GA, USA) at 77 K and a relative pressure (P/P<sub>0</sub>) range from  $10^{-7}$  to 1 [32]. The vacuum degassing pretreatment of the tested samples was carried out at 473 K for 12 h. Moreover, the specific surface area (S<sub>BET</sub>) of the samples was calculated using a BET model in a relative pressure range of 0.05–0.2 [33]; the total pore volume (V<sub>tot</sub>) caused by the adsorption value of liquid nitrogen at a relative pressure of 0.98 was obtained using the *t*-plot method [34]; the micropore volume (V<sub>mic</sub>) of the samples was calculated using the Horvath–Kawazoe (HK) method [35]; the nonlocal density functional theory (NLDFT) was used to obtain the pore size distribution of the micropore and mesopore, and the relative pressure range was  $10^{-7}$ ~0.9 [13].

#### 2.4. SO<sub>2</sub> Adsorption Test

A fixed-bed experimental system was used to investigate the SO<sub>2</sub> adsorption performance of ACs. This system included four parts: the gas distribution system, the fixed-bed reactor, the heating and insulation system, and the gas analysis system, as shown in Figure 1. First, 250 mL of deionized water were added to the humidifying tank, which was placed in a constant temperature water bath to maintain it at 90 °C. Simulated flue gas was prepared by mixing a certain amount of N<sub>2</sub> with SO<sub>2</sub>, O<sub>2</sub> and other gases. The water vapor content in the simulated flue gas was controlled by adjusting the N<sub>2</sub> flow rate.



Figure 1. Schematic figure of the fixed-bed reactor system for SO<sub>2</sub> adsorption.

The experimental process is as follows: 5 g of tested sample were placed in a glass tube reactor that consisted of a glass tube and sand core. Furthermore, this sand core not only supported AC particles, but also played the role of current sharing. The filling height and diameter of the adsorbent in the glass tube reactor were 25 mm and 20 mm, respectively. The SO<sub>2</sub> adsorption test was performed at 80 °C for 210 min. The gas volumetric composition used in the experiments was: SO<sub>2</sub>, 1500 ppm; O<sub>2</sub>, 5%; water vapor, 10%; and N<sub>2</sub>, balance, total flow rate 250 mL·min<sup>-1</sup>. The SO<sub>2</sub> concentrations at the entrance and exit were measured by an on-line Fourier transform infrared gas analyzer (FTIR, Dx4000, Gasmet, Vantaa, Finland) for calculating the SO<sub>2</sub> removal efficiency and the change of the removal rate with time. According to the integral area and reaction time on the removal curve, the SO<sub>2</sub> removal capacity of the coal-based ACs was obtained [36]. In addition, the SO<sub>2</sub> removal efficiency, SO<sub>2</sub> removal rate and cumulative sulphur capacity were calculated with the following formula:

 $SO_2$  removal efficiency (*DeSO*<sub>2</sub>):

$$DeSO_{2}(\%) = \frac{SO_{2}(in) - SO_{2}(out)}{SO_{2}(in)} \times 100\%$$
(1)

In the formula,  $SO_2$  (*in*) and  $SO_2$  (*out*) are the  $SO_2$  concentrations at the reactor inlet and outlet measured by FTIR, respectively.

 $SO_2$  removal rate ( $RSO_2$ ):

$$RSO_2(\text{mg} \cdot \text{g}^{-1} \cdot \text{min}^{-1}) = \frac{DeSO_2 \cdot SO_2(in) \cdot 0.3 \cdot 64}{22400}$$
(2)

In the formula,  $DeSO_2$  is the SO<sub>2</sub> removal efficiency and  $SO_2$  (*in*) is the SO<sub>2</sub> concentration at the reactor inlet measured by FTIR,

The accumulated sulfur capacity  $(ASO_2)$  refers to the cumulative removal capacity of SO<sub>2</sub> from samples varying with time and is obtained by integrating the removal rate of SO<sub>2</sub> with the time.

$$ASO_2(\mathrm{mg} \cdot \mathrm{g}^{-1}) = \int_0^t RSO_2 dt \tag{3}$$

#### 2.5. Thermal Regeneration

For the thermal regeneration, desulfurized ACs were placed in a glass tube, and afterwards were settled in a vertical furnace (Figure 1). The ACs were heated in a flow of nitrogen (200 mL/min), at a heating rate of  $10 \,^{\circ}$ C min<sup>-1</sup> and maintained at 400  $^{\circ}$ C for 30 min, before being cooled for 30 min while the nitrogen purge was continued.

