Optimal Design of a Distillation System for the Flexible Polygeneration of Dimethyl Ether and Methanol Under Uncertainty



Thomas A. Adams II



Tokiso Thatho



Matthew C. Le Feuvre



Christopher L. E. Swartz

McMaster University Department of Chemical Engineering McMaster Advanced Control Consortium

CCEC 2019 – Halifax, Nova Scotia - October 21, 2019

Download this Talk from LAPSE!

PSEcommunity.org/LAPSE:2019.XXXX

- Links to articles cited in the study
- Links to data sets and simulations used in cited studies





LAPSE Living Archive for Process Systems Engineering	Type search text: Login Register Submi	all fields t New About Contact Us Help	✓ SEARCH
LAPSE:2019.0620		Download	
Maximizing Our Impact: A call for the standardization of techno-economic analyses for sustainable energy systems design research	f Conference Presentation	Files [Download 1v1.pdf] (4.3 MB) Presentation Draft	Jul 11, 2019 [Full Details]
Thomas A Adams II		CC BY 4.0	[details]
July 11, 2019 This presentation makes the case for the development of a new ISO standard for conduction eco-technoeconomic analyses (eTEAs) within the field of energy systems engineering and chemical process systems engineering. The talk provides a motivating example of a recent study that showed how standardization of eTEAs made it possible to make fair comparisons between different types of power plants using carbon capture and sequestration by using eTEAs reported in the literature that have been converted to certain standards. That lead to informed decisions which were not possible without standardization methods, because it major variables are controlled such that analyses can focus on the value of the process concept itself rather than external factors like size, financing, and case-specific assumptions. Then, the talk outlines how the proposed ISO standards would work, their goals and scope, examples of standard practices, methods, and assumptions that could be used and what they might look like. The talk ends with a call for interested stakeholders to participate in the standardization process.			
		Record Statistics Record Views Version History [v1] (Original Submission) Verified by curator on This Version Number Citations	3 Jul 11, 2019 Jul 11, 2019 v1
Record ID LAPSE:2019.0620		LAPSE:2019.0620	Most Recent
Keywords eco-Technoeconomic Analysis, Life Cycle Analysis, Standardization, Technoeconomic Analysis		LAPSE:2019.0620V1	THIS VERSION
Subject Process Design	Process Design Adams TA II. Maximizing Our Impact: A call for the standardization of techno-economic analyses for sustainable energy systems design research. (2019). LAPSE:2019.0620		E-2019 0620
Suggested Citation Adams TA II. Maximizing Our Impact: A call for the standardization of tec sustainable energy systems design research. (2019). LAPSE:2019.0620			Original Submitter
Author Affiliations Adams TA II: McMaster University (ORCID) (Google Scholar)		momas A. Adams II	

Thomas A. Adams II

Basic Premise: Flexible Production



Design Under Uncertainty

- Operating policy: Operators will choose either DME or Methanol Mode depending on prevailing market conditions at that time.
- Uncertainty: Can only guess during the design phase what that proportion will be.
- Design Implications: If you think you will spend most of your time in Methanol Mode:
 - Invest in more capital to ensure lower operating costs for the Methanol section
 - Want less efficient DME section to save capital, since high energy costs will be brief



Optimization Strategy (Naïve Approach)

Decision variables are Minimize TAC of each column separately. $TAC_{BaseCase,Exp} = \sum_{c=C1..C4} Z_c$ number of stages above Because each column must meet a design spec $Z_c = \min TAC_{c,Exp}$ by definition, they can be split into the sum of and below feed for each \dots $N_{A,c}, N_{B,c}$ four minimization problems. column. s.t. $TAC_{c,Exp} = a_f TDC_c + AOC_{c,Exp}$ $AOC_{c,Exp} = h (Q_{H,c} U_{H,c} + Q_{C,c} U_{C,c}) (1 - \phi_{Exp,D}) (1 - \delta_c)$ Key uncertainty parameter. $+h(Q_{H,c}U_{H,c}+Q_{C,c}U_{C,c})(\phi_{Exp,D})\delta_{c}$ The amount of time we expect to $\delta_{c} = \begin{cases} 0 \text{ for } c = C1, C2 \text{ (MeOH Mode)} \\ 1 \text{ for } c = C3, C4 \text{ (DME mode)} \end{cases}$ operate in DME mode over the 15 Surface area of condenser / year life time. reboiler for column c $TDC_{c} = f_{1}(A_{C,c}) + f_{2}(A_{H,c}) + f_{3}(N_{A,c} + N_{B,c}, D_{c})$ $A_{C,c} = f_{4,c}(N_{A,c}, N_{B,c})$ Capital cost models (can be equations or table lookups) $A_{H,c} = f_{5,c}(N_{A,c}, N_{B,c})$ Diameter of column c $D_c = f_{6,c}(N_{A,c}, N_{B,c})$ All of these can be exhaustively pre-tabulated with rigorous Reboiler/condenser duties of $Q_{H,c} = f_{7,c}(N_{A,c}, N_{B,c})$ models in Aspen Plus. column c $Q_{C,c} = f_{8,c}(N_{A,c}, N_{B,c})$ Implemented as table lookup. **McMaster**



Solve quickly through exhaustive search



Download Slides at PSEcommunity.org/LAPSE: 2019.XXXX

Alternative Design Strategy





Very quick optimization, trivial extra work

Only 4 decision variables instead of 8.

