

Modeling and Simulation of Nitrogen Generation by Pressure Swing Adsorption for Power-to-Ammonia: Supplementary Material

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January 2026

1 Adsorbent parameters

We study the kinetic separation of air $\mathcal{C} = \{\text{N}_2, \text{O}_2, \text{Ar}\}$ over a bed of carbon molecular sieve (CMS) pellets. We consider the commercial Takeda 3A CMS adsorbent studied in [1, 3, 4]. Parameters describing the adsorbent are given in Table 1.

Table 1: Adsorbent parameters.

CMS-T3A		
Bed porosity, ε [-]	0.3	[1, 3, 4]
Particle diameter, d_p [m]	$5.66 \cdot 10^{-3}$	[4]
Particle density, ρ_p [kg/m ³]	900	[1, 3, 4]
Particle heat capacity, $c_{p,p}$ [MJ/(kg·K)]	$1.05 \cdot 10^{-3}$	[4]
Particle porosity, ε_p [-]	0.3	[3]

2 Adsorption rate parameters

2.1 Adsorption equilibria

Following [3], we consider the modified Langmuir (ML) isotherm

$$q_\alpha^* = q_{\max,\alpha} \frac{b_\alpha P_\alpha}{1 + \sum_{\beta \in \mathcal{C}} b_\beta P_\beta},$$

given $\alpha \in \mathcal{C}$. The necessary component parameters were estimated in [3] based on the data in [1, 2] provided at temperatures $T \in [293, 313]$ [K] across pressures $P \in [1, 15]$ [atm]. Originally, in [3], the saturation capacity is reported on a mass basis with units q_α^{\max} . To get the saturation capacity on a volumetric basis, we multiply it by the particle density $q_\alpha^{\max} \rightarrow \rho_p q_\alpha^{\max}$. The Langmuir parameters were fit to temperature-dependent correlations

$$q_{\alpha,\max}(T) = k_{1,\alpha} - k_{2,\alpha}T, \quad (1)$$

$$b_\alpha(T) = k_{3,\alpha} \exp\left(\frac{k_{4,\alpha}}{T}\right), \quad (2)$$

$$n_\alpha(T) = k_{5,\alpha} - \frac{k_{6,\alpha}}{T}. \quad (3)$$

The component-wise parameters are reported (with original units) in Table 2. From the measured equilibrium capacities in [1, 2], the component-wise heat of adsorption ΔH can be experimentally computed from the Clausius-Clapeyron relation [1, 5]. We consider the averages reported in [3] seen in Table 3.

Table 2: Equilibrium isotherm parameters [3].

	N ₂	O ₂	Ar
k_1 [kmol/kg]	$1.13 \cdot 10^{-2}$	$5.817 \cdot 10^{-3}$	$9.556 \cdot 10^{-3}$
k_2 [kmol/(kg·K)]	$2.8 \cdot 10^{-5}$	$7.512 \cdot 10^{-6}$	$2.101 \cdot 10^{-5}$
k_3 [1/kPa]	$3.089 \cdot 10^{-4}$	$7.948 \cdot 10^{-6}$	$6.566 \cdot 10^{-5}$
k_4 [K]	359.7	1381	773.8

Table 3: Component-wise heat of adsorption [3].

	N ₂	O ₂	Ar
ΔH [MJ/kmol]	-13.39	-13.81	-14.23

2.2 Rate constants

Pressure-dependent models of the apparent time constants D_α/r_p^2 are introduced in [1] and fitted in [3], against the data in [2, 1]. We employ the supercritical-structural-Langmuir (SSL) model

$$\frac{D_\alpha}{r_p^2} = k_\alpha \sqrt{P_{r,\alpha}} (1 + b_\alpha P_\alpha)^2. \quad (4)$$

specified by the reduced pressure $P_{r,\alpha} = P_\alpha/P_{c,\alpha}$. The remaining parameters are specified in Table 4.

Table 4: Rate parameters [3, 6].

	N ₂	O ₂	Ar
k [1/s]	$9.0 \cdot 10^{-5}$	$2.4 \cdot 10^{-2}$	$4.7 \cdot 10^{-5}$
P_c [kPa]	3398	5043	4898

References

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