#### 3. Results and Discussion

#### 3.1. Microstructure and Surface Morphology Analysis by HRTEM and SEM

Figure 2 shows several HRTEM and SEM images of samples produced under pyrolysis and different activation conditions, including (a) HRTEM and (h) SEM of Char; (b) HRTEM and (i) SEM of Char-PA; (c) HRTEM and (j) SEM of Char-PA-N2-12; (d) HRTEM and (k) SEM of Char-PA-N2-48; (e) HRTEM and (l) SEM of Char-PA-CO<sub>2</sub>-12; (f) HRTEM and (m) SEM of Char-PA-CO<sub>2</sub>-48; (g) HRTEM and (n) SEM of Char-PA-CO<sub>2</sub>-48H<sub>2</sub>. There are some crystalline layers with different orientations near small quantities of amorphous carbon for Char in Figure 2a. In addition, a smooth surface and compact texture of Char can be found in Figure 2h. He et al. [37] found that metaplast material that was formed via the combination of transferable hydrogen and aliphatic hydrocarbons during pyrolysis can not only promote the ordered arrangement of aromatic layers but also reshape the particle surface. After CO<sub>2</sub> activation, a large amount of long and multi-layer crystallite with a consistent orientation can be found in Char-PA, as shown in Figure 2b; the highly ordered crystalline layers of Char-PA can hinder the further diffusion of activated gas into the interior of particles, leading to severe carbon losses on the particle surfaces, as shown in Figure 2i. After 12 h of high-energy ball milling, some short and thin crystallite layers of Char-PA-N<sub>2</sub>/CO<sub>2</sub>-12 with a granular structure and rough surface can be found in Figure 2c,e,j,l. Furthermore, as the time of ball milling increases from 12 h to 48 h, blurred boundaries and a disordered arrangement of crystalline layers of Char-PA-N<sub>2</sub>/CO<sub>2</sub>-48 with a rougher surface and some smaller particles are also found in Figure  $2d_{,f_{k}}$ . The above results show that the mechanical collision caused by ball milling can significantly promote the disordered conversion of the microstructure and improve the surface morphology of particles with the increase of the ball-milling times from 12 to 48 h. In the process of mechanical activation, the high-energy ball milling can reduce the reaction temperature of the solid state and cause the increase of the local temperature on the material [24,25]. Based on this fact, a strong mechanical collision under dry ice can rapidly promote the solid-gas reactions between  $CO_2$  and the carbon matrix, as a result of which Char-PA- $CO_2$ -12/48 shows more obvious changes in its microcrystalline structure and surface morphology than Char-PA-N<sub>2</sub>-12/48 under the same ball-milling time.



**Figure 2.** The HRTEM and SEM images of the samples produced at different treatment conditions. (a) HRTEM and (h) SEM of Char; (b) HRTEM and (i) SEM of Char-PA; (c) HRTEM and (j) SEM of Char-PA-N<sub>2</sub>-12; (d) HRTEM and (k) SEM of Char-PA-N<sub>2</sub>-48; (e) HRTEM and (l) SEM of Char-PA-CO<sub>2</sub>-12; (f) HRTEM and (m) SEM of Char-PA-CO<sub>2</sub>-48; (g) HRTEM and (n) SEM of Char-PA-CO<sub>2</sub>-48H<sub>2</sub>.