 $TAC_{CaseA,Exp} = \sum_{c=A1,A2} Z_c$ $Z_c = \min TAC_{c,Exp}$ Still have the $N_{A,c}$, $N_{B,c}$ uncertainty factor. s.t. $TAC_{c,Exp} = a_f TDC_c + AOC_{c,Exp}$ $AOC_{c,Exp} = h(Q_{H,c,MeOH}U_{H,c} + Q_{C,c,MeOH}U_{C,c})(1 - \phi_{Exp,D})$ + $h(Q_{H,c,DME}U_{H,c} + Q_{C,c,DME}U_{C,c})(\phi_{Exp,D})$ $TDC_{c} = f_{1}(A_{C,c}) + f_{2}(A_{H,c}) + f_{3}(N_{A,c} + N_{B,c}, D_{c})$ $A_{C,c} = \begin{cases} \max[f_{4,C1}(N_{A,c}, N_{B,c}), f_{4,C3}(N_{A,c}, N_{B,c})] & \text{for } c = A1\\ \max[f_{4,C2}(N_{A,c}, N_{B,c}), f_{4,C4}(N_{A,c}, N_{B,c})] & \text{for } c = A2 \end{cases}$ The max function ensures that the equipment is large enough to handle both modes. McMaster

 $A_{H,c} = \begin{cases} \max[f_{5,C1}(N_{A,c}, N_{B,c}), f_{5,C3}(N_{A,c}, N_{B,c})] & \text{for } c = A1 \\ \max[f_{5,C2}(N_{A,c}, N_{B,c}), f_{5,C4}(N_{A,c}, N_{B,c})] & \text{for } c = A2 \end{cases}$ $D_{c} = \begin{cases} \max[f_{6,C1}(N_{A,c}, N_{B,c}), f_{6,C3}(N_{A,c}, N_{B,c})] & \text{for } c = A1 \\ \max[f_{6,C2}(N_{A,c}, N_{B,c}), f_{6,C4}(N_{A,c}, N_{B,c})] & \text{for } c = A2 \end{cases}$ $Q_{H,c,MeOH} = \begin{cases} f_{7,C1}(N_{A,c}, N_{B,c}) for \ c = A1 \\ f_{7,C2}(N_{A,c}, N_{B,c}) for \ c = A2 \end{cases}$ $Q_{H,c,DME} = \begin{cases} f_{7,C3}(N_{A,c}, N_{B,c}) for \ c = A1 \\ f_{7,C4}(N_{A,c}, N_{B,c}) for \ c = A2 \end{cases}$ $Q_{C,c,MeOH} = \begin{cases} f_{8,C1}(N_{A,c}, N_{B,c}) for \ c = A1 \\ f_{8,C2}(N_{A,c}, N_{B,c}) for \ c = A2 \end{cases}$

Can reuse the tabulated data from the Aspen Plus simulations without needing to rerun.

Quantify the Value of Flexibility.

Basically, my EXPECTED TAC is about 20% lower if I am flexible, regardless of what I expect.

"Noise" in equipment costs is expected and due to the impact of discrete decisions (# stages, discrete column diameters).

These are globally optimal.





Option B: "Fat / Skinny" columns

The column receiving the product feed, and the feed location changes with the mode.

Maybe I can save money by having one column for large loads and one column for small loads.





Well, ok, not as good.





Download Slides at PSEcommunity.org/LAPSE:2019.XXXX

Ok, but what if my predictions are wrong?



Design Under Uncertainty Options

Probability Distribution Functions

Find the design that minimizes Expected TAC

 $TAC_{CaseB,Exp} = \sum_{c=B1,B2} Z_c$

 $Z_{c} = \min_{N_{A,c,MeOH}, N_{B,c,MeOH}, N_{A,c,DME}} \sum_{i=1}^{i=S} P(\phi_{Exp,D,i}) TAC_{c,Exp,i}(\phi_{Exp,D,i})$

Example: Normal distribution around a guessed $\varphi_{\text{EXP, D}}$

Example: Uniform distribution of $\phi_{\text{EXP, D}}$ (i.e. no predictive knowledge at all).

Robust (Min Max) Formulation

Find the design that minimizes the worst case TAC of any outcome

$$TAC_{caseB,Exp} = \sum_{c=B1,B2} Z_c$$

$$Z_c = \min_{N_{A,c,MeOH}, N_{B,c,MeOH} N_{A,c,DME}} \max_{i=1..S} TAC_{c,Exp,i}(\phi_{Exp,D,i})$$

Example: Also useful with no predictive knowledge at all.

All of these can be solved to global optimality with no loss of fidelity in a few seconds.

Uncertainty formulation comparison



Design Under Uncertainty with No Predictions

- Both methods result in a single design without making assumptions.
- This is the Actual TAC depending on the outcome.
- Neither is better in all cases, but uniform distribution happens to be better more often.
- Both are very good





Conclusions

- Strategic tabulation and problem decoupling makes for very fast optimal design under uncertainty solutions with many scenarios to global optimality
- Can re-use design tables for many case studies
- Uniform distribution recommended (requires no knowledge of the final outcomes) to minimize overall risk at little cost

Download Slides at PSEcommunity.org/LAPSE:2019.XXXX