# 3.2. Crystal Structure Analysis by XRD

The XRD profiles of the samples produced under pyrolysis and different activation conditions are given in Figure 3. There are two obvious broad diffraction peaks at  $2\theta = 16-32^{\circ}$  and  $36-52^{\circ}$  in all of the samples; the information on two diffraction peaks (such as positions and half-peak width) can be obtained using the peak fitting treatment, as shown in Figure 4. Some crystal parameters, including the interlayer distance ( $d_{002}$ ), stacking height ( $L_c$ ), and the size ( $L_a$ ) and numbers (N) of the aromatic layers, are calculated via the following formulas [38]:

$$d_{002} = \frac{\lambda}{2\sin\theta} \tag{4}$$

$$L_c = \frac{0.89\lambda}{\beta\cos\theta} \tag{5}$$

$$L_a = \frac{1.84\lambda}{\beta\cos\theta} \tag{6}$$

$$N = \frac{L_c}{d_{002}} \tag{7}$$



Figure 3. The XRD profiles from the samples produced at different treatment conditions.



Figure 4. The fitting curve of the peaks for Char-PA in the 2θ range (a) 15–32° and (b) 35–53°.

In the above formulas,  $\lambda$ : the wavelength of the X-ray,  $\lambda = 1.54$  Å;  $\theta$ : peaks' positions (°); and  $\beta$ : half peak width. The results of the crystal parameters of all the samples are given in Table 2.

Samples	La (Å)	Lc (Å)	d <sub>002</sub> (Å)	$N = Lc/d_{002}$
Char	24.81	13.48	3.50	3.85
Char-PA	25.73	13.79	3.45	3.99
Char-PA-N <sub>2</sub> -12	24.31	13.15	3.58	3.67
Char-PA-N <sub>2</sub> -48	23.19	12.43	3.72	3.34
Char-PA-CO <sub>2</sub> -12	23.91	12.86	3.69	3.48
Char-PA-CO <sub>2</sub> -48	22.28	11.79	3.96	2.98
Char-PA-CO <sub>2</sub> -48H <sub>2</sub>	22.75	12.97	4.05	3.20

Table 2. The crystal parameters of the samples produced at different treatment conditions.

First, the rapid increase in the numbers (*N*), stacking height ( $L_c$ ) and size ( $L_a$ ) of the aromatic layers and the obvious reduction in the layer spacing ( $d_{002}$ ) can be found in the Char-PA during CO<sub>2</sub> activation. The longitudinal condensation and transversal growth of the aromatic layers are related to the rapid consumption of the side chains and bridge bonds within the aromatic layers and defective structure on the edge of the aromatic layers [14,39]. Then, with the ball-milling time increases from 12 to 48 h, there is a sustained decrease in the  $L_a$ ,  $L_c$  and N values and a persistent increase in the  $d_{002}$ value for Char-PA-CO<sub>2</sub>/N<sub>2</sub>-12/48, indicating the disordered conversion of the microcrystalline structure. These changes are closely related to the breakdown and distortion of the aromatic layers caused by a strong mechanical collision, which can further destroy the parallelism of the layer and the constancy of the interlayer spacing. Finally, the changes of the crystal parameters of Char-PA-CO<sub>2</sub>-12/48 are more obvious than those of Char-PA-N<sub>2</sub>-12/48 under the same ball-milling time, which may be related to the fact that the local high temperature caused by ball milling promotes CO<sub>2</sub> etching on the aromatic layers. In this process, the more defective structures on the edge of the aromatic layers can also be formed as active sites.

#### 3.3. Carbon Structure Analysis by Raman

The Raman spectra of the samples produced under pyrolysis and different activation conditions are shown in Figure 5. There are two obvious broad diffraction peaks at 1230–1450 cm<sup>-1</sup> (D peak) and 1450–1580 cm<sup>-1</sup> (G peak) in all of the samples. Some researchers [40,41] have found that the widening of the D and G peaks is serious for incomplete graphitized materials in Raman spectra, indicating the existence of many sp<sup>2</sup>-hybridized structures and sp<sup>2</sup>–sp<sup>3</sup> hybridized structures. Thus, it is necessary to resolve overlapped peaks using a fitting treatment, including for the D<sub>1</sub> peak (1300 cm<sup>-1</sup>), D<sub>3</sub> peak (1520 cm<sup>-1</sup>), D<sub>4</sub> peak (1200 cm<sup>-1</sup>) and G peak (1550 cm<sup>-1</sup>). Figure 6 shows the fitting curve of the Raman spectrum for Char-PA-N<sub>2</sub>-48. Furthermore, the D<sub>1</sub> peak is represented as the defective sp<sup>2</sup> bonding carbon atoms; the D<sub>3</sub> peak is represented as the amorphous sp<sup>2</sup> bonding carbon atoms; the  $D_4$  peak is represented as the sp<sup>2</sup>–sp<sup>3</sup> bonding carbon atoms; the G peak is represented as the crystalline sp<sup>2</sup> bonding carbon atoms; furthermore, the relative quantities of different hybridized structures is as follows: (1)  $A_{D1}/A_G$  represents the relative quantity of the big aromatic rings, including C–C between aromatic rings and aromatics with no fewer than 6 rings with a defective structure; (2)  $A_{D3}/A_G$  represents the relative quantity of the small aromatic rings including aromatics with 3–5 rings and the semi-circle breathing of aromatic rings; and (3)  $A_{D4}/A_G$  represents the relative quantity of the cross-linking structure, including  $C_{aromatic}$ – $C_{alkyl}$ , aromatic (aliphatic) ethers and C–C on hydroaromatic rings [42]. The results of the different hybrid carbons in the form of area ratios of the samples are shown in Table 3.



Figure 5. The Raman spectra from the samples produced at different treatment conditions.



Figure 6. The fitting curve of the Raman spectrum for Char-PA-N<sub>2</sub>-48.

**Table 3.** Hybrid carbon in the form of the area ratio of the samples produced at different treatment conditions.

Samples	$A_{D1}/A_{G}$	$A_{D3}/A_{G}$	$A_{\rm D4}/A_{\rm G}$
Char	3.179	1.947	0.589
Char-PA	1.460	0.479	0.187
Char-PA-N <sub>2</sub> -12	2.014	0.481	0.385
Char-PA-N <sub>2</sub> -48	3.311	0.495	0.597
Char-PA-CO <sub>2</sub> -12	2.187	0.486	0.418
CH-PA-CO <sub>2</sub> -48	3.785	0.501	0.657
Char-PA-CO <sub>2</sub> -48H <sub>2</sub>	3.785	0.501	0.657

First, the values of  $A_{D1}/A_G$ ,  $A_{D3}/A_G$  and  $A_{D4}/A_G$  of Char-PA obviously decrease when compared to those of Char. In the process of  $CO_2$  activation, the defective structure at the edge of the aromatic layers and some small aromatic rings are consumed preferentially [43]. The consumption of the defective structure can promote the dehydrogenation of the big aromatic rings; and the removal of the small aromatic rings can help the inner reactivation of the big aromatic rings accompanied by the breakdown of the cross-linking structure [44]; these changes finally lead to a substantial increase in the quantities of crystalline  $sp^2$  bonding carbon atoms, which further promotes the stability of the carbon structure. Then, with the increase of the ball-milling time from 12 to 48 h, the values of  $A_{D1}/A_G$  and  $A_{D4}/A_G$ of Char-PA-N<sub>2</sub>/CO<sub>2</sub>-12/48 increase gradually; but there is a slight increase in the value of  $A_{D3}/A_G$ . It can be inferred that a strong mechanical collision caused by the ball milling has partly destroyed the crystalline sp<sup>2</sup> bonding carbon structure, decomposing it into the big aromatic rings, which is accompanied by the formation of new crosslinking structures. In particular, the variety of the hybrid carbon parameters of Char-PA-CO<sub>2</sub>-12/48 is more obvious than that of Char-PA-N<sub>2</sub>-12/48 under the same ball-milling time. Some oxygen atoms from dry ice are easily bonded and fixed to the carbon matrix in the form of cross-linking bonds (such as -COO- and -O-), and some oxygen-containing heterocycles under a local high temperature are caused by a strong mechanical collision; furthermore, the presence of O-containing structures can also promote the reorganization of aromatic fragments to form more big aromatic rings.

#### 3.4. Pore Structure Analysis by N<sub>2</sub> Adsorption

The N<sub>2</sub> adsorption isotherm and pore-size distribution of the samples under pyrolysis and different activation conditions are given in Figure 7, and the corresponding pore parameters are shown in Table 4.

Samples	$S_{\rm BET}$ (m <sup>2</sup> /g) <sup>a</sup>	$V_{\rm t}$ (m <sup>3</sup> /g) <sup>b</sup>	$V_{ m mic}$ (m <sup>3</sup> /g) <sup>c</sup>	Non- $V_{\rm mic}$ (%) <sup>d</sup>
Char	48.45	0.048	0.034	29.17
Char-PA	414.78	0.24	0.10	58.33
Char-PA-N <sub>2</sub> -12	715.89	0.33	0.22	33.33
Char-PA-N <sub>2</sub> -48	919.74	0.38	0.30	21.05
Char-PA-CO <sub>2</sub> -12	859.14	0.36	0.26	27.78
Char-PA-CO <sub>2</sub> -48	1259.74	0.42	0.34	19.056
Char-PA-CO <sub>2</sub> -48H <sub>2</sub>	1214.85	0.38	0.31	18.42

Table 4. The pore structure parameters of the samples at different treatment conditions.

<sup>a</sup> Specific surface area determined by the BET method for P/P<sub>0</sub> from 0.05 to 0.24. <sup>b</sup> Total pore volume calculated at P/P0  $\frac{1}{4}$  0.98. <sup>c</sup> Volume of micropores (< 2 nm) calculated by the *t*-plot method. <sup>d</sup> V<sub>t</sub> minus V<sub>mic</sub> (>2 nm).

First, the N<sub>2</sub> adsorption isotherm of Char is attributed to a type I according to the IUPAC classification, and its N<sub>2</sub> adsorption capacity is very small, showing small amounts of pores. The metaplast formed by the combination of transferable hydrogen with free radicals during pyrolysis can plug the pores, thus leading to an S<sub>BET</sub> value of 48.45 m<sup>2</sup>·g<sup>-1</sup>, V<sub>mic</sub> value of 0.034 m<sup>3</sup>·g<sup>-1</sup> and non-V<sub>mic</sub> value of 29.17% for Char, with a narrow size distribution of less than 2 nm. Then, the N<sub>2</sub> adsorption isotherm of Char-PA exhibits a typical characteristic of type IV, with the increase of the relative pressure from 0 to 1. This isotherm has begun to branch, and a hysteresis loop has also been formed with the increase of the relative pressure, indicating the formation of hierarchical pores. In the process of CO<sub>2</sub> activation, some micropores can be formed at the initial stage of activation, after which these micropores can further be enlarged into mesopores, as channels, can promote the diffusion of activated gas to help the production of new micropores [17,18]. Therefore, the N<sub>2</sub> adsorption capacities of Char-PA are higher than those of Char with the increase of the relative pressure, presenting an S<sub>BET</sub> value of 414.78 m<sup>2</sup>·g<sup>-1</sup> and V<sub>mic</sub> value of 0.1 m<sup>3</sup>·g<sup>-1</sup>. However, the non-V<sub>mic</sub> value of 58.33% of

Char-PA with a wide pore distribution indicates the rapid development of mesopores and macropores instead of that of micropores during CO<sub>2</sub> activation.



**Figure 7.** (**a**,**c**,**e**,**g**) The N<sub>2</sub> adsorption isotherm and (**b**,**d**,**f**,**h**) pore-size distribution of the samples at different treatment conditions.

After 12 h of high-energy ball milling, the  $N_2$  adsorption isotherms of Char-PA-CO<sub>2</sub>/N<sub>2</sub>-12 exhibit the typical characteristic of type IV, with an increase of the relative pressure from 0 to 1. With the increase of the ball-milling time from 12 to 48 h, the flat development of adsorption isotherms and a

small hysteresis loop can also be found for Char-PA-CO<sub>2</sub>/N<sub>2</sub>-48, with high N<sub>2</sub> adsorption capacities at a low pressure and presenting a rapid increase of the S<sub>BET</sub> and V<sub>mic</sub> values and an obvious decrease of the non-V<sub>mic</sub> value of Char-PA-CO<sub>2</sub>/N<sub>2</sub>-12/48, accompanied by a gradual narrowing of the pore size distribution. These changes indicate a sustained formation of new micropores and a rapid decrease of mesopores and macropores during the ball milling, which are related to the fact that the collapse of the mesopores and macropores caused by the strong mechanical collision brings about the production of new micropores. Furthermore, a stronger solid-gas reaction caused by the mechanical collision under dry ice can favor the development of the porous structure. Therefore, the variety of pore structures of Char-PA-CO<sub>2</sub>-12/48 is more obvious than that of Char-PA-N<sub>2</sub>-12/48 under the same ball-milling time.

# 3.5. Surface Chemical Structure Analysis of XPS

Figure 8 shows the broad scanning energy spectrum of all the samples, determined by XPS in the range of 10–1200 eV binding energy to obtain the strongest peak for most elements. There are two obvious peaks (C1s and O1s peaks) in Char-PA and Char-PA-N<sub>2</sub>/CO<sub>2</sub>-12/48, indicating the dominant position of C and O in the element composition; however, the disappearance of the O1s peak of Char is related to the release of the oxygen elements in the form of small molecules (such as CO, CO<sub>2</sub>) during pyrolysis. With the increase of the ball-milling time from 12 to 48 h, there is a slight increase in the oxygen content of Char-PA-N<sub>2</sub>-12/48 from 4.09% to 4.11%. A ball milling under dry ice can rapidly promote the combination of surface unsaturated carbon atoms with CO<sub>2</sub> to fix a large number of O atoms in the form of oxygen-containing functional groups; thus, the oxygen content of Char-PA-CO<sub>2</sub>-12/48 increases rapidly from 6.79% to 9.48%.



Figure 8. The survey XPS spectra of the samples at different treatment conditions.

In carbon materials, surface oxygen-containing functional groups are the most important functional groups that have been identified as affecting the surface chemical properties of carbon materials. In order to further explore the types and contents of oxygen functional groups on the surface of Char-PA and Char-PA-N<sub>2</sub>/CO<sub>2</sub>-12/48 quantitatively, the O1s peak of five samples is fitted and analyzed

according to different binding energies, as follows: carboxyl or ester carbon (C=O) at 530.9 eV, phenolic hydroxyl or ether (C–O) at 532.4 eV, carboxyl or ester carbon (O–C=O) at 533.8 eV and chemisorbed O<sub>2</sub> (or H<sub>2</sub>O) at 535.2 eV. The results of the curve fitting of the five samples are given in Table 5. In addition, the XPS spectra of Char and Char-PA-CO<sub>2</sub>-48H<sub>2</sub> are not treated further using the fitting method due to a minor oxygen content. After CO<sub>2</sub> activation, the carbonyl and quinone group (C=O) of Char-PA accounts for the most part (39.6%); its phenol and ether group (C–O) takes second place (27.3%), and the carboxyl group or ester group (O–C=O) and chemisorbed O (or H<sub>2</sub>O) come last (18.4% and 14.7%) out of all the oxygen-containing functional groups. After ball milling under N<sub>2</sub>, the proportions of C=O, C–O and O–C=O of Char-PA-N<sub>2</sub>-12/48 are gradually consistent with each other with the prolongation of the ball-milling time. After ball milling under dry ice, the proportion of O–C=O of Char-PA-CO<sub>2</sub>-12/48 increases and its proportion of C–O, C=O decreases gradually, indicating the existence of oxidation phenomena. The above results illustrate that the content and type of oxygen-containing groups in the samples can be controlled by the ball-milling treatment in different atmospheres.

**Table 5.** The results of the curve fitting of Char-PA and Char-PA-N<sub>2</sub>/CO<sub>2</sub>-12/48 in O1s from the XPS spectra.

Samples	C–O (%)	C=O (%)	O–C=O (%)	Chemisorbed O (or H <sub>2</sub> O) (%)
Char-PA	27.3	39.6	18.4	14.7
Char-PA-N <sub>2</sub> -12	29.5	35.4	25.6	9.5
Char-PA-N <sub>2</sub> -48	30.4	31.7	29.7	8.2
Char-PA-CO <sub>2</sub> -12	26.7	29.5	36.1	7.7
Char-PA-CO <sub>2</sub> -48	23.9	26.4	41.2	8.5

#### 3.6. Study of SO<sub>2</sub> Adsorption

In order to further explore the effect of the physicochemical structure of ACson SO<sub>2</sub> adsorption, an SO<sub>2</sub> adsorption test of Char-PA, Char-PA-N<sub>2</sub>-48, Char-PA-CO<sub>2</sub>-48 and Char-PA-CO<sub>2</sub>-48-H<sub>2</sub> from a simulated flue gas is performed at 80 °C for 210 min. In these tested samples, Char-PA-CO<sub>2</sub>-48-H<sub>2</sub> is obtained via a thermal annealing treatment of Char-PA-CO<sub>2</sub>-48 at 800 °C for 1 h in 5% H<sub>2</sub>/Ar atmosphere, and the results of the physicochemical structure and corresponding parameters are given in Figures 2–8 and Tables 2–4. It can be found that the thermal annealing process has removed almost all of oxygen-containing functional groups (the oxygen content is only 0.89% in Figure 8) but cannot further change its porosity, microstructure and surface morphology. The results of the SO<sub>2</sub> removal of Char-PA-N<sub>2</sub>-48, Char-PA-CO<sub>2</sub>-48 and Char-PA-CO<sub>2</sub>-48-H<sub>2</sub> are shown in Figure 9.



Figure 9. SO<sub>2</sub> removal of typical ACs: (a) SO<sub>2</sub> breakthrough curve and (b) SO<sub>2</sub> adsorption quantity.

First, the efficient adsorption of Char-PA is mainly presented within only 60 min, while the SO<sub>2</sub> concentrations of the gas outlet arrive quickly 1500 ppm; this result indicates that Char-PA has already been penetrated by  $SO_2$ . In addition, Char-PA can only achieve 21.2 mg/g at the end of the experiment. Therefore, Char-PA, with undeveloped pores and fewer activated sites, can only maintain an efficient SO<sub>2</sub> adsorption and conversion at the initial stage. Then, the SO<sub>2</sub> adsorption of Char-PA-CO<sub>2</sub>-48 can be maintained at 100% within 30 min. After that, there is a slow increase from 70 to 1500 ppm in the  $SO_2$  concentrations of the gas outlet, and its  $SO_2$  adsorption capacity can reach 138.5 mg/g at the end of the experiment. Remarkably, Char-PA-N<sub>2</sub>-48, with relatively developed pores and some active sites, also has a relatively high SO<sub>2</sub> adsorptive capacity (92.2 mg/g) at the end of the experiment, and its SO<sub>2</sub> adsorption curve is similar to the curve of Char-PA-CO<sub>2</sub>-48. In the presence of  $O_2$  and  $H_2O$ , the SO<sub>2</sub> removal of porous carbon is a multi-step heterogeneous reaction. First, SO<sub>2</sub>, O<sub>2</sub> and  $H_2O$ can be rapidly absorbed by a lot of micropores, inside of which the oxidation and hydration of  $SO_2$ with  $O_2$  and  $H_2O$  is further catalyzed by active sites to form  $H_2SO_4$  [45]; after that, the active sites can continue to migrate H<sub>2</sub>SO<sub>4</sub> from micropores to meso-/macro-pores to release the microporous space [46]. Therefore, Char-PA-CO<sub>2</sub>-48, with a large quantity of micropores and active sites, presents a high adsorption capacity as compared to that of samples in the previous literatures [47–49]. In addition, Char-PA-CO<sub>2</sub>-48-H<sub>2</sub>, with a large number of micropores and fewer active sites, has a limited adsorptive capacity (48.7 mg/g) at the end of the experiment, and its  $SO_2$  adsorption curve is similar to the curve of Char-PA. In the desulphurization process of Char-PA-CO<sub>2</sub>-48-H<sub>2</sub>, SO<sub>2</sub> can be adsorbed effectively by its micropores in the initial stage, but the adsorbed SO<sub>2</sub> within the micropores cannot be further catalyzed and migrated into the mesopores and macropores due to its limited active sites.

In order to measure the cyclic desulfurization performance of the prepared adsorbent, a thermal regeneration of Char-PA-CO<sub>2</sub>-48 is performed at 400 °C for 30 min in N<sub>2</sub> atmosphere, and the corresponding result is given in Figure 10. The SO<sub>2</sub> removal capacities of Char-PA-CO<sub>2</sub>-48 exhibit a general decreasing trend from 133.3 mg/g in the first-time desulfurization to 81.2 mg/g in the 10th cycle. Pi et al. [47] found that the pore structure and chemically active sites were damaged during a long-time (30 min), high-temperature (400 °C) and repeated thermal-treatment process, thus leading to rapidly decreased SO<sub>2</sub> removal capacities.



Figure 10. SO<sub>2</sub> removal capacities vs. cycling number of Char-PA-CO<sub>2</sub>-48.

# 4. Conclusions

The effect of physical and mechanical activation on the physicochemical structure of coal-based activated carbons (ACs) for  $SO_2$  adsorption has been investigated in this work. Char, using Jixi bituminous coal as raw materials obtained by pyrolysis, is activated sequentially via physical and mechanical methods. The results of the physicochemical structure of a series of AC samples indicate that a substantial reduction in the defective structure at the edge of the aromatic layers and the rapid growth of the aromatic layers accompanied by the dehydrogenation of the aromatic rings result in the

order transformation of microstructures of Char-PA and its severe carbon losses on the particle surfaces in the stage of CO<sub>2</sub> activation. Furthermore, the oxygen content of Char-PA is increased to 4.03%, and the proportions of the different oxygen-containing functional groups in Char-PA are as follows: C=O (39.6%), C-O (27.3%), O-C=O (18.4%) and chemisorbed O (or H<sub>2</sub>O) (14.7%). The pore development of Char-PA follows a hierarchical model, leading to a relatively low  $S_{BET}$  value (414.78 m<sup>2</sup>/g) and a high value of Non- $V_{\rm mic}$  (58.33%). Char-PA with undeveloped pores and fewer activated sites can only maintain an efficient SO<sub>2</sub> adsorption and conversion within 60 min and achieve 21.2 mg/g at the end of the experiment. In the subsequent mechanical activation under  $N_2$  and dry ice from 12 to 48 h, the strong mechanical collision can improve the surface morphology and destroy the parallelism of the aromatic layers and the constancy of the interlayer spacing, resulting in the disordered conversion of the microstructure and the formation of more defective structures with the prolonging of the ball-milling time. In addition, the collapse of mesopores and macropores caused by a strong ball milling facilitates the formation of more micropores, leading to a sustained increase in the SBET value from 715.89 to 1259.74 m<sup>2</sup>/g and of the micropore volume from 0.22 to 0.34 m<sup>3</sup>/g, as well as a sustained decrease in Non-V<sub>mic</sub> from 33.33 to 19.05% with the prolonging of the ball-milling time. However, the oxygen content of Char-PA-N<sub>2</sub>-12/48 increases slowly from 4.09 to 4.11%, presenting a similar distribution proportion, whereas the oxygen content of Char-PA-CO2-12/48 increases rapidly from 6.79 to 9.48%, presenting an increased proportion of O–C=O and a decreased proportion of C–O, C=O. It is worth noting that the varieties of physicochemical parameters of Char-PA-CO<sub>2</sub>-12/48 are more obvious than those of Char-PA-N<sub>2</sub>-12/48 under the same ball-milling time, which is related to the strong solid-gas reactions between  $CO_2$  and the carbon matrix caused by the mechanical collision under dry ice. The desulfurization efficiency of Char-PA-CO<sub>2</sub>-48 with a desirable physicochemical structure can be maintained at 100% within 30 min and reached 138.5 mg/g. Char-PA-N<sub>2</sub>-48 has a similar structure to Char-PA-CO<sub>2</sub>-48, thus presenting a relatively high  $SO_2$  adsorptive capacity (92.2 mg/g). Char-PA-CO<sub>2</sub>-48-H<sub>2</sub>, with fewer active sites obtained by the thermal annealing treatment, has a limited adsorptive capacity (48.7 mg/g) at the end of the experiment. After the 10th cycle of thermal regeneration, Char-PA-CO<sub>2</sub>-48 still has a strong adsorptive capacity (81.2 mg/g).

